Manantial-Espejo Project
Canadian Standard NI 43-101

Santa Cruz Province, Argentina

Prepared For
Minera Triton Argentina, S.A.

Author:
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M3 Engineering & Technology Corp.
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A Qualified Persons

- Certificates of Qualified Persons and Consents of Authors
- Resumés of Principal Authors

Responsibility	Qualified Person	Registration
Resource Modeling	Dr. Michael Steinmann, PAS	Ph. D., P. Geo.
Reserves	Martin Wafforn, PAS	P.Eng.
Geology	Dr. Michael Steinmann, PAS	Ph. D., P.Geo.
Metallurgical Testing	Tom Drielick, M3	P.Eng.
Pit Geotechnical	Dr. Luiz Castro, Golder	P. Eng., Ph.D.
Process Plant	Dr. Conrad Huss, M3	Ph.D., P.Eng.
Tailings Facility	David Ritchie, Golder	P. Eng
Geohydrology	Todd Hamilton, GWI	P. Geo
Mine Planning–Underground	Allan Polk, Snowden	P.Eng.
Mine Planning–Open Pit	Michael Lawlor, Snowden	CP. Eng.

B Manantial Espejo Resource Estimate Composites

1 TITLE PAGE

This Technical Report has been prepared in accordance with the *National Instrument 43-101 Standards of Disclosure for Mineral Projects* ("NI 43-101") and the contents herein are organized and in compliance with *Form 43-101F1 Contents of the Technical Report* ("43-101F1"). The first two items are the Title Page and Table of Contents that are presented previously in this report and are simply mentioned herein to maintain the specific report outline numbering contained in *Form 43-101F1 Contents of the Technical Report*.

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See discussion in Section 1.

3 SUMMARY

3.1 Background

This Technical Report has been prepared following the completion of a multi-volume feasibility study prepared by an international team of professionals and consultants for the Manantial-Espejo Project. M3 Engineering & Technology Corporation ("M3") of Tucson, Arizona, USA has compiled the results from the feasibility study and Dr. Michael Steinmann, P. Geo. Senior Vice President of Exploration and Geology of Pan American Silver Corp. ("PAS"), a Qualified Person (as defined in NI 43-101), is the author of this Technical Report.

3.2 Property Ownership, Location and Description

The Manantial-Espejo Project is a silver and gold mine development project that belongs to Minera Triton Argentina S.A. ("Triton") and Compañía Minera Alto Valle S.A. ("Alto Valle"). The Project is operated and controlled by Triton and the mineral concessions are held either by Triton or by Alto Valle. Triton is controlled 50% by PAS and 50% by Silver Standard Resources Inc. ("SSR"). Alto Valle is controlled 80% by Triton, 10% by PAS, and 10% by SSR. Therefore, all assets and the Manantial-Espejo Project are controlled 50% by PAS and 50% by SSR. PAS became the operator of the Triton joint venture on January 1, 2004 when a decision was made to advance the Manantial-Espejo Project to a feasibility study stage.

Triton is currently advancing the Manantial-Espejo Mine Project with the assistance of M3 which is providing Feasibility Study Engineering Services.

The Manantial-Espejo Project is situated in Santa Cruz Province, 160 km west of San Julian on Route 25 and 50 km west of Gobernador Gregores, in southern Argentina (Patagonia).

The Manantial-Espejo property consists of 17 mineral concessions covering a total of 25,533 hectares, and extending roughly 36 kilometers east-west and 19

kilometers north-south. The property also includes ownership of 3 surface properties purchased by Triton to facilitate support and improve the performance of its mining and exploration activities. These surface rights cover an area of 43,207 hectares and sufficiently cover the current area of the reported mineral resources and planned facilities described herein.

3.3 Geology and Mineralization

The Manantial-Espejo deposit is hosted in Jurassic flat lying rhyolite volcanic units of the Chon Aike Formation lying within a broad 20 km wide zone of west-northwest striking structures. Mineralization is interpreted as occurring at the intersection of west-northwest trending fault zones and semi-circular structures that could be related to a possible volcanic center. Gold occurs mainly as electrum in pyrite while the silver occurs in a number of forms including native silver, argentiferous galena and silver sulphosalts. Sulfides account for up to 3 to 5% of the rock mass as veinlets and disseminations.

Styles of mineralization include massive quartz veins, vein breccias, sheeted and stockwork veining, and minor dissemination. Quartz is the main infill mineral, displaying distinctive textures indicating the overprinting of hydrothermal events which occurred in the area.

Primary ore minerals present in the quartz veins include argentite/acanthite, silver sulfosalts, electrum, native gold and silver, proustite, freibergite, uytenbogaardita, iodargirite, galena, sphalerite (mainly Fe-poor), pyrite, marcasite and chalcopyrite (Espinosa Neupert and Núñez, 1996). The gangue minerals include quartz (dominant), adularia, bladed calcite (replaced by quartz and adularia), and platy barite (replaced by quartz and adularia). Primary mineralization is mainly related to crustiform gray and white banded quartz, late breccias, replacements, and open space infillings (particularly vugs). There are six hydrothermal stages defined by cross cutting relations of vein textures in the Maria and Concepción Veins.

Secondary mineralization and enrichment includes limonites (jarosite, goethite), cerussite, pyrolusite, psilomelane and hematitic oxides. The oxidation zone is very variable ranging from the surface down to about 200 m locally due to fracture control.

3.4 Exploration and Development

The exploration concept for the Manantial-Espejo Project followed conventional geological mapping, target definition, and drill sampling to define zones of potentially economic mineralization. To date, three types of drilling have been used on the Manantial-Espejo Project: diamond core, reverse circulation and wagon drilling. The drilling data were used for metals exploration, resource modeling, geotechnical studies, metallurgical studies, and hydrological exploration/studies.

The status of the Manantial-Espejo Project exploration is to continue mapping, targeting, and drill testing the vast areas of untested potential economic mineralization on the property. This will be done at a reduced intensity as the Manantial-Espejo Project focuses on mine development.

3.5 Mineral Resource and Reserve Estimates as at December 31, 2005

A mineral resource estimate for the Manantial-Espejo Project as of December 31, 2005 is summarized in Table 1 below. This mineral resource estimate was prepared under the supervision of and reviewed by Dr. Michael Steinmann, P. Geo., Senior Vice President Geology & Exploration at PAS, who is a Qualified Person as that term is defined in NI 43-101.

Table 1 Total Resource

Domain	Class	Tonnes	Ag (g/mt)	Au (g/mt)
All Areas	Measured	5,041,202	176	2.47
	Indicated	3,684,610	159	2.20
	M+I	8,725,812	169	2.35
	Inferred	1,328,180	142	1.50

Inclusive of appropriate dilution depending on deposit geometry and mining method.

A mineral reserve estimate for the Manantial-Espejo Project as of December 31, 2005 is summarized in Table 2 below. This mineral reserve estimate was prepared under the supervision of and reviewed by Martin G. Wafforn, P.Eng., Director of Mine Engineering at PAS, who is a Qualified Person as that term is defined in NI 43-101.

Table 2 All Areas Reserves Proven and Probable

Area	Category	DMT	Ag g/mt	Au g/mt
All Open Pit	Proven	2,743,111	176.0	2.47
	Probable	1,133,693	152.6	2.60
	Total Reserves	3,876,804	169.1	2.51
All Underground	Proven	0	-	-
	Probable	1,713,825	248.8	3.56
	Total Reserves	1,713,825	248.8	3.56
Total	Proven	2,743,111	176.0	2.47
	Probable	2,847,518	210.5	3.18
	Total Reserves	5,590,630	193.6	2.83

Not all of the 8.73 million tonnes of the overall measured and indicated resources are mined by current plans. Table 3 summarizes the remaining 2.89 million tonnes of measured and indicates resources. The remaining measured and

indicated resource is less than the total resource minus the proven and probable reserve due to estimated losses of resource associated with mining (pillars etc.).

Table 3 Remaining Resources

Domain	Class	Tonnes	Ag (gpt)	Au (gpt)
All Areas	Measured	1,223,989	108	1.22
	Indicated	1,669,641	118	1.22
	M+I	2,893,630	114	1.22
	Inferred	1,042,230	133	1.2

Residual resource considers permanent loses from the global resource due to mining pillar loses necessary to extract the reserve.

3.6 Mining

The optimum mine plan approach for the Manantial-Espejo Project consists of a combination of open pit surface and underground mining methods. The surface mining method proposed for Manantial-Espejo ore is conventional open pit mining. In some areas, the open pits will also be used for underground access via in-pit portals. Open pits will be constructed for portions of the Maria, Karina-Unión, and Concepción deposits. Maria will be sub-divided into three (3) sub-pits.

The considerable variation in dip and thickness of the various mineralized zones throughout the property requires a number of different underground mining methods to be utilized to maximize the profitability and recovery of the mineral resources. The underground mining operations consist of either long-hole, cut and fill, or shrinkage methods to accommodate the geometry and accessibility.

3.7 Designated Author's Conclusions

The results of the feasibility study for the Manantial-Espejo Project indicate the project is technically feasible and economically viable at conservative silver and gold prices. It will create jobs and economic stimulus to an area that is economically depressed, and can be constructed and operated in an environmentally sound manner. Support from the government would likely ensure this project going forward. To date, the discussions with government agencies have been constructive.

3.8 Designated Author's Recommendations

It is the author's recommendation that the Manantial-Espejo Project should be developed pending availability of financing according to the Project Schedule illustrated in Figure 18 while focusing on cost control and schedule opportunities to allow early start-up taking full advantage of current favorable metal prices utilizing qualified construction contractors.

The anticipated tentative overall Project Schedule is provided in Figure 18 and highlights a 21 month schedule from authorization of project development through design and construction and first production. The SAG and Ball mill equipment delivery necessary for the processing plant is the critical path for the Manantial-Espejo Project. The project design is based on using ductile iron ring gear for the milling equipment in order to obtain a favorable delivery time and maintain the Figure 18 Project schedule.

The next steps for the project are to initiate the basic engineering and arrange for the project financing.

4 INTRODUCTION

This Technical Report has been prepared in accordance with National Instrument 43-101 *Standards of Disclosure for Mineral Projects* ("NI 43-101") and the contents herein are organized an in compliance with Form 43-101 F1 *Contents of the Technical Report.* This Technical Report has been prepared for Triton for the purpose of (1) reporting and summarizing the results of the feasibility studies completed in 2005, (2) providing a support document to pursue project financing, and (3) updating the reserve and resource estimate for the Manantial-Espejo Project.

Dr. Michael Steinmann, P.Geo., PAS's Senior Vice President Geology & Exploration serves as the Qualified Person with respect to the mineral resources statements described herein in sections 2, 9, 10, 11, 12, 13, 14, 15, 16, 19, 20, 21, 22, 23, 24 and the illustrations of this Technical Report. In addition, Dr. Steinmann is the author of this Technical Report and serves as the primary Qualified Person with respect to the contents of this Technical Report that is a consolidation of work from several other professionals indicated herein in this section 4. Dr. Steinmann visited the site on May 26 to 28, 2004 and again on May 16 to 18, 2005.

PAS's Mr. Martin Wafforn, P.Eng, Director of Mine Engineering, serves as a Qualified Person with respect to the mineral reserve statements contained herein this Technical Report described herein in sections 2, 19, and 25 of this Technical Report. Mr. Wafforn visited the site May 26 to 28, 2004 and again April 16 to the 18, 2005.

PAS retained Qualified Persons from M3 to provide assistance in preparing the Manantial-Espejo feasibility study, performing Qualified Person reviews, and preparing this Technical Report for the Manantial-Espejo Project. M3's work included a review of numerous project development reports referenced in section 23 of this Technical Report and to summarize the various reports as necessary to complete the requirements of this Technical Report. M3's work included development of a design and capital and operating cost estimate for the project's plant and site infrastructure requirements described herein in section 25 of this Technical Report. Dr. Conrad Huss, P.Eng. with M3, is the Qualified Person responsible for preparation of this capital estimate and Mr. Thomas Drielick, P.Eng. and Dr. Huss provided Qualified Person assistance for metallurgical testing, plant design, infrastructure design and capital and operating cost estimations described herein in sections 18 and 25 of this Technical Report. Neither Dr.

Huss nor Mr. Drielick has visited the site due to timing and logistical constraints; however, Dr. Huss did have Sam Maldonado of M3 to visit the Manantial-Espejo Project site on March 21, 2004.

Parallel to the M3 effort, MWH Argentina, S.A. prepared and submitted an Environmental Impact Statement, ("EIS").

PAS also retained Mr. Robert Wells of EV Technical Services Inc. to develop the mineral resource and reserve estimate for the Manantial-Espejo Project described in sections 3, 9, 10, 11, 12, 13, 14, 15, 16, and 19 of this Technical Report. The work entailed analysis and verification of the Manantial-Espejo Project's data and developing the estimate of mineral resources for the mineralization comprising the Manantial-Espejo Project. Mr. Wells visited the site more than 100 days on various occasions during the years of 2004 and 2005. Mr. Wells is well experienced in mineral resource and reserve model development; however, he is not a certified Qualified Person. As such, PAS's Dr. Michael Steinmann has reviewed and verified the work of Mr. Wells.

In addition, PAS retained Snowden Mining Industry Consultants Inc. ("Snowden") to build the mine plan and develop production schedules in accordance with the CIM Mineral Reserve definitions referred to NI 43-101. Snowden engineers Allan Polk, P. Eng. and Michael Lawlor, CP. Eng. are Qualified Persons responsible for preparation of the Underground and Open Pit mine plans respectively described herein in sections 3, 19, and 25. Neither Allan Polk nor Michael Lawlor has visited the Manantial-Espejo Project site due to timing and logistical constraints.

PAS also retained Golder Associates Ltd. ("Golder") to conduct geotechnical and support geochemical studies for the open pits, underground mines, and tailings facility designs. Golder engineers Dr. Luiz Castro, P. Eng. and Dave Ritchie, P. Eng. are Qualified Persons responsible for geotechnical studies described herein in section 25. Luis Castro has visited the Manantial-Espejo Project site, but Dave Ritchie has not due to timing and logistical constraints.

In addition, PAS retained Ground Water International ("GWI") of Lima, Peru to conduct geohydrological studies and develop a hydrologic model of the surface and groundwaters of the Manantial-Espejo Project site. GWI's respesentative Todd Hamilton, P. Geo. directed the geohydrologic studies and visited the Manantial-Espejo Project site on several occasions during 2004 and 2005. Mr. Hamilton serves as the Qualified Person responsible for defining the hydrologic aspects of the Manantial-Espejo Project described in section 25 of this Technical Report.

The data, reports, and other information used for the compilation of this Technical Report were obtained from personnel in the PAS offices in Vancouver, British Columbia, Triton's offices in Argentina, M3's offices in Tucson, and from the various consultants and contractors listed in Appendix A who has prepared the reports listed in section 23.

All tonnages stated in this report are dry metric tonnes (dmt or mt) unless otherwise

specified. Ounces pertaining to silver metal content are expressed in troy ounces.

Qualified Persons

Information and data for the resource and reserve estimates were obtained from Triton personnel in Argentina and was compiled and extensively evaluated by Mr. Robert Wells of EV Technical Services Inc.. Information and data for matters pertaining to metallurgy and processing, cost estimates, environmental and geotechnical investigations, and economic analyses were provided by PAS during the preparation of feasibility study by M3. Based on the above and other data, Dr. Michael Steinmann and Mr. Martin Wafforn, both of PAS, reviewed and verified the mineral resource and reserve estimation work for the Manantial-Espejo Project and serve as the Qualified Persons for the resource and reserve estimates respectively. The Qualified Persons for the Pit, Facilities, and Tailings Geotechnical Analysis are Dr. Luiz Castro and Dave Ritchie of Golder.

The Qualified Person for Geohydrology is Todd Hamilton of GWI.

M3 provided capital cost estimates based on M3 flowsheets and plant layout, and design criteria.

Dr. Michael Steinmann of PAS is the designated author of this Technical Report.

The following Table 4 sets out the Qualified Persons involved in the preparation of this Technical Report and the portions of this Technical Report for which they are responsible, respectively.

Table 4 Qualified Persons

Qualified Person	Technical Report Section
Dr. Michael Steinmann	2, 9, 10, 11, 12, 13, 14, 15, 16, 19, 20, 21, 22, 23, 24 and the illustrations
Martin Wafforn	2, 19, and 25
Tom Drielick	18 and 25
Conrad Huss	18 and 25
David Ritchie	25
Todd Hamilton	25
Allan Polk	3, 19, and 25
Michael Lawlor	3, 19, and 25

5 RELIANCE ON OTHER EXPERTS

The Qualified Persons for this Technical Report have relied upon the reports referenced in Section 23 – References and opinions and statements from the various Qualified Persons and non-Qualified Persons listed in Appendix A in preparing this Technical Report.

These reports, documents, and statements were found to be generally well organized and presented, and where applicable, the conclusions reached are judged to be reasonable. It is assumed that these reports and documents were prepared by technically qualified and competent persons. It is also assumed that the information and explanations given verbally to the Qualified Persons and those assisting Qualified Persons by the employees of PAS, Triton, and the various consultants and contractors who provided the reports listed in section 23 during the time of preparation of the Manantial-Espejo Project feasibility study and this Technical Report were essentially complete and correct to the best of each employee's, contractor's, or consultant's knowledge, and that no information was intentionally withheld. It is the opinion of the author of this Technical Report that the materials referenced above are prepared and presented according to Mining and Engineering Contract Industry Standard specifications. The author concludes that the contents are reasonably organized and presented and the conclusions reached are prudent.

In addition, M3 and the author of this Technical Report have reviewed the following work and concludes they are in generally well organized and presented, and where applicable, the conclusions reached are judged to be reasonable:

- Negotiations with the power company were by Triton and as such all power line capital and operating costing data was supplied by Triton.
- Mining designing and costing are by Snowden.
- Tailings design and capital costs are by Golder. M3 supplied the operating costs.
- Resource estimate by Triton.
- Environmental aspects of the project are by Montgomery Watson Harza.
- Reserve estimate by Robert Wells and Snowden.

In addition, the author has relied upon the information contained in a report by Pincock Allen & Holt dated April 6, 2001,which analyzed and concluded that the assaying and security procedures have been carried out according to accepted industry practice. In addition, the author has relied upon the information provided and discussions held with Mr. Robert Wells of EV Technical Services Inc. who preformed the Manantial-Espejo Project data verification evaluations. These reports, documents, statements, and evaluations were found to be generally well organized and presented, and where applicable, the conclusions reached are judged to be reasonable. It is assumed that these are technically qualified and competent people and their information and explanations given are essentially complete and correct to the best of their knowledge and that no information was intentionally withheld. It is the author's opinion that the conclusions reached from the information provided by these people in accordance with Mining and

Engineering Industry Standards.

6 PROPERTY DESCRIPTION & LOCATION

The Manantial-Espejo Project (Manantial-Espejo) is located in the Magallanes Department of the Santa Cruz Province in southern Argentina and is centered at the geographical coordinates of 69° 30' west longitude and 48° 46' south latitude (see Figure 2). The proposed mine development is located within a portion of the San Lorenzo and Manantial-Espejo "Estancias" (essentially ranches) which titles have been acquired by and owned free and clear by Triton.

The Manantial-Espejo property consists of 17 mining concessions granted by the Mining Authority of Santa Cruz to Triton and to Minera Altovalle S.A. (hereinafter jointly referred to as "Triton") as shown in Table 5 below, covering a total of 25,533 hectares, and extending roughly 36 kilometers east-west and 19 kilometers north-south. These mining concessions are contiguous and were located by legal survey. Under the Argentine Mining Code, the mining concession vests the concessionaire with a property title over the mine and therefore mining concessions are also called mining properties. The mining properties are, by law, granted in perpetuity under certain conditions (hereinafter "good standing conditions") including the payment of "canones" to the Santa Cruz Province (exploitation fees payable per mine and calculated on the type and amount of mining claims of each mine during its life), the fulfillment of certain legally required "works" on the mine (minimum mine works, survey and continuous works in order to avoid abandonment) and the presentation and fulfillment of a plan containing minimum expenditure requirements ("Investment Plan").

To the best of the authors' knowledge, Triton has complied with and continues to comply with the obligations related to the mining claim payments and the "works" requirements to be done in the mining property. With regards to the Investment Plan, Triton has filed a presentation with the Mining Authority of Santa Cruz containing an estimate of the works to be carried out and the investments that are necessary to such effect. Triton believes it is presently in compliance with such presentation and has received a resolution of acceptance of Triton's Environmental Impact Statement from the Mining Authority authorizing the development of the Manantial-Espejo Project. As such, there is no expiration date associated with the Manantial-Espejo Project's mineral concessions.

The good standing of the mining properties has been recently confirmed by the Mining Authority of Santa Cruz through Certificate N°006/2006, dated February 17, 2006 of Minera Triton Argentina S.A. and Certificate Nº 007/2006, dated February 17, 2006 of Minera Altovalle S.A., issued by the Santa Cruz´s Notary of Mines.

Table 5 summarizes the mining properties and Figure 3 provides plan details for the claims and estancias (i.e. ranches).

Table 5 Triton Mineral Concessions (All Claim Types are "MINA")

	Name	Document No.	Mineral Rights Owner	Number of Claims	Surface Area Hectares
1	Ayelen	411.694-B-95	Altovalle	27	2,700.00
2	La Laguna	407.215-CMSJ-93	Altovalle	24	2,400.00
3	Maria Este	413.930-B-95	Altovalle	18	1,800.00
4	La Madriguera	407.216-CMSJ-93	Altovalle	24	2,400.00
5	La Alianza I	407.781-B-94	Altovalle	10	990.03
6	La Alianza II	407.780-B-94	Altovalle	5	500.00
7	La Gruta	404.149-B-97	Altovalle	22	2,138.50
8	Candelaria	411.583-N-94	Altovalle	18	1,798.00
9	San Lorenzo II	408.610-T-98	Altovalle	8	800.00
10	Manantial Oeste II	408-960-B-98	Altovalle	1	100.00
11	Rosa	410.234-T-99	Triton	3	224.00
12	Susie	415.131-A-00	Altovalle	10	10,000.30
13	Luciana	414.705-T-00	Triton	30	2,978.45
14	Sol	414.704-T-00	Triton	21	2,003.16
15	Ana Maria	401.561-A-01	Altovalle	7	700.00
16	Patricia I	401.562-A-01	Altovalle	3	300.00
17	La Esmeralda	403.399-A-02	Altovalle	27	2,700.00
				TOTAL	**25,532.44**

As noted above, there are no expiration dates associated with the above mineral concessions.

The property also includes free and clear ownership of three surface properties purchased by Triton to provide areas for exploration and mine development activities. These surface rights cover an area of 43,207 hectares and sufficiently cover the current area of known resources and planned facilities necessary for development (See Figure 3).

Production from the Manantial-Espejo Project is subjected to royalties to be paid to Barrick Resources Ltd. ("Barrick") as follows:

- 60 cents per metric ton of ore mined from the Property and fed to process at a mill or leaching facility with a maximum of 1 million tons; and
- One half of one percent (0.5%) of net smelter returns derived from the production of minerals from the Manantial-Espejo Project.

In addition, Triton is required to negotiate a royalty payable to the Santa Cruz Province applied against basically the operating cashflows of the Manantial-Espejo Project which is dependent on the degree of metal extraction at the site up to a maximum of 3% of the operating cashflows according to the following:

- 2 to 3% of operating cashflows for direct shipped ores and low-grade concentrate products;
- 1 to 2% of operating cashflows for high grade mineral concentration or doré production; and
- 0 to 1% of operating cashflows for final bullion production.

The processing circuit described in this Technical Report will produce a doré product on-site and will therefore demand a 1 to 2% operating cashflows royalty payable to the Province of Santa Cruz. This Technical Report has assumed a 1.7% operating cashflow royalty payment to the Province of Santa Cruz.

The Manantial-Espejo Project has no known existing environmental liabilities. Development of the Manantial-Espejo Project requires securing the permits described in the Table 12 permit matrix. There are no known issues that would prevent Triton from securing all these permits listed in the matrix.

MWH performed an Environmental Impact Study (EIS) for the Manantial-Espejo Project as required under the laws of the Province of Santa Cruz and the Argentine Republic. The study includes all the items required under Argentine legislation, including a detailed report of the base line and the consulting steps taken with regard to the community and the authorities.

The EIS identifies the main environmental impacts, both positive and negative, arising from the project in such environment, and lists mitigation steps that are necessary in an Environmental Care and Management Plan, which also includes a full Environmental Monitoring and Social Program.

The EIS performed for the Project did not identify any severe environmental impacts that could compromise the project's feasibility from the environmental point of view.

The identified environmental impacts are in almost all cases low to moderate and can be reasonably mitigated by the Environmental Care and Management Plan attached to the Project.

The balance between the unwanted effects that could arise by implementing the Manantial-Espejo Project, against the local benefits that would be obtained, is favorable to the performance of the Manantial-Espejo Project.

The EIS has been submitted and a resolution of acceptance has been received from the Mining Authority in the Santa Cruz Province of Argentina. The following permit list provided in Table 12 indicates the current status of major permits:

Table 6 Permit Matrix

Type of Permit	Enforcement Authority	Permit	Status
ENVIRONMENT	Province Mining Directorate of Santa Cruz (DPM)	EIS: Environmental Impact Study	Presented on 07/11/05. Triton presentation of response to DPM final questions 7/03/06. Waiting formal approval.
		Mining Producer Register	Granted -Annual Renewal
	Water Resources Office of the Province of Santa Cruz	Water extraction and use - Exploration Phase	Presented on 01/09/05 Approved on 27/10/05 by Disposition 011/DPRH/05
	Environment Secretariat of the Province of Santa Cruz	Registration in the "Generation of Hazardous Waste Register"	Requested on 28/October/05.Legal and technical report approved. Waiting for a resolution of the Authority.
	Gobernador Gregores' Municipality	Municipal License- Offices	Granted
CONSTRUCTION and TRANSPORTATION	Commerce and Industry Division of the Province of Santa Cruz	Registration in the Commerce and Industry Activities Register	Granted on 15 December 05
	Registro Nacional de Armas (RENAR)	License as "user who received explosives services"	Granted on 20-January-2006
	National Communications Commission (CNC)	Radios Permit	Granted. Frecuencies habilitated by authorization N° 18401/2005
TAXATION - LABOR	National Mining Secretariat	Tax Stability	In process
		Registration in Law 24 196 (Other benefits: Double Deduction- Accelerated Depreciation- Importation of Equipments	Granted in 1997 - Valid up to January 2006
	Federal Administration of Public Revenues (AFIP)	National taxes registrations (DGI)	Granted
		Importer-Exporter registration. (DGA)	Granted
	Subsecretaria de Recursos Tributarios de Santa Cruz	Tax Provincial Registration	Granted
		Application for exemption over exportations.	To apply when exporting.
	Commerce and Industry Division of the Province of Santa Cruz	Application for Certificates of origin for exportations.	To apply when exporting.
	Secretary of Labor of Santa Cruz -Labor and Union Authorities	Collective Labor Agreement - Mining employees. (AOMA)	Without Collective Labor Agreement by now.

7 Accessibility, Climate, Local Resources, Infrastructure And Physiography

Although remote, the access to the project is reasonably good with some occasional winter road closures. The main access is via the provincial Ruta (Route) 25, a wide gravel secondary road that connects the project with San Julian, a town of approximately 5,500 inhabitants located 160 km to the east on the Atlantic Coast and with Gobernador Gregores, a town of 2,519 inhabitants, located approximately 60 kilometers (km) to the west. Access to the site is by an 8 kilometer gravel road off provincial Ruta 25. Commercial airline service is available into the area through either the city of Comodoro Rivadavia which lies approximately 400 kilometers north or the city of Rio Gallegoes which lies approximately 300 kilometers south of the town of San Julian.

The topography of the region is generally characterized by relatively low-lying mesas with broad flat valleys, containing no, or poorly-developed, drainage channels. To the north, the Deseado massif area is characterized by bedrock knolls and hills of moderate relief, with interspersed “deflationary” (probably wind-eroded) basins, containing flat-bottomed playas and often ephemeral shallow ponds and lakes with internal drainage. The Manantial-Espejo Project site is extremely arid and has very limited development of soils and vegetation. The elevation of the project site is situated between 350 and 400 meters above sea level (masl).

The northern part of the site contains bedrock knolls and hills of the Deseado Massif, with interspersed "deflationary" basins, containing flat-bottomed playas and usually ephemeral shallow ponds and lakes with internal drainage.

The southern portion of the site is dominated by a broad, flat valley known as the Pampa which trends east-southeast and lies between the Deseado Massif to the north and a volcanic plateau to the south. The Pampa is interpreted as a paleo-canal of the Rio Chico. The "Pampa" basin extends 150 km east from a point about 2 km east of Gobernador Gregores to the Atlantic coast near San Julian. The Pampa ranges in elevation from 310 to 298 masl and the elevation typically varies less than 10 m across the valley floor. Both the Pampa and the mesa on the southern portion of the camp are largely formed of Tertiary and Quaternary glacially-derived gravel and cobble deposits.

The surface elevation ranges between 250 masl in the east to 480 masl in the western portion of the property. Within the Deseado Massif, approximately 35 to 40% of the surface is outcrop exposure and the other 60 to 65% is comprised of a rubbly sub-crop covered by a thin layer of wind blown soil. Several exploration drill holes encountered overburden and regolith to depths of up to 20 meters. Volcanic domes generally form topographic highs, and vuggy silica zones, more resistant to weathering, form prominent knobs and pinnacles. Elsewhere on the property, bedrock generally does not occur at the surface, except for portions of the mesa south of the site which contains remnant Tertiary basalts.

These basalts typically overlie glacial gravel and cobble deposits. The margins of these basalt sequences form steep cliffs with talus cones from mass wasting of the columnar-jointed flows. Other mesas, free of basaltic cover, have a more rounded profile.

A meteorological station located near the Maria Vein (as described in section 9 hereto) at Manantial-Espejo provides local precipitation, potential evaporation and temperature data for the period May 1997 to date. The station was replaced with a new station following damage caused by a vehicle collision in September 2004. Longer-term meteorological data is available from the Gobernador Gregores airport, located about 55 km west of the site, for the period 1963 to 2003. Vector Argentina (2005) compared precipitation data for the Manantial-Espejo and Gobernador Gregores and found the correlation was generally good between the two stations.

The climate at the project area is a dry to arid continental type. The average monthly temperatures vary between 1°C (June and July) and 15°C (January and February). The Patagonia Region is well known for fierce westerly cold winds, particularly during August to October when westerly daily winds can gust between 120 to 170 kph. Highest average monthly precipitation at Manantial-Espejo has been recorded for June, at 21 mm, coincident with the lowest levels of potential evaporation for the year, at 7 mm.

The general area is low lying, undulating terrain. The climate is dry, (average rainfall 158 mm per annum), and cool to cold. Snowfalls occur in winter, and are generally light, but some occasional more severe snowstorms have occurred. The area is commonly

subjected to high winds. Silver and gold mineralization is known to be quite widespread in the general area, from exploration activity reported over the past twenty years.

Snow frequently accumulates on site between June and August, and infrequent snowfall events can range up to about 50 mm or more based on limited data. Annual potential evaporation is estimated at between 750 mm and 1,250 mm (Golder., 2005). An annual potential evaporation of 1,000 mm was assumed for the Manantial-Espejo site for the purposes of the Project design.

Average monthly precipitation ranges from approximately 100 mm of rainfall in January to approximately 10 mm of rainfall in June and July. Overall, the region is arid.

The Triton owned surface rights are sufficient to allow for the mine development described in this Technical Report.

Initial Construction power will be supplied by on-site diesel electric generator sets. Permanent electrical power to the project site will be supplied from a proposed new 132 kV overhead transmission line. An agreement has been reached with the Provincial and National Government to share in the cost of construction of a new approximately 200 kilometer 132 kV overhead transmission line and associated components. This line will supply power to the Manantial-Espejo Project as well as the community of Gobernador Gregores. The provincial Government will manage the installation of the power line. This power line will be fed from an interim natural gas generation facility located 160 kilometers east of the Project near the town of San Julian. It is anticipated that a connection to the National power grid will be completed in late 2008 and the interim natural gas generation facility will be decommissioned. This powerline installation will be sufficient for the requirements of the Manantial-Espejo Project described in this Technical Report. At the mine's main substation, provisions for temporary connections to portable standby diesel generator(s) will be included in the design and switchgear lineup used to provide limited standby electrical power to process critical loads. The generator connection interface can be made directly at 3.3 kV switchgear using a manual transfer scheme, or at the 380 Volt level connected via a manual transfer switch and dedicated motor control center to which the critical loads will be served. The exact configuration will be determined during design once the critical loads are identified and located.

Water for the Manantial-Espejo Project will be supplied from underground mine water and surface mine dewatering wells. Water from the wells will be pumped to a Fresh/Fire water tank located at slight elevation relative to the process area. Water will be pumped and distributed from this tank for use at the site. The average site make-up water requirement is estimated to be 15 L/s (54 m^3/hr or about 1300 m^3/day); however, this will vary somewhat depending on the season and special requirements, such as at plant startup. Based on a 10-year mine life, the total water requirement for the operation is estimated at about 4.7 million cubic meters (Mm^3), or roughly 4% of the estimated ground water resources practically accessible on the project site as defined by a comprehensive site hydrological evaluation completed by GWI of Lima, Peru. The

hydrologic study estimates the annual recharge and regional through flow that needs to be extracted to allow for mining at about 35,000 m^3/a or 3.2 Mm^3 over the life of the mine. Most of this water will be replaced within the first 25 years following closure of the mine and shutting down the dewatering although full water table recovery around the Maria Central and Karina- Unión Pits will require substantially longer.

The plant tailings will be neutralized in detoxification tanks where the weak acid dissociable residual cyanide content will be oxidized to the relatively non-toxic form of cyanate using sulfur dioxide and oxygen, with copper sulfate as a catalyst. Milk of lime will also be added to maintain a slurry pH in the range of 8.0 to 8.5. The more stable iron cyanides are removed from solution as an insoluble ferrocyanide precipitate. The cyanide levels are thereby reduced to an acceptable level for discharge to the tailings impoundment. The detoxification reactors tanks will provide a residence time of approximately two and a half hours. Slurry discharged from the detoxification circuit will be final plant tailing and will be pumped to a tailings impoundment.

A comprehensive tailings site evaluation study was undertaken as part of the feasibility preparation. A total of 6 sites were evaluated with a matrix of 11 parameters. Based on this analysis the selected tailings disposal site was the collapsed caldera that has been designated as the North Volcanic Centre (NVC). It is a low risk site because it is completely contained topographically (there is no external drainage). The selected tailings storage area is a closed drainage basin within a collapsed caldera located approximately 4.5 kilometers to the North of the proposed plant site. The geological, geotechnical and geohydrological aspects of this area are favorable for providing stable long term tailings disposal given its natural enclosed basin features. The facility to be constructed includes a primary slurry disposal and an external decant and seepage collection pond. Solution accumulated in the reclaim pond will be recycled to the plant as makeup water. Given the arid conditions in the region, the system will be maintained as a complete solution recycle facility.

The tailings disposal facility is completely founded on the relatively impervious siltstone that is partly covered with lacustrine clays. This siltstone, which occurs within the NVC, has an estimated maximum thickness of at least 40 m, and thins at the edges. A total of nine hydraulic tests were carried out within the North Volcanic Centre siltstone at two wells and on two open boreholes, both within the upper fractured portions and deeper within the lower, less disturbed siltstone, with a slight bias in favor of the fractured siltstone. The geometric mean horizontal hydraulic conductivity was 3 x 10-8 m/s, considered to be of low permeability. As is typical for horizontally-layered formations, vertical hydraulic conductivity is expected to be 2 to 10 times less. The facility has three other elements; the tailings storage area, a reclaim pond and a ditch around the perimeter of the tailings area to collect runoff from the surrounding high ground and also seepage from the tailings.

Tailings water will be pumped or will seep through the main dam into the reclaim pond. The main dam is designed as a leaky dam. The reclaim pond will also collect water from the perimeter ditch. Any water that accumulates in the external pond will also be pumped

to the reclaim pond. The water in the reclaim pond will be re-circulated to the mill. Due to the arid conditions in the region, the tailings system will be a complete solution recycle facility.

In addition, Triton has selected sufficient areas for the waste dump and plant sites required for the Project.

At the present time there is no land line or cellular telephone coverage in the area of the mine site. Based on the remote mine site location, radio or satellite telecommunication technology using tower type repeater stations will have to be considered. Detailed options to provide voice and data service for the project were not examined, but have been included as allowances in the Manantial-Espejo Project's capital cost estimate. The Manantial-Espejo Project plan includes utilization of an existing radio system for on site operations and maintenance communications.

During the operation phase, the Manantial-Espejo Project will require approximately 400 direct work positions. Given the extreme sparse population of the region, recruitment and training programs are a significant consideration for the Project. Triton has begun characterizing the capabilities of the potential workforce in the region, the province, and at the national level. The results of this characterization work will be used to facilitate the employment selection process and define the training requirements which will be sufficient for staffing the Project. Triton has designed and is carrying out a selection and recruitment Human Resources plan that supports the construction and operational stages of the Project. This includes an analysis of the type and amount of labor required, development of a digital Human Resources system, and implementation of training planning.

Indirect employment would include new work positions related to the building of houses, subcontracting of services related to the project and due to the development of local micro enterprises, such as food provisions or services related to the project (transport and accommodation).

8 HISTORY

In 1989, ownership of the original interest in the mineral properties constituting the Manantial-Espejo Project was acquired by Mr. Roberto Schubach. Mr. Schubach sold the mining rights to St. Joe Minerals which was later acquired by Lac Minerals Ltd. in 1991. Barrick, through its subsidiary Barrick Exploraciones Argentina S.A., acquired acquired Lac Minerals and assumed ownership of the Project in 1994.

From 1996 to 1998, Triton Mining Corporation acquired 80% of the Manantial-Espejo property through fulfillment of an option agreement with Barrick and assigned these rights to their wholly owned Argentine subsidiary Minera Triton Argentina S.A. ("Triton"). Barrick and Triton (Argentina) subsequently incorporated Compania Alto Valle S.A. ("Alto Valle") for the purpose of holding beneficial title to the properties, and pursuant to a shareholders' agreement, Barrick held 20 percent and Triton held 80

percent of the shares of Alto Valle, respectively. Triton was designated operator of the project.

In 1998, Black Hawk Mining Inc. ("Black Hawk") purchased all of the issued shares of Triton Mining Corporation, which was a public company with shares traded on the Toronto Stock Exchange.

Also in 1998, Silver Standard Resources Inc. ("SSR") entered into an option agreement with Triton Mining Corporation, now a wholly-owned subsidiary of Black Hawk, to acquire a 50% interest in Triton (Argentina). In 2001, SSR acquired Barrick's 20% interest in Alto Valle, half of which was sold to Black Hawk in consideration for an interest in an unrelated mining venture.

In 2002, SSR acquired Triton Mining Corporation's remaining 50% interest in Triton , as well as Black Hawk's interests in Alto Valle, giving SSR complete ownership of Triton and Alto Valle. Concurrently, SSR agreed to sell PAS 50% of the shares of Triton and 50% of the shares of Alto Valle directly yielding the current 50/50 joint venture ownership that currently exists between PAS and SSR.

Details of the type, amount, and quantity and results of the exploration and Project development works are described in Section 12 of this Technical Report.

Reconnaissance exploration on the Manantial-Espejo property was first carried out in the 1970s by the Argentinean government.

In 1996, 62 diamond drill holes of the property were completed by Triton totaling 9,653 meters on the Maria Vein. In 1997, an additional forty two (42) core drill holes were completed totaling 6,795 meters and Kilborn Engineering Pacific Ltd. ("Kilborn") was retained to prepare a pre-feasibility study for the construction of an open pit mine and cyanidation mill processing facility to treat and recover silver and gold from the Maria Vein resource.

In 1998, Triton, with SSR as operator, drilled 1,024 meters of HQ-size core in 18 holes, concentrating on the Maria Vein. In 1999, Triton completed some additional prospecting, soil sampling, mapping, and drilled 1,417 meters of HQ-size diamond drill core in 17 holes on targets other than the Maria Vein.

In 2000, a stratigraphic, structural, and quartz texture survey, and several reverse circulation and diamond drill campaigns, were completed in order to sample the newly defined Karina, Unión, and Melissa deposits.

In 2001, a reconnaissance campaign was conducted with the goal of expanding the geological resources of the project and diamond drilling in the Maria, Melissa, and Karina-Unión veins were completed.

A previous mineral resource was reported on the Manantial-Espejo Project on April 6, 2001 by Pincock Allen & Holt, entitled the Manantial-Espejo Technical Report. The

results are summarized below.

> *"The Manantial-Espejo Project contains a Measured and Indicated Resource of 4.144 million tonnes at a grade of 245.0 grams per tonne (g/t) Ag and 4.53 g/t Au with an additional Inferred Mineral Resource of 1.817 million tonnes at a grade of 252.1 g/t Ag and 3.89 g/t Au."*

The mineral resources of the Manantial-Espejo Project were updated numerous times since the April 6, 2001 Pincock Allen & Holt report which complied with NI 43-101 and was considered reliable based on the exploration data available at that date. None of the updates to the resource estimates following the Pincock Allen & Holt report until the date of this Technical Report necessitated filing a material change report.

There has been no known historic mineral production from this Project site.

9 GEOLOGICAL SETTING

Silver and base metal mineralization in the Manantial-Espejo district is spatially and genetically related to a large bimodal igneous province, the Deseado Massif, which is dominated by acid volcanics and their resedimented products of the Chon Aike and La Matilde Formations (Upper Jurassic), and andesites of the Bajo Pobre Formation (Middle Jurassic). The older volcanics form the basement unit and are locally mineralized. The Chon-Aike and La Matilde Formations host mineralization, which occurs at the faulted contacts of volcanic facies as well as at contacts of volcanic stages.

9.1 Regional Geological Setting

The Deseado Massif, a large igneous province in the south of Argentina, is dominated by rhyolitic ignimbrites and minor andesites and basaltic andesites and covers an area of about 60,000 km^2. Manantial-Espejo lies near the southwest end of the Deseado Massif.

The rocks outcropping in the Deseado Massif range from Precambrian to Tertiary. Precambrian basement rocks and Paleozoic (Permian to Triassic) sedimentary rocks do not outcrop on the Manantial-Espejo property and may be covered by the dominant lithologies of the Bajo Pobre, Chon Aike, and La Matilde Formations.

Igneous activity in the area occurred during the Lower Jurassic and continued through the Middle Tertiary. Lower Jurassic formations are present in the NE portion of the Deseado Massif, related to the opening of the Atlantic Ocean. In the Manantial-Espejo District, the Bajo Pobre Formation, primarily andesites and basaltic andesites, represent the Middle Jurassic Volcanism. In contrast, the Chon Aike and La Matilde Formations, essentially rhyolitic to dacitic ignimbrites and resedimented products, correspond to the Middle to Upper Jurassic volcanism.

Succeeding the volcanism, continental sedimentation occurred during Upper Jurassic to Lower Cretaceous, and basalts of Upper Cretaceous age and Lower Tertiary sediments in turn overlie them. Middle to Upper Tertiary rocks, which are present in the Manantial-Espejo District, include basalts and sediments which locally overlay the silicic rocks of the post-mineral stage of the Chon Aike and La Matilde Formations. Sedimentary deposits of Quaternary age, gravels and silts, usually fill small depressions at the southern end of the property which is located in the plains.

9.2 Local & Property Geological Setting

The Manantial-Espejo Project area consists of a volcanic complex (possibly a field dome complex) related to a caldera which collapsed and domed up after a last extrusive episode.

The lithologies of the area consist mostly of sub-aerial volcanic extrusive sequences of Jurassic age. The basement is formed by metamorphic and granitic rocks; however, they are not exposed within the mapped area. Figure 22 is a geologic map of the project area.

10 DEPOSIT TYPES

There are four main deposits that have been investigated and constitute the mineral resources defined in this Technical Report, known as the “P” Maria veins, Karina Unión, Melissa, and Concepcion deposits.

Extensional tectonics during the Jurassic led to normal faulting and the formation of horst and graben structures and block tilting. Two major trends are recognized in landsat image; one trending west-northwest and another, apparently younger, trending northeast. With these two major fracture fabrics, four fracture systems are recognized in the Central Vein Zone set out in Figure 19. The dominant fracture system has a strike of N120-N130. The present veins are the infill of fractures and faults (Ayelen, “P”-Maria veins, Marge-Cindy, Union, and Karina Extension System). In addition, the sanidine-bearing rhyolite dikes have this preferred orientation. The second system comprises vein-filled faults striking N090-N115 (Marta, Melissa, Michelle); and the third one strikes N060-N070 (Concepción, Karina, Sol South and Sol North veins). The last recognized system strikes N030-N040 (Ayelen west, Sandra and NN structures). More than 80% of faults in the area have apparent normal displacement and dip steeply towards SW with small (< 10 m) sinistral/dextral strike slip movement. Minor, but also important, these veins have gentle dips towards the south.

In the Central Vein Zone an inferred horst structure is bounded by the Maria and Karina Faults. The veins and dikes are segmented, having small variations on strike directions and thicknesses.

Circular features are also easily identified on landsat images, particularly one located north of the Central Vein Zone which probably represents the rim of a volcanic center.

The deposit types at Manantial-Espejo District are related to a shallow epithermal low-sulfidation sub-type of mineralization, characterized by the occurrence of different types and styles of silicification (microcrystalline, chalcedonic to opaline silicification) and quartz vein types having characteristic textures (crustiform and colloform banding, replacement of calcite and barite) mostly related to boiling, as well as abundant adularia related to different stages of hydrothermal pulses. Alteration assemblages include propylitization, intermediate argillization, and silicification. The deposits display a vertical and horizontal zonation with silica in the central part changing to argillic alteration that in turn grades to propylitic alteration distal to the veins; silicification also occurs as extensive bodies at surface. The silica bodies are broadly distributed and are interpreted as a paleo-water table, being mostly replacements of aquifer units below and at the surface, by either deep ascending fluid or by steam-heated waters. Nevertheless, it is possible that true sinter deposits punctuated by small hydrothermal eruptions are present.

The exploration of the Project was based on following conventional surface mapping and geochemical characterization followed by drilling of perspective targets. Areas with extensive drilling and defined ore bodies are discussed in the following section. Future exploration programs will be planned on the same basis on previous programs.

The following list provides the basic rock units that have been defined and are routinely logged for the Project:

1. Massive Quartz Vein (>1 meter thick)
2. Thin Quartz Vein (<1 meter thick)
3. Vein Breccia (with typical quartz cement)
4. Fine Tuff [LXT]
5. Volcanic Breccia [EBR]
6. Equigranular Quartz Porphyry [EQR]
7. Andesite/Dacite [BP]
8. Bimodal Quartz Porphyry [BQR,CBR,FBR]
9. Sandstone/Conglomerate [SED]
10. Lithic/Lapilli Tuff [LXT]
11. Volcaniclastic Flow [EBR]
12. Fine Crystal Tuff [UVD]
13. Crystal Ash Tuff [UVD]
14. Rhyolite Dike [SRI]
15. Sandstone/Claystone/Graywacke Sequence [SED]

11 MINERALIZATION

The ore deposits at Manantial-Espejo are predominantly veins with short strike slip and larger down dip displacements. Styles of mineralization include massive quartz veins, vein breccias, sheeted and stockwork veining, and minor dissemination. Quartz is the main infill mineral, displaying distinctive textures indicating the overprinting of hydrothermal events which occurred in the area.

Primary ore minerals present in the quartz veins are argentite/acanthite, silver sulfosalts, electrum, native gold and silver, proustite, freibergite, uytenbogaardita, iodargirite, galena, sphalerite (mainly Fe-poor), pyrite, marcasite and chalcopyrite. The gangue minerals are quartz (dominant), adularia, bladed calcite (replaced by quartz and adularia), and platy barite (replaced by quartz and adularia). Primary mineralization is mainly related to crustiform gray and white banded quartz, late breccias, replacements, and open space infillings (particularly vugs). Six hydrothermal stages are described below.

Secondary mineralization and enrichment comprises limonites (jarosite, goethite), cerussite, pyrolusite, psilomelane and hematitic oxides. The oxidation zone is very variable ranging from surface down to about 200 m locally due to fracture control.

Disseminated mineralization includes microveinlets proximal to main veins and associated with the stockwork veining; bulk dissemination might be found in or proximal to the Laguna Breccia Zone.

Four vein zones have been extensively drilled up to now; all localized in the Central Vein Zone: Maria and P veins, Melissa, Concepción, and Karina-Unión.

Maria vein has a continuous outcrop of 950 m length with a thickness varying from <1 to about 20 m. The strike is N120-N130 and it dips 50-70° to the SW, showing a characteristic pinch and swell geometry. The major hosting lithologies of the vein are BQR (defined in section 10) at footwall and LXT (defined in section 10) at hangingwall. In the hanging wall of the Maria structure, several so-called *P veins* strike sub-parallel to the Maria vein. The thickness of those veins ranges between 0.6 and 18 m, with an average of 4.2 m. They still remain to be explored at their eastern extension. Discrete veins named *P1, P6, P8, P10,* and *PM* have been defined in the resource and reserve. With the exception of the *P8 vein*, the *P veins* are distinctly silver-poor as compared to the Maria vein. The Maria vein is characterized by a number of textures and mineral parageneses representing a depth of formation of up to several hundreds of meters. A fluid inclusion study conducted by Lang Geoscience, Inc. (1999) resulted in a depth of fluid entrapment of high-grade mineralization between 250 and 800 m. The main vein textures are white to gray crustiform quartz, massive white quartz with replaced bladed calcite, massive quartz, colloform banded quartz-adularia and diverse breccia types. In addition, Maria vein shows the largest variety in textures and hydrothermal stages. Studies of cross-cutting relations in outcrops and drill cores in two of the main ore bodies revealed a paragenetic sequence of six hydrothermal stages.

Stage 1 consists of crustiform banded fine-grained quartz, carrying ore minerals, which occurs mostly in the uppermost portion of the Maria vein (about 50-100 m) and reaches just locally 200 m depth below surface.

Stage 2 includes massive white quartz with replaced bladed calcite and massive to vuggy white quartz, with or without minor blades. It is low-grade; however, it shows partial replacement and late infill of vugs by ore minerals from a later stage, which accounts for some ore grade where this paragenetic stage is present.

Stage 3 contains colloform banded quartz and adularia, including generations of amethyst and replaced minerals (calcite or barite) having a needle-like and platy aspect. The abundance of adularia increases downwards, increasing to almost massive adularia below 150 m depth. Also, this stage is low-grade, but it serves as a good host for later primary and secondary mineralization.

Stage 4 can be summarized as a main brecciation stage, although brecciation occurred during all stages. It consists of various breccia types. This stage is generally low-grade, with probably one event carrying high-grade silver ("Ag") mineralization. It is a dark pyrite- and Ag-mineral-rich fine-grained material, occurring as breccia matrix, thin veins, open space infill and replacements. It can be found in levels deeper than 150 m below surface, and is responsible for the highest Ag grades in Maria (locally >10 kg/t, and containing native Ag).

Stage 5 consists of thin (< 1cm) veins and open space infill of base metal sulfides (mainly Fe-poor sphalerite and galena and minor chalcopyrite). These veins cut through the breccias of stage 4.

Stage 6 is represented by post-mineralization chalcedony and supergene alunite, mainly filling open spaces.

The *Maria vein* structure, in the area where modeled for resource and reserve, shows excellent continuity, with little evidence for significant transverse fault offsets. Combined outcrop and drill data show vein continuity over 1,000 meters along strike and over 250 meters along dip. Ore-grade mineralization of the vein is less continuous. Open pit ore-grade zones measure tens to hundreds of meters in longitudinal dimension. Underground ore-grade zones measure tens of meters in longitudinal dimension, with over 100 meters of vertical extent in the Maria West area. Variograms and correlograms indicate mineralization continuity on the order of fifty (50) to one hundred (100) meters for both gold and silver.

The *"P" Maria veins* have less continuity than the Maria vein, both in terms of extent of vein-filled structure and in terms of gold and silver mineralization. Continuity of mineralization is expected to be in the range of tens of meters.

The *Concepción vein system* consists of several sub-parallel veins with a general strike between N060 and N070 and a dip of 45°. The largest vein has a length of about 600 m and a thickness that varies from 1 to 12 m. The outcrop is not continuous, but drill holes demonstrate its existence to a depth of at least 200 m. The main vein at surface occurs at the contact of BQR (defined in section 10) and EQR (defined in section 10) lithologies. The paragenetic sequence of Concepción is similar to the sequence of Maria vein, but some stages and texture are missing (Figure 3-3). In drill cores, mainly massive white to milky quartz with minor blades and adularia can be observed, probably corresponding to stages 2 and 3 of Maria vein. The ore minerals occur as spots and striae (partially crustiform banded) together with more transparent quartz cracking and healing of the white quartz, forming a breccia. This main mineralizing event probably corresponds to

the high-grade event in stage 4 of Maria vein.

The *Concepción main vein* structure, in the area where modeled for resource and reserve, shows excellent continuity, with little evidence for significant transverse fault offsets. Combined outcrop and drill data show vein continuity over 600 meters along strike and over 150 meters along dip. Open pit ore grade zones measure tens to hundreds of meters of strike length and tens of meters along the dip direction.

The *Melissa vein system* strikes N090-N115 having subvertical dips with a recognized length of about 600 m and a depth of about 100 m. The thickness varies between 0.5 and 3 m, with an average of 1.5 m. At the surface, it occurs at the faulted contact of two lithologies - the EQR (defined in section 10) and LXT (defined in section 10) units. This system is distinctively gold bearing, displaying textures and paragenetic sequence similar to the Concepción System.; and it is dominantly brecciated, with strong associated oxidation.

The continuity of the main *Melissa vein* - the North Vein - is defined entirely by drill data, since it is not exposed at the surface. As such, its structural continuity is based on alignment of high grade intercepts and core axial angle information. The structure, as modelled, contains moderate to high grade intercepts continuously for 225 meters along strike and 150 meters along dip. A few small transverse fault offsets on the order of meters are expected to interrupt the structural continuity of the vein.

Karina-Unión is a complex system of sheeted and stockwork veining, with dips from near vertical to 60° to the north. Karina Vein has an east-northeast and Unión Vein west-northwest strike. The two veins have a surface exposure of 850 m length and are recognized to a depth of 150 m. The whole system has a width of over 100 m; the thickest single veins reach approximately 10m. Textures and paragenetic sequences on these veins are also similar to the Concepción vein system. Silver and gold values vary from low to high grade.

Because of the stockwork and sheeted aspect of Karina-Union, continuity of discrete structures has not been established. Rather, continuity of aggregates of veins and veinlets having elevated gold and silver grades has been established. The measure of that continuity is the interpreted 25 to 90 meter variogram and correlogram ranges of gold and silver composite grades within the aggregate zones.

Veins with sparse or no drilling, which are subject to future exploration and which occur within the Central Vein Zone, include the: Marge, Michelle, Sol Veins, Punta Maria, Maria Este, Karina Extension, Cindy, Martha, Ayelen and Maria Oeste. They constitute drill targets and are being evaluated. They have varied lengths, up to several hundred meters and thicknesses exceeding 1 m. They appear to contain mineralization as reported by surficial sampling and limited exploration drilling.

Potential targets outside of the Central Vein Zone are grouped into the West Central Vein Zone targets comprising Nueve Vetas, Mesa, Candelaria and Candelaria Extension, the

East Central Vein Zone including La Gruta and other minor targets, and the North Central Vein Zone containing the Laguna Breccia as a major target. These areas and other exploration targets are shown in Figure 19.

12 EXPLORATION

PAS acquired its interest in Triton in March of 2002. The exploration efforts prior to PAS's ownership are described in section 8 above.

In 2002, Triton collected geochemical samples, completed 2,200 meters of surface trench sampling, reviewed the stored drill core, and completed some camp improvements including building a new core storage warehouse, a communications antenna and sanitary facilities.

Drilling and trenching programs continued into 2003, as did additional reviews of the drill cores, to check and correct stratigraphic nomenclature and to verify that all veins and mineralized stockwork areas had been appropriately sampled. In addition, a 4,472 meter diamond drilling program was completed in the María and Karina-Unión veins focusing on gathering geotechnical stability data. Also, core drilling was completed in a prospective tailings impoundment area to determine fracture and permeability characteristics in addition to placing piezometer wells to measure and monitor changes in the groundwater.

In late 2003, PAS and SSR made a decision to initiate a feasibility study on the Manantial-Espejo property.

Feasibility activities in 2004 included the following:

- Completion of 19,600 meters of infill, extension and exploration drilling. This drilling resulted in a 25% increase in measured and indicated resources. The measured and indicated resource growth was attributable to a combination of infill drilling and the inclusion of the Melissa deposit.
- Environmental baseline studies were essentially completed to allow for timely submittal of Project permit documents.
- Completion of feasibility level flowsheet development metallurgical testing. This testing confirmed previous gold recovery estimates and indicates potentially improved silver recoveries at a coarser primary grind.
- Completion of geologically constrained and diluted resource estimates for the Maria, Karina-Unión, Melissa, and Concepción deposits.
- Completion of feasibility level pit slope stability work.
- Development of methodology for optimization of open pit versus underground mine development. Results indicated project economics would likely be improved by utilizing a combination of underground and open pit mining.

- Completion of 1,100 meters of water exploration drilling. Drilling indicated likely success in pursuing structurally controlled groundwater associated with the mineral deposits.
- Finalization of the purchase of the 6,750 hectare land package directly overlying all reported resources.
- Initiation of community relations activities to ensure community support should a positive production decision be made.
- Completion of a comprehensive project scoping study (the "Scoping Study") in September. Previous to the completion of the feasibility study and this Technical Report, the Scoping Study was completed for the Manantial-Espejo Silver/Gold Project by Hatch Ingenieros y Consultores LTDA out of their office in Santiago, Chile ("The Scoping Study"). Following that, in the first half of 2006, M3 completed work to update the capital and operating cost for the process plant and infrastructure.
- This study was utilized to focus ongoing exploration and engineering optimization studies, and also highlighted potential tax and infrastructure issues for possible Argentine Government participation. Based on scoping work, formal presentations were made to various Provincial and National Government representatives to petition support.

PAS assumed the operator role for the project at the beginning of 2004. During 2004, improvements were made to the base camp including building of an office, enlarging the dormitories, remodeling the sanitary facilities, and improving access roads.

Additional work completed in 2004 included mineral resource modeling by Mr. Robert Wells of EV Technical Services Inc., topography, open pit and underground geotechnical studies with Golder, tailings geotechnical studies with Golder, waste and tailings geochemical studies with Golder and consultant Steve Atkins, Ph.D, metallurgical studies with SGS Lakefield Reasearch Limited, infrastructure analysis, geohydrological studies with GWI, and Induced Polarization geophysical studies (aimed at gathering data for water, geotechnical and mineral exploitation exploration). A total of 176 drill holes totaling 19,854 meters were completed including collection of metallurgical samples and condemnation drilling in the proposed facility areas. In addition, 4 trenches were excavated to obtain bulk samples for metallurgical analysis. Metallurgical investigations were completed to determine the optimum methods for gold and silver recovery, develop a process flowsheet, determine the rock hardness and abrasiveness, determine reagent consumptions, and optimize gravity concentration and cyanidation leach times.

In late 2004, groundwater studies were performed by GWI to determine the existence of suitable groundwater sources to support project operation. Also, Vector S.A. was hired to prepare the Baseline Environmental Report (the completion of which was performed by MWH.) and Hatch Ingenieros Y Consultores LTDA was hired to complete the Scoping Study to determine the potential technical and economical aspects of constructing a precious metals mining and processing operation at the site.

During 2005, Triton completed a second phase of project scoping with the assistance of EV Technical Services Inc., Snowden, and M3 to significantly advance the project feasibility study. Following the completion of scoping evaluations, a final feasibility study was initiated in the third quarter of 2005. This work included:

- Finalizing tailings geotechnical investigations and designs;
- Finalizing metallurgical flow sheet testing and completing variability testing;
- Finalizing Open Pit and Underground Mine designs and schedules;
- Estimating Open Pit and Underground Mine capital and Operating cost estimates;
- Completing plant and infrastructure layout and design work; and
- Completing plant and infrastructure capital and operating cost estimates.

During 2005 Triton also undertook the following activities:

- Completed 20,832 meters (187 holes) of additional diamond core and RC drilling to in-fill selected areas of known resources, investigated potential for economic mineralization outside of the current resource area, continued the water exploration program, and improved the geotechnical database for the feasibility tailings design;
- Initiated recruitment for key development staff positions;
- Opened the main project administrative office in Gobernador Gregores;
- Initiated open dialog with the local community, made public presentations of the project, and solicited public inputs for final consideration in the Project EIS;
- The Environmental Impact Statement was prepared and submitted by MWH Argentina, S.A. to the Provincial Mining authority. This document was supported by numerous geotechnical, geohydrological, and geochemical studies as well as environmental baseline studies; and
- Negotiated and signed a letter of intent with the Santa Cruz Province to jointly develop a high voltage electrical transmission line to supply power to the project from either low cost natural gas generation or via connection to the national grid.

Triton is currently advancing the Manantial-Espejo Project under an agreement with M3, which is providing feasibility study engineering services. Triton and M3 have prepared this Technical Report, with assistance from the various consultants, describing the Manantial-Espejo Project.

The results and investigations and the procedures and parameters relating to the surveys and investigations are described in section 13 - Drilling.

With the exception of five reverse circulation holes in the Maria deposit, only diamond drill samples from the exploration programs have been used to define the resource and reserve for the Manantial-Espejo Project. These holes have been located by surface and down-hole survey with sufficient accuracy for resource and reserve definition. With few exceptions, geologic logs of these drill holes have been recorded with consistent

methodology. Geological contacts, such as vein boundaries, faults, and stratigraphic contacts, and assay intervals have been located with decimeter accuracy by depth in each hole. Assay sampling and analytical procedures have been consistently applied. The drill intercepts of the discrete veins defined in the resource and reserve are spaced at 25 to 50 meters along the veins. These drill data have been found to be of sufficient quantity and quality to define the stated resources and reserves.

Surface trenching and geologic mapping have been utilized to locate diamond drill holes and to locate the near-surface position of veins in the resource and reserve models. The accuracy of these data is sufficient for these uses.

13 DRILLING

Manantial-Espejo Project drilling data was used for metals exploration, resource modeling, geotechnical studies, metallurgical studies, and hydrological exploration/studies. This report section details the procedures used to acquire and verify that drill data procedures characterize the drill database. Triton procedures characterize the drill database.

The resource models for Manantial-Espejo were derived from the following drill data sets:

1. Diamond core drill hole location and orientation;
2. Diamond core assays for gold and silver;
3. Diamond core density determinations; and
4. Diamond core rock type, clay alteration, and core axial angle description by Triton geologists.

To date, three types of drilling have been used on the Manantial-Espejo Project: diamond core, reverse circulation, and wagon drill. Refer to Tables 7 and 8 for tabulation of the counts and total meters drilled for each type of hole, up to Triton hole number T-724.

Table 7 Drill Holes by Type and Operator, Property Wide

Type	Operator	Count	Meters
Diamond Drill	BARRICK	45	6,285
	Triton	698	77,643
	ALL	743	83,928
Reverse Circulation	BARRICK	38	3,260
	Triton	46	3,439
	ALL	84	6,698
Wagon Drill	BARRICK	216	3,242
	Triton	0	0
	ALL	216	3,242
ALL	BARRICK	299	12,786
	Triton	744	81,081
	ALL	1043	93,867

Table 8 Drill Holes by Resource Area and Type

DRILL HOLES BY RESOURCE AREA AND TYPE					
Area	Type	Hole Count	Hole Length	Assay Count	Assay Length
CONCEPCION, 148,700 m^2	Diamond Drill	86	8,476	2,739	3,681
	Reverse Circulation	7	687	304	307
	Wagon Drill	26	413	386	386
	ALL	119	9,576	3,429	4,374
KARINA-UNION, 149,300 m^2	Diamond Drill	88	11,234	7,219	8,947
	Reverse Circulation	2	250	71	71
	Wagon Drill	0	0	0	0
	ALL	90	11,484	7,290	9,018
MARIA, 330,900 m^2	Diamond Drill	311	36,943	12,403	14,903
	Reverse Circulation	28	2,620	1,323	1,332
	Wagon Drill	81	1,276	1,096	1,096
	ALL	420	40,838	14,822	17,331
MELISSA, 57,400 m^2	Diamond Drill	38	4,904	2,036	2,481
	Reverse Circulation	1	165	0	0
	Wagon Drill	0	0	0	0
	ALL	39	5,069	2,036	2,481
ALL, 686,300 m^2	Diamond Drill	523	61,557	24,397	30,011
	Reverse Circulation	38	3,722	1,698	1,710
	Wagon Drill	107	1,689	1,482	1,482
	ALL	668	66,967	27,577	33,203

13.1 Diamond Core Drilling

With the exception of five (5) reverse circulation holes in Maria, the resource model grades are based only upon diamond drilled core samples. Therefore, this Technical Report details only the diamond drilling procedures. Triton diamond drill holes numbered up to T-669 were considered in the resource evaluation.

All Triton core has been HQ diameter (approximately 6cm), with the exception of re-entry into Barrick holes for deepening, for which NQ diameter was used.

Diamond drill holes are located and oriented by geologists in the field to obtain drill spacing in the 25 to 50 meter range on vein, with the closer spacing in the higher grade zones.

Typical drill holes are oriented to cut across the vein zones at an orientation perpendicular to the local strike of the zones and inclined to intercept the vein at as high an angle as is practical. In some cases, uncertainty of vein orientation and greater depths cause veins to be intercepted at less than 45 degree core axial

angles. These cases are handled by resource modeling methods that remove the necessity of correcting for core angle.

Diamond drill holes were used for purposes in addition to exploration and resource definition. Oriented core for geotechnical study was taken from 13 holes totaling 1,389 meters. Piezometers for hydrological study were installed in 26 diamond drill holes totaling 965 meters. Most of the piezometer holes were drilled exclusively for this purpose, though each hole was logged in standard manner and sampled for precious metals if necessary. Metallurgical samples were taken from many of the exploration and resource definition holes. Please see section 18 of this Technical Report for details of the metallurgical study samples.

The last Triton diamond drill hole drilled prior to the resource calculation was T-669. Drill hole exploration on the project is still active, as of December 2005.

Diamond Drill Hole Collar Location

Triton drill holes are initially located by project geologists in the field by GPS (Global Positioning System) or by reference to pre-existing holes or geological features. Initial collar orientation is determined and set by the project geologist also.

All Triton drill hole collar locations have been surveyed by an Argentine land surveyor (Carlos Berasaluce). Coordinates are recorded in the Gauss-Kruger system, which is the national standard for Argentina. When drill hole locations have been questioned because of anomalous geological content, survey checks have been requested and all such collars are confirmed within 2 meters.

Diamond Drill Hole Orientation

Collar and down-hole orientations of Triton diamond drill holes are typically determined by Sperry-Sun single-shot survey tool, which utilizes a magnetic compass to measure down-hole azimuth. Holes with starting inclination shallower than -75 degrees deviate 0.89 degree in azimuth and 0.51 degree in inclination per 50m of drill depth, on average for Sperry-Sun measurements. This is equivalent to an average net deviation of 0.90 meters per 50 meters. Anomalous deviations are checked and corrected, if necessary. In most cases, a Sperry-Sun survey shot is taken in the 7-15 meter depth range. This survey is substituted for the collar survey, because it is deemed to be more reliable than the collar orientation measured by hand-held compass.

Prior to Triton hole number T-332, a Tropari single-shot survey tool was used for down-hole surveys. In cases where this tool has been found to yield anomalous results, the holes have been re-surveyed with the Sperry-Sun tool. In most of

these cases, the Tropari surveys are entirely replaced by the Sperry-Sun surveys in the drill hole database used for resource calculation.

In some cases, shallow holes (less than 50 meters), vertical, and isolated exploration holes were not surveyed with a down-hole tool. The hand-held compass orientation for the collar is used in these cases.

Table 9 details the count of holes in each resource area with tool surveys, up to Triton hole T-669. Some of the holes combine both Sperry-Sun and Tropari surveys, where the Tropari data could not be entirely replaced by the Sperry-Sun determinations. In most cases where holes have no surveys, the hole is not relevant to the definition of ore, the hole is vertical, or the hole is shallow. The low average deviation rate cited above indicates that the unsurveyed holes have a reasonable probability of being straight.

Table 9 Diamond Drill Hole Survey Type

Area	Sperry Sun	Tropari	None	Total
Maria	185	73	59	311
Karina-Unión	77	0	11	88
Melissa	35	3	2	38
Concepción	68	8	15	86
All	365	84	87	523

13.2 Reverse Circulation Drilling

Reverse circulation ("RC") drilling has been used at Manantial-Espejo, largely for precious metals and water resource exploration purposes. Between Barrick and Triton, 84 RC holes totaling 6,698 meters have been drilled property-wide. Of these holes, only five (5) Barrick holes have been retained for use in resource and reserve model estimation. These five occur in areas of sparse diamond drill data in the Maria vein only.

Nineteen (19) RC holes were drilled exclusively for water exploration, water pump testing, and/or piezometer installation. These holes total 1,449 meters.

13.3 Wagon Drill Holes

A wagon drill machine was used for shallow exploration purposes by Barrick. This drill was essentially a wheel-mounted percussion drill, similar to a jack-hammer drill. Maximum depth drilled by this method is 20 meters, typically in angle holes. Samples were of poor quality. Barrick drilled 216 such holes totaling 3,242 meters.

14 SAMPLING METHOD AND APPROACH

Samples of the various deposits were collected from reverse circulation, diamond core, or wagon drill holes defined in Table 8. The diamond core samples are considered to be of a superior quality and representative of the deposits, since the sample collected is more characteristic of the in-place rock being sampled relative to other sampling methods and is therefore considered not to be biased. Therefore, with the exception of 5 reverse circulation holes in Maria, the resource models are based only upon diamond drilled core samples. This report details only the diamond drill sampling, analytical, and descriptive procedures.

The typical core sampling procedure was to half-saw the HQ core after descriptive geological and geotechnical logging with Triton employees. Half of the core was submitted for analysis, while the remaining half was stored on the Manantial-Espejo site. Zones having indications of mineralization, such as precious metal minerals, veining, stockworking, fracturing, sulfidization, and other types of alteration, were sawed and submitted for assay to a commercial laboratory service. In some holes, zones judged to be barren were not sawed or sampled. Vein intercepts from the first few Triton diamond drill holes were sent whole for analysis, without sawing.

For the purposes of resource and reserve calculation, individual assays were arithmetically composited, according to the deposit type and estimation method used. Listings, by estimation domain, of all 2,813 composites used for the resource estimates are contained in Appendix B. In some cases, the composites used for the reserve calculations were different than those used for the resource estimates, because of different dilution assumptions for the reserve. Two basic types of compositing were used: whole-vein composites for the discrete veins and continuous fixed length or bench composites within non-discrete vein domains.

In the case of the Maria, Concepción, and Melissa discrete vein domains, resource modeling composites were averaged over the entire diluted vein width, as defined by intersection with discrete three dimensional vein wire-frame geometry. In cases where wall rock and vein had significant density contrast, composites were weighted by modeled density. Though the estimated vein true widths are known at all points along the wire-frame geometry, the composite listing does not show true widths because quantification of the true width at each vein intercept was not necessary for resource or reserve estimation. The vein wire-frame geometry used for composite definition contains all of the geometric information necessary to define true width, vein dip, shape, and volume. The use of whole-vein composites obviates the need to measure and record the true width of each composite for estimation purposes. The average dip and undiluted true width of each of the discrete veins are as follows:

Maria Main Vein	55°SW	7.7m
Maria P1 Vein	77°SW	4.1m
Maria P6 Vein	87°SW	2.4m
Maria P8 Vein	65°SW	3.1m
Maria P10 Vein	67°SW	1.6m
Maria PM Vein	83°S	1.0m
Melissa North Vein	80°N	2.2m
Melissa South Vein	77°N	1.1m
Concepción Main Vein	45°SE	3.3m
Concepción HG Vein	41°SE	3.1m

In the case of all estimation domains in Karina-Unión, continuous five (5) meter fixed length composites were defined for both resource and reserve calculation purposes, regardless of hole orientation. Though the holes are sampled continuously for the most part, unassayed intervals were assigned zero grade prior to compositing. At domain boundaries and at ends of holes, the composites can be truncated at shorter lengths. The stockwork and sheeted nature of all domains in this deposit, along with variable dips (60-90°N) and strikes (Northeast to Southeast), cause the true structural width of any single composite to be poorly defined or unknown. Most of the drill holes are 45-60 degree angle holes drilled approximately perpendicular to the local strike of the principal veins, so the structures are intersected at moderate to high core axial angles.

In the case of the silver-enriched domain in Maria, five (5) meter bench composites were calculated for both resource and reserve estimation. Composites were calculated with available assayed intervals, excluding any assays of vein intervals, since the primary mode of silver deposition in the zone is along steeply dipping fractures and stockworks. As such, true widths represented by the composites are unknown.

15 SAMPLE PREPARATION, ANALYSES AND SECURITY

Triton employees prepared the various drill samples and sent them to a commercial laboratory, as described below, for sample preparation and analysis. None of the sample preparation and analysis done at the commercial laboratory was conducted by an employee, officer, director or associate of Triton.

Core Sampling, Preparation, and Assay Procedures

Manantial-Espejo drilling, sample handling, assaying, data handling, and resource modeling have been reviewed by Pincock Allen & Holt (April 6, 2001) on behalf of SSR. They found that, up to that time, "Silver Standard's assaying and security procedures have been carried out according to accepted industry standards using accepted practices." With the exception of the introduction of blank standard pulps into the primary lab sample stream, the procedures from drill to assay database have remained largely unchanged since 2001.

The primary assay laboratory is ALS Chemex ("ALS") of Mendoza, which has been

certified by Global Quality, and the second laboratory for replicate checks of approximately 10% of all assays is Acme Analytical Laboratories S.A. of Santiago, which has been certified by the International Certification Network. Both of these labs fulfil the requirements of ISO 9001:2000 standard.. Variable sample intervals are chosen by Triton geologists as the core is logged. Typical sample interval lengths are chosen in the 0.20 to 3.0 meter range, with boundaries chosen at rock type, texture, mineralization, or structural boundaries. The average length of a sample taken in a vein in all drilling to date is 0.92 meters.

The standard sample flow, preparation, analysis, and database entry consists of the following steps:

1. Triton geologists make lithologic logs and mark core for assay sample selection. Core is also photographed.
2. Core is half-sawed at Manantial-Espejo Project site.
3. Each half-sawed sample is placed into a plastic bag with sample number and stapled shut (remaining half core is stored in warehouse facility at Manantial-Espejo Project site).
4. Plastic bags are grouped into larger woven or plastic bags for shipping.
5. Bagged samples are transported by Triton personnel by light truck to Puerto San Julian.
6. Bagged samples are transported by bus or truck to Mendoza, Argentina.
7. ALS receives core, logs it in, and weighs it as received.
8. ALS crushes entire sample to 70% -10 mesh (Tyler Series basis).
9. ALS splits sample with riffle splitter down to 1000 grams, retaining the coarse reject until instructed by Triton as to disposition.
10. ALS pulverizes the entire split to 85% -200 mesh (Tyler Series basis).
11. ALS performs 50 gram fire assay with Atomic Absorption (“AA”) finish for Au.
12. ALS performs 1g four acid digestion with AA finish for Ag.
13. For initial values of >100gpt Ag and/or >10gpt Au, ALS performs a 50 gram fire assay with gravimetric finish for the metal or metals which are over-limit.
14. If Triton calls for it, the sample is analyzed for potential “ore-grade” levels of Cu-Pb-Zn by four acid digestion followed by AA determination of those metals.
15. ALS reports assay by email and by paper copy to Triton, both as spreadsheet and as certificate in Adobe .pdf format.
16. Triton personnel assign the assay data to hole and depth interval, keying on sample number.
17. Incremental assay data are combined into a global drill database for the project.

Assay and other quality control measures are discussed in Section 16 of this report.

Core Logging Procedure

With the exception of five (5) RC holes, five (5) Barrick diamond core holes, and a few intervals of early Triton core which were sent full diameter to the assay lab, all holes used in the resource estimates have been completely logged for geological description by uniform methods. All Barrick diamond drill holes in the resource areas have been logged by Triton as well. Two types of log form are constructed: graphical/verbose with assay sample numbers and interval log form with fixed data fields for computer data entry into a lithology data table for all logged holes. The geological descriptor fields in the interval log form include color, rock type, stockwork level, various alteration types and levels, vein texture, fracture level, and structural features and their core axial angles. Of these log data, only rock type, clay alteration, and core axial angles are used to define the vein solids, estimation domains, and other rock bodies which are used to calculate the resource values for all of the modeled vein systems and their wall rock.

The principal logging field used to define vein and wall rock geometry for resource modeling was the "Primary Rock Type" field or "Rock1". This field contains types which have been found useful for subsurface interpretation. In the following list of "Rock1" logging units, the equivalent surface mapping unit described in the Geologic Setting Section is shown in square brackets. The data field numeric values for each type is the same as the list number below:

1. Massive Quartz Vein (>1 meter thick)
2. Thin Quartz Vein (<1 meter thick)
3. Vein Breccia (with typical quartz cement)
4. Fine Tuff [LXT]
5. Volcanic Breccia [EBR]
6. Equigranular Quartz Porphyry [EQR]
7. Andesite/Dacite [BP]
8. Bimodal Quartz Porphyry [BQR,CBR,FBR]
9. Sandstone/Conglomerate [SED]
10. Lithic/Lapilli Tuff [LXT]
11. Volcaniclastic Flow [EBR]
12. Fine Crystal Tuff [UVD]
13. Crystal Ash Tuff [UVD]
14. Rhyolite Dike [SRI]
15. Sandstone/Claystone/Graywacke Sequence [SED]

A secondary rock type field - "Rock2" - was described to account for intervals which contained mixed rock types. For example, a vein breccia might contain minority wall rock clasts or a wall rock interval might have thin quartz veinlets. This field only contains values where secondary rock types exist.

Qualitatively clay alteration was used in the calculation of dry bulk density for wall rocks in the resource model for Maria. Pyrite level was used in the calculation of pyrite presence/absence coding in the block models for potential use in waste rock classification in Maria, Concepción, and Karina-Unión.

Most of the core in the resource areas has been logged for geotechnical descriptors by uniform methods. Descriptors include recovery, RQD (Rock Quality Designation), fracture count per meter, and discontinuity core axial angles. Most of these data have been keypunched, and the RQD/Recovery data have been compiled into a global data table for Triton diamond drill holes up to T-565. None of these geotechnical data have been audited for accuracy, nor have they been used for resource modeling purposes.

Core Density Determination Procedure

Manantial-Espejo rocks have been found to have significant variation in dry bulk density. A simple bench-top method has been devised to measure the density of all rock types. The method allows many determinations to be made to overcome the variance inherent to the method.

The sample selection and analytical procedure is as follows:

1. Samples are air-dried, in many cases for years under cover.
2. Samples are selected to represent particular rock types in particular areas representing the areas to be mined and their vertical extent.
3. Sample core fragments averaging 21cm in length (minimum 6cm and maximum 37cm) were selected, which means that core fractured into smaller fragments was rejected for analysis. Samples varied from whole core to half-sawn core, with rare selections of quarter-sawn core.
4. Dry weight in grams (dw) of the sample was measured with electronic balance to the nearest gram, with average dry weight of 859 grams.
5. The sample was suspended from a string and slowly dipped in water, such that displaced water reported to a container of known dry tare weight.
6. The water displaced by the dipped sample was weighed to the nearest gram and the volume of the displaced water was converted to volume in cubic centimeters (dv) assuming water density of 1 gm/cc. Such volumes averaged 358 cc.
7. The sample was removed from the water, patted dry to remove surficial water droplets, and weighed wet to the nearest gram (ww).
8. Sample dry bulk density (dbd) was calculated with the following formula: dbd = dw / (dv+ww-dw).

This method assumes that the water absorbed by the sample during immersion (ww-dw) represents the volume of internal sample porosity accessed by the water used for immersion. This increment of absorbed water averaged 6 cc and ranged from 0 to 34 cc.

Since this water was absorbed into the bulk volume of the rock as each sample was immersed, it did not report to the displaced water volume. Since this water in effect became part of the bulk volume during immersion, its volume was reported arithmetically to the bulk displacement volume by adding it to the displaced water volume.

Sample Handling and Security

At the diamond drill rig site, all core is loaded into metal core trays. Triton personnel handle the core from drill site through shipment of half-sawn core to Puerto San Julian, Argentina. All un-sawed and remaining sawn core are stored in warehouse or outdoor enclosures at the Manantial-Espejo Project site for future retrieval and inspection. The storage site is remote, but Triton personnel are present on a daily basis at the core storage site to monitor the security of the core.

The quality control measures are described in Section 16 – Data Verification including the certification statement of the commercial laboratory who conducted the sample preparation and analysis. In conclusion, it is the authors' opinion that the Manantial-Espejo Project's sampling, sample preparation, security, analytical procedures, and quality assurance program meets industry standards.

16 DATA VERIFICATION

Triton performs routine assay data verification by two principal means - primary assay laboratory standard analyses and secondary laboratory replicate check assays. The primary laboratory ALS Chemex performs numerous internal standard determinations and checks.

Historically, no duplicate assays have been systematically performed. Such assays would be derived from coarse preps of standard core samples. On rare occasions, half-sawn core in storage has been quarter-sawn and submitted for assay to check unexpected results.

Analysis of Primary Laboratory Assay Standards

Since April 2005, Triton submits standard pulps with every sample batch for quality control measures, whereby ten (10) percent of all primary lab determinations are for Triton standards, with half being blanks and the other half consisting of equal amounts of two metal-bearing standards.

A blank standard is inserted every 20th sample. This practice was started in November, 2004. Determinations of this sample should yield assay values near or below detection limits for both Au (<=0.005gpt) and Ag (<=0.5gpt). Three cases of significantly elevated gold (>0.10gpt) and three cases of significantly elevated silver (>10gpt) are being investigated, out of a total of 282 determinations since January 2005.

Two gold and silver bearing standards are currently in use for primary lab control samples. Prior to April, 2005, only one standard was used, and it was inserted at a rate of

one every 20th sample. Prior to use of the blanks detailed above, this single standard was inserted at a rate of one every 10th sample. Starting in April 2005, a second standard of medium grade was introduced in addition to the older high grade standard, both being utilized with equal frequency of 1 in 40 in each submittal. Expected values and primary lab results for 2005 are shown in the Table 10. There is no discernable drift in the results with time and significant deviations from the expected value have not occurred.

Table 10 Primary Lab Standard Assays, January-July 2005

Standard Name	Metal	Expected Value	Primary Lab Results				
			Average Value	Standard Deviation	Minimum	Maximum	Number of Assays
High Grade	Ag	385	384.1	8.8	357	410	234
	Au	N.A.	6.52	0.23	5.80	7.11	234
Medium Grade	Ag	173.2	168.7	7.3	1.31	1.47	44
	Au	1.40	1.38	0.04	153	179	44

Analysis of Secondary Laboratory Replicate Check Assays

Since hole T-405 drilled in March, 2004, Triton has submitted ten (10) percent of the pulps prepared by the primary lab, ALS Chemex of Mendoza, to Acme Labs of Santiago for assay as a replicate check. The current protocol for sample selection was designed to avoid excessive checks of very low grade samples and provide complete replicate checks of high grade samples. Sample selection is as follows:

1. The current unchecked group of assays are compiled - usually several thousand samples.
2. All samples with primary assay result greater than or equal to 1000gpt Ag or 10gpt Au are selected for secondary lab check assay.
3. The number of samples (=X) remaining to total 10% of the total primary lab determinations is determined by difference.
4. After removal of high grade samples from the available pool of all assays, the samples with primary assay result greater than or equal to 20gpt Ag or 0.50gpt Au are isolated from the pool of samples.
5. A random selection of X samples from the samples selected in step 4 above is made to complete the 10% check assay sample selection.

After Triton hole T-104 and prior to hole T-405, the selection protocol was a hand-picked selection averaging eight (8) percent of all assays, which emphasized selection of many of the high grade samples. This protocol was used from Triton holes T-105 to T-404. Prior to T-105, check assays were performed on 5% of the samples from T-001 to T-045 concentrating on high grade, and no check assays were performed on samples from holes T-046 to T-104.

Three scatterplots each for gold and silver in different grade ranges showing all 1,650 Triton primary vs. secondary lab checks were made. A selection of 99 Triton core samples in the ore grade range, having check sample variance for gold or silver greater than 25%, have been submitted for data transcription check. If this check confirms the observed variance for an individual sample, that sample will be quarter-sawn and re-submitted for assay.

A small but definite relative bias from primary to secondary lab can be observed in the silver data for grades above 50gpt Ag. For grades in the 50 to 200gpt Ag range, the primary lab averaged 103.1gpt, while the secondary lab averaged 105.3gpt (+2.1%). For grades in the 200 to 1000 gpt Ag range, the primary lab averaged 413.7gpt, with the secondary lab averaged 429.8gpt (+3.9%). For grades in the 1000gpt+ range, the primary lab averaged 2201gpt, while the secondary lab averaged 2268gpt (+3.0%). The reason for this bias has not been resolved. The resource estimates are based entirely upon the primary lab results, so the implication is that the silver resource estimated would be approximately 3% higher, were all the assaying to have been done at the secondary lab. A similar comparison for gold replicate assays indicate mixed results, with the second lab having 3.7% lower average grade for grades in the 0.50 to 10gpt range, and 0.6% higher average grade in the 10gpt+ range. The apparent relative gold bias would tend to cancel the relative silver bias, so the global effect of the relative lab bias is negligible.

Core Drill Hole Location and Orientation Verification

Hole locations which are found to be questionable with respect to surrounding holes or with respect to geological features are checked by land surveyor. Measurable errors in collar survey have not been found.

Since Triton hole T-332, down-hole survey procedures have been standardized to use a Sperry-Sun single-shot tool to characterize collar and down-hole orientation. Extensive efforts have been made to re-enter and use the same tool to re-survey holes which are critical to the resource and reserve. If re-entry was not possible then collar orientations were measured with the Sperry-Sun tool.

Holes or individual down-hole shots which are anomalous are checked by repeated measurement with the Sperry-Sun tool. In every case, when a hole had strong deviation (greater than 1 degrees per 40 meters), re-survey has found that the hole is actually nearly straight. This happens most often with older Tropari measurements. Systematic checks, focusing on the resource areas, of such anomalous surveys have eliminated significant initial deviation measurements.

Core Drill Geological and Geotechnical Digital Log Verification

Since January, 2005, all digital geological log data have been checked for data type and range by Mr. Robert Wells of EV Technical Services Inc.

In logs of all ages, zones with anomalous or unexpected log descriptions have been checked on an as-needed basis during the process of geological interpretation and resource assessment. Some keypunching errors have been found and corrected during this process.

Data analysis and verification evaluations have been performed for the Manantial-Espejo Project by Mr. Robert Wells of EV Technical Services Inc. Mr. Wells is well experienced in mineral resource and reserve model development; however, he is not a certified Qualified Person. As such, PAS's Dr. Michael Steinmann has reviewed and verified the work of Mr. Wells.

17 ADJACENT PROPERTIES

Adjacent properties are not relevant for the review of the Manantial-Espejo Project.

18 MINERAL PROCESSING AND METALLURGICAL TESTING

18.1 General Overview

Metallurgical testing has been completed in phases over an eight year period. The test program consisted of bottle roll leach tests to determine the metallurgical response of the ore types to cyanidation, flotation, gravity concentration, and cyanide leaching of the gravity tails and concentrates, and whole ore cyanidation.

Process testing of ore from the deposits have validated the proposed treatment method and determined key processing parameters.

Representative drill core samples from 76 drillholes were used in metallurgical testing of the ore bodies. A limited amount of grindability tests were completed on near surface trench samples.

Gravity separation and cyanidation testing performed by SGS Lakefield Research Limited produced data was used as the basis for the metallurgical performance target of a commercial operation. Final flowsheet development and optimization testing was conducted on six individual samples and four composites; Karina-Unión and Maria Global, Melissa and Concepción.

Testwork has followed industry accepted practices and is believed to be technically sound and representative for the deposit, although, there can be no guarantee that all mineralogical assemblages have been tested. M3 did not participate in the sample collection or testing.

The following companies have been involved with various aspects of the Manantial-Espejo Project metallurgical evaluations: Lakefield Research Chile S.A., Santiago, Chile ("LRCSA"); Asesorias Y Servicios de Geologia Y Mineralogia Aplicada, Santiago, Chile, ("GMA"), Process Research Associates, Vancouver, British Columbia, Canada ("PRA"); SGS Lakefield Research Limited, Lakefield, Ontario, Canada ("Lakefield" or "MacPherson"); and Pocock Industrial, Inc., Salt Lake City, Utah ("Pocock").

18.2 Types of Testing

The following test data was analyzed by M3 in support of flowsheet development.

- Bottle Roll Whole Ore Cyanidation Leach
- Apparent Bulk Density
- Grinding
- Flotation
- Settling
- Filtration
- Gravity Concentration
- Electrowinning
- Thickening
- Hardness
- Abrasion
- Gravity Concentrate Leach
- Gravity Tail Leach

18.3 Analysis

Testwork was completed to evaluate several processing methods. All available test data was compiled into one database for review. Testwork not representative of the selected process was excluded from this review, i.e., flotation. Testwork included in this review includes 46 gravity separation tests and 127 bottle roll cyanidation tests. Of the 127 bottle roll tests 55 were completed on whole ore samples, 32 on gravity concentrate samples and 40 on gravity tails samples. This analysis assumes that there is no difference in results between open pit and underground ore in a deposit. The test data was arranged by ore deposit (Maria, Karina-Unión, Melissa, and Concepción).

Results of the test work give the following optimum plant operating parameters:

- Grind size P_{80} = 105 µm
- Weight to concentrate= 21%
- Concentrate regrind size P_{80} = 40 µm
- Concentrate leach NaCN concentration => 2-2.5 g/L
- Concentrate leach pH = 10.5-11
- Concentrate leach retention time => 144 hours
- Tails leach NaCN concentration => 1.5-2.0 g/L
- Tails leach pH = 10.5-11
- Tails leach retention time => 76 hours

The reagent consumptions were:

NaCN

- Karina-Unión 0.4-0.5 kg/t ore
- Maria 0.6-0.8 kg/t ore
- Melissa 0.7 kg/t ore
- Concepción 0.6 kg/ t ore

CaO

- Karina-Unión 0.7-0.8 kg/t ore
- Maria 0.6-0.8 kg/t ore
- Melissa 0.5 kg/t ore
- Concepción 0.5 kg/ t ore

Overall average Cyanide and Lime Requirements assumed are:

- Cyanide 1.0 KG/tonne of ore including Detox
- Lime 2.6 KG/tonne of ore including Detox

Based on the results of the test work, the following recoveries can be expected for the Manantial-Espejo ores:

Table 11 Ore Recoveries

	Au	Ag
Mine Head Grades (gpt)	2.82	189
Gravity Recovery (%)	58.3	60.2
Concentrate Leach Extraction (%)	99.2	99.4
Gravity Tail Leach Extraction	88.6	85.3
Overall Extraction (%)	94.8	93.8
Soluble Loss (%)	0.6	0.2
Overall Recovery (%)	94.2	93.6

Note: Assumed tails in barren solution in Merrill-Crowe

19 MINERAL RESOURCE AND MINERAL RESERVE ESTIMATES

The Mineral Resources of the Manantial-Espejo Project were developed by an independent consultant Bob Wells of EV Technical Services Inc. A reserve summary by open pit bench was derived for each pit by Bob Wells by extracting the pit volume out of the appropriate resource block model. Dilution was applied according to the mining method to be used. Ore loss of 0.5% of total ore tonnes was applied to all open pit ore. Losses were applied to the underground ore as well, as specified in the underground mining report by Snowden. A cutoff grade of 130gpt (grams per metric tonne) silver equivalent was applied to obtain the reserve portion of the resource within the open pits to be fed to the milling process. The silver equivalent grade of each block was derived by adding the silver grade to the gold grade multiplied by 82.24. The economic and metallurgical parameters from which this cutoff grade was derived are shown in Table 22. The open pit reserve was derived from the resource block model diluted for open pit mining. The underground reserve was derived from the resource block model diluted for the appropriate underground mining method. Underground reserves were extracted from these models by summarizing within the designed stoping panels. Any wall rock outside of the diluted wireframe or any Inferred Resource occurring within the stope volume was assigned zero grade.

For the underground portion of the reserve, the Measured Mineral Resource was converted to a Probable Mineral Reserve. This is because there has not been an opportunity to confirm the assumptions made for stoping methods by direct observation from underground development. The geotechnical assumptions in particular are very important to the stoping method selection and for the amount of ground support that will be required in the development. Although it is believed that reasonable assumptions have been made based on experience, sound analysis and observation of the diamond drill core, there remains some degree of uncertainty in the stoping and development cost assumptions that would be mitigated by being able to make first hand observation on a larger scale underground operation.

Table 12 Measured, Indicated and Inferred Resource

(Inclusive of All Reserves) Summary by Deposit

		December 2005 Resource		
Deposit	Resource Category	tonnes	Ag	Au
		millions	gpt	gpt
Maria Vein	Measured	2.89	151.6	2.69
	Indicated	2.24	130.3	2.15
	Total Maria M&I	5.13	142.3	2.45
Karina-Unión	Measured	1.72	194.8	1.89
	Indicated	0.75	160.9	1.72
	Total KU M&I	2.48	184.5	1.84
Melissa	Measured	0.10	487.9	7.04
	Indicated	0.15	453.0	6.28
	Total Melissa M&I	0.25	466.9	6.58
Concepción	Measured	0.33	192.4	2.18
	Indicated	0.54	195.7	1.95
	Total Concepción M&I	0.87	194.5	2.03
TOTALS	Measured	5.04	175.6	2.47
	Indicated	3.68	159.2	2.20
	Total M&I	8.73	168.7	2.35
Maria Vein	Inferred	0.73	123.5	1.44
Karina-Unión	Inferred	0.35	137.5	1.42
Melissa	Inferred	0.05	348.4	3.12
Concepción	Inferred	0.20	159.0	1.44
	Total Inferred	1.33	141.8	1.50

Dr. Michael Steinmann, P.Geo., Senior Vice President of Exploration and Geology for PAS is the qualified person responsible for mineral resources estimates at the Manantial-Espejo Project.

The mineral resource model has been developed with the following steps of evaluating economically significant analysis:

- Geological and geostatistical exploratory data analysis.
- Determination of lithologic and estimation domains.

- Determination of mining method and its affect on grade distribution of selectable material.
- Determination of grade capping by estimation domain to limit risks posed by outlier grades.
- Compositing of gold and silver grade data.
- Modeling of spatial distribution of gold and silver grade, estimation confidence, density, lithology, clay alteration, disseminated pyrite content, and topography into three dimensional mineral block models. The models are diluted to match the anticipated, dominant mining methods to be used in each resource area.
- Application of cost, revenue, and metal extraction models to define a silver equivalent cutoff grade of 121 gpt to be applied to co-located gold and silver grades for resource summary, based on a net revenue Au:Ag ratio of 75.657. The cutoff for Melissa was set at 288 gpt silver equivalent grade to reflect the fact that this deposit will most likely be mined exclusively by underground methods.

Table 13 Open Pit Cutoff Parameters for Mine Plan and Reserve

Items		Units	Maria, Karina-Unión, Concepción Open Pit Reserve Cutoff
Au/toz Items	Sales	$/toz	$425.00
	Refining Factor		0.9975
	Smelting	$/toz	$0.74
	Royalty Fraction		0.0143
	Port Tax Credit Fraction		0.0122
	Export Tax Net of Reimbursement		0.03
	Net Sales	$/toz	$409.61
Ag /toz Items	Sales	$/toz	$5.50
	Refining Factor		0.9975
	Smelting	$/toz	$0.24
	Royalty Fraction		0.0143
	Port Tax Credit Fraction		0.0122
	Export Tax Net of Reimbursement		0.03
	Net Sales	$/toz	$5.078
Recovery	Au Net Recovery to Smelter	%	94.11%
	Ag Net Recovery to Smelter	%	92.31%
Ore $/tonne	Overall G&A	$/tonne	$3.53
	ROM rehandle	$/tonne	$0.50
	Milling	$/tonne	$15.48
	Total for Open Pit	$/tonne	$19.51
Cutoff	Ag:Au ratio		82.240
	Open Pit Ag Eq Cutoff Grade	gpt Ag Eq	130

The following tables summarize the open pit and underground reserves for Manantial-Espejo. Mr. Martin Wafforn, P.Eng., Director of Engineering for PAS is the qualified person responsible for mineral reserve estimates at the Manantial-Espejo Project.

Table 14 Maria Reserves by Area

Area	Category	DMT	Ag g/mt	Au g/mt
Maria Open Pit West	Proven	245,437	184.3	1.72
	Probable	42,754	207.5	2.12
	Total Reserves	288,191	187.7	1.78
Maria Open Pit Central	Proven	961,007	112.9	3.21
	Probable	440,516	91.2	3.20
	Total Reserves	1,401,523	106.1	3.21
Maria Open Pit East	Proven	27,109	74.3	5.84
	Probable	40,098	65.6	5.51
	Total Reserves	67,207	69.1	5.64
Maria Open Pit Total	Proven	1,233,553	126.3	2.97
	Probable	523,368	98.7	3.29
	Total Reserves	1,756,921	118.1	3.07
Maria Longhole West Portal	Proven	0	-	-
	Probable	875,878	218.3	3.03
	Total Reserves	875,878	218.3	3.03
Maria Shrinkage West Portal	Proven	0	-	-
	Probable	41,350	151.4	3.58
	Total Reserves	41,350	151.4	3.58
Maria Longhole East Portal	Proven	0	-	-
	Probable	361,114	194.8	2.84
	Total Reserves	361,114	194.8	2.84
Maria Shrinkage East Portal	Proven	0	-	-
	Probable	53,293	35.3	6.90
	Total Reserves	53,293	35.3	6.90
Maria Underground Total	Proven	0	-	-
	Probable	1,331,635	202.5	3.15
	Total Reserves	1,331,635	202.5	3.15
Maria Total	Proven	1,233,553	126.3	2.97
	Probable	1,855,003	173.2	3.19
	Total Reserves	3,088,556	154.5	3.10

Table 15 Melissa Reserves

Area	Category	DMT	Ag g/mt	Au g/mt
Melissa Shrinkage	Proven	0	-	-
	Probable	234,216	442.0	6.26
	Total Reserves	234,216	442.0	6.26

Table 16 Karina-Unión Reserves

Area	Category	DMT	Ag g/mt	Au g/mt
Karina-Unión Open Pit	Proven	1,405,193	214.3	2.00
	Probable	486,467	191.5	1.85
	Total Reserves	1,891,660	208.4	1.96

Table 17 Concepción Reserves

Area	Category	DMT	Ag g/mt	Au g/mt
Concepción Open Pit	Proven	104,366	247.4	2.92
	Probable	123,858	228.2	2.63
	Total Reserves	228,223	237.0	2.76
Concepción Underground	Proven	0	-	-
	Probable	147,974	359.8	3.03
	Total Reserves	147,974	359.8	3.03
Concepción Total	Proven	104,366	247.4	2.92
	Probable	271,832	299.8	2.85
	Total Reserves	376,197	285.3	2.87

Table 18 All Area Reserves

Area	Category	DMT	Ag g/mt	Au g/mt
All Open Pit	Proven	2,743,111	176.0	2.47
	Probable	1,133,693	152.6	2.60
	Total Reserves	3,876,804	169.1	2.51
All Underground	Proven	0	-	-
	Probable	1,713,825	248.8	3.56
	Total Reserves	1,713,825	248.8	3.56
All Total	Proven	2,743,111	176.0	2.47
	Probable	2,847,518	210.5	3.18
	Total Reserves	5,590,630	193.6	2.83

Not all of the 8.73 million tons of measured and indicated resources are mined by current plans. Table 19 provides the distribution of the remaining 2.89 million tons of measured and indicates resources by area. The remaining resource is less than the initial resource discounted for mining due to losses of resource associated with mining (pillars etc.).

Table 19 Manantial-Espejo Remaining Resource

		December 2005 Resource					
Deposit	Resource Category	tonnes millions	Ag gpt	Au gpt	Ag oz millions	Au oz million	AgEq million
Maria Vein	Measured	0.79	106.3	1.09	2.71	0.03	4.82
Maria Vein	Indicated	1.10	112.9	1.09	4.00	0.04	6.92
	total	1.90	110.2	1.09	6.71	0.07	11.73
Karina-	Measured	0.27	111.0	1.51	0.97	0.01	1.96
Karina-	Indicated	0.25	106.6	1.54	0.84	0.01	1.77
	total KU	0.52	109.0	1.52	1.81	0.03	3.73
Melissa	Measured	0.00	260.3	2.69	0.01	0.00	0.02
Melissa	Indicated	0.01	214.0	1.69	0.04	0.00	0.06
	total	0.01	221.6	1.85	0.05	0.00	0.08
Concepción	Measured	0.16	109.9	1.38	0.56	0.01	1.09
Concepción	Indicated	0.31	142.9	1.41	1.45	0.01	2.52
	total	0.47	132.0	1.40	2.01	0.02	3.62
TOTALS	Measured	1.22	108.0	1.22	4.25	0.05	7.89
TOTALS	Indicated	1.67	118.0	1.22	6.33	0.07	11.27
	total M&I	2.89	113.7	1.22	10.58	0.11	19.16
Maria Vein	Inferred	0.63	127.9	1.07	2.60	0.02	4.25
Karina-	Inferred	0.21	119.3	1.45	0.82	0.01	1.57
Melissa	Inferred	0.02	291.0	1.73	0.23	0.00	0.33
Concepción	Inferred	0.17	148.2	1.29	0.82	0.01	1.36
	Total	1.04	133.3	1.20	4.47	0.04	7.51

Dr. Michael Steinmann, P.Geo., Senior Vice President of Exploration & Geology for PAS is the qualified person responsible for mineral resource estimates at the Manantial-Espejo Project.

There are no known issues relating to the environmental, permitting, legal, title, taxation, socio-economic, marketing, political, mining, metallurgical, infrastructure, or other relevant factors that would materially affect the reported resource and reserve estimates reported in this Technical Report.

20 OTHER RELEVANT DATA AND INFORMATION

No other data or information is relevant to make this Technical Report understandable and not misleading, which has not been otherwise described herein.

21 INTERPRETATION AND CONCLUSIONS

The results of the feasibility study for the Manantial-Espejo Project indicate the project is technically feasible (i.e. supports the design engineering basis describing the Manantial-Espejo Project) and is economically viable at conservative silver and gold prices (i.e. based on $6.25/oz. silver and $425/oz. gold, this project has an after tax undiscounted net present value of $40,465,000 and internal rate of return of 7.0% payback in 4.7 years). It will create jobs and economic stimulus to an area that is economically depressed, and can be constructed and operated in an environmentally sound manner. Support from the government would likely ensure this project going forward. To date, the discussions with government agencies have reportedly been constructive.

It is the opinion of Michael Steinmann, author of this Technical Report, that the data contained herein is of sufficient quality, density and reliability to make the conclusions stated.

22 RECOMMENDATIONS

It is the author's recommendation that the Manantial-Espejo Project should be developed pending availability of financing according to the Manantial-Espejo Project development schedule illustrated in Figure 18 while focusing on cost control and schedule opportunities to allow early start-up, taking full advantage of current favorable metal prices and utilizing qualified construction contractors.

The anticipated tentative overall Project schedule is provided in Figure 18 and highlights a 21 month schedule from authorization of project development through design and construction and first production. The SAG and Ball-mill equipment delivery necessary for the processing plant is the critical path for the Manantial-Espejo Project. The project design is based on using ductile iron ring gear for the milling equipment in order to obtain a favorable delivery time and maintain the Figure 18 Project schedule.

The next steps for the project are to initiate the basic engineering and arrange for the project financing.

23 REFERENCES

Reference Titles

1 **A.R. McPherson Corp.,** *Manantial-Espejo 2 Samples Drop Weight Test Report on MEO4GC and MEO4GC-5 Deposit, April 2004*

2 **A.R. McPherson Corp.,** *Proposed Grinding System for the Manantial Communition Circuit, March 11, 2005*

3 **A.R. McPherson.,** *Pan Am Manantial-Espejo SMC Test Report – SMC Test Report on 5 Rock Samples from Deposit, April 2004*

4 **Beattie Consulting Ltd.,** *Metallurgy of Manantial-Espejo Project – Confirmation Test Work*, December 2000

5 **Delkor South America**, *Delkor Comments on Jar Test; Thickener Selection – Jar Settling Tests,* August 10, 2004

6 **Golder Associates Ltd**., *Estudio de Factibilidad Depósito de Relaves,* June 1, 2005

7 **Golder Associates Ltd.**, *Pre-Feasibility Level Evaluation of Tailings - Management Alternatives; Draft Final Report*, September 2004

8 **Golder Associates Ltd**., *Seismic Hazard Assessment,* June 10, 2004

9 **Golder Associates Ltd.**, *Technical Memo – Hydro-Meteorological Analysis*, August 11, 2004

10 **Hatch Ingenieros Y Consultores LTDA**, *Scoping Study for the Manantial-Espejo Silver – Gold Project; Final Report,* August 2004

11 **Kilborn Engineering Pacific**, *Pre-Feasibility Study – Volume 1*, October 1997

12 **M3 Engineering & Techology,** *Feasibility Study for the Manantial-Espejo Argentine Project*, March 2006

13 **MWH Argentina, S.A.,** *Minera Triton Argentina, S.A., Proyecto Manantial-Espejo; Estudio de Impacto Ambiental*, November 2005

14 **MWH Argentina, S.A,** *Gobernador Gregores, Province of Santa Cruz, Argentina, Environmental Feasibility Review Manantial-Espejo Project*, January 2006

15 **Pincock Allen & Holt**, *Manantial-Espejo Property, Technical Report, Silver Standard Resources Inc,* April 6, 2001

16 **Pocock Industrial Inc**., *PAS – Lakefield; Flocculant Screening, Gravity Sedimentation, Pulp, Rheology, Vacuum Filtration Test Report*, November 2004

Reference Titles

17 **Process Research Associates Ltd.,** *PRA Test Report 11, Metallurgical Testing of Maria and K.U. Samples,* August 11, 2004

18 **SGS Lakefield Research Limited**, *An Investigation of Gold/Silver Leaching for a Sample of Manantial/Espejo Gold Project for Triton Mining Corporation,* February 21 1997

19 **SGS Lakefield Research Limited**, *Test Results*, July 1997

20 **SGS Lakefield Research Limited**, *Clima y Meteorología*

21 **SGS Lakefield Research Limited**, *Inventario y Recursos Naturales y Humanos, Tarea 3*

22 **SGS Lakefield Research Limited**, *October 2005 10803-002 Report No. 2; Recovery of Gold and Silver from Project Samples,* October 12, 2005

23 **SGS Lakefield Research Limited**, *Pan American Silver Corp. Interim Report; Process Related Environmental Characterisation Interim Report*, February 16, 2005

24 **SGS Lakefield Research Limited**, *The Recovery of Gold and Silver from Project Samples; LR 10803-001, 002 Report No. 1,* January 31, 2005

25 **SGS Lakefield Research Limited,** *Conception, Four spread sheets; Leaches, Head Assays, Cyanidization, Concentrate,* September 2005

26 **Snowden Mining Industry Consultants Inc, Canada**, *Portion of Feasibility Study - Underground Mining,* December 19, 2005

27 **Snowden Mining Industry Consultants Inc, Canada**, *Manantial-Espejo Feasibility Study; Open Cut Mining Cost Estimation,* June 12, 2005

24 DATE

The information in Technical Report is current as of March 16, 2006.

25 ADDITIONAL REQUIREMENTS FOR TECHNICAL REPORTS ON DEVELOPMENT PROPERTIES AND PRODUCTION PROPERTIES

25.1 Mine Operations

The optimum mine plan approach for the Manantial-Espejo Project consists of a combination of open pit surface and underground mining methods. The surface mining method proposed for Manantial-Espejo ore is conventional open pit mining. In some areas, the open pits will also be used for underground access via in-pit portals. The underground mining operation consists of either long-hole, cut & fill, or shrinkage methods depending on geometry and accessibility.

The open pits will be excavated using five (5) meter high, horizontal benches. Ore and waste will be transported out of the pits by 54-tonne haul trucks via ramps built into the walls of the pits. Truck haulage will continue from the open pit ramp exit points on surface roads leading to waste dumps and the primary crusher ore stockpile. Open pits are to be constructed for portions of the Maria, Karina-Unión, and Concepción deposits. Maria is to be sub-divided into three (3) sub-pits.

A total of five (5) portals and associated declines will be required to access all of the underground mining reserves. Two portals are required for the Maria main structure, Maria West and Maria East, two portals are required for the Concepción area, and one is required for Melissa. At both Melissa and Maria West, a surface excavated box-cut is proposed and required to allow portal development into solid rock. At both the Maria East and Concepción, portals will be developed in the wall of the open pit. Select uncemented rockfill will be used to backfill the Maria Longhole and Concepcion cut and fill stopes for dilution and ground control. All main declines were designed to be 3.7 meters high, measured to top of arch and 3.8 meters wide. A nominal gradient of -15% was used where possible. Reduced gradient sections were designed at all decline intersections. Hydraulic drill jumbos (both one and two boom models), medium capacity (2.7 m^3) load-haul-dump units (LHDs), stoper drills (for rock support) and 15 tonne capacity haulage trucks were assumed for the development of access declines in all areas.

The pit design process was initiated with computer optimized, rampless pit shells. These preliminary designs were used to approximate profit-maximized pit envelopes which balance the value of the recoverable metal against the cost of extraction for that metal. The cost of extraction includes both process plant and mining costs for ore and waste. In the Karina-Unión area, only open pit economics were considered. In the Maria and Concepción areas, both open pit and underground extraction costs were balanced against each other. In Maria and Concepción, the differences between modeled open pit and underground dilution were also taken into account. See Table 20.

The ultimate pit designs presented for Maria and Concepción are smaller than they would be if they were designed with open pit assumptions alone, because the

open pit derived resource block values were reduced by the underground value of each resource block, assuming it was to be mined by underground methods with 90% recovery. Each block in the resource block model was assigned a net value, and the Lerchs-Grossman algorithm was applied to obtain the optimized pits. Design pit slope maximum were input into the algorithm to approximate the overall slope of the ultimate pits with ramps. The resulting computer-optimized pits shells were used as templates for ramped pits which conform to the maximum pit slope design criteria described below.

Bench summaries were used to create a yearly mine plan schedule, assuming that the pits would be mined by extracting entire benches of ore and waste in sequence from top to bottom. The surface mine schedule was coordinated with the underground access and production. The combined production provided for mill feed and the maintenance of a ROM stockpile for production flexibility. The resultant mine plan was the basis for project financial analysis.

The open pit schedule was designed in concert with the underground mining and considers both the desire for higher grade ores in the early years of the mine plan and the need for timely underground access.

The preliminary Maria and Concepción open pit designs were derived by computed optimization where both open pit and underground mining block valuation were allowed to compete. This method relies on an assumption that the underground candidate "ore" occurred in continuous bodies which had "ore" grade above a nominal underground mining cutoff grade. Both areas qualify by this measure. Only Measured and Indicated Resource were allowed to contribute positive value to the optimization. Each resource model block was considered to have two possible values:

1. Open pit value, which was the net of mining the block with open pit costs, processing any potential ore in the block at the milling cost, and sales of the recovered metals. The open pit cutoff grade was determined as the marginal cutoff grade that would at least pay for mill processing of open pit diluted resource. The open-pit cutoff grade was calculated as a silver equivalent grade.
2. Underground mine value, which was the net of mining the ore portion of the block with underground mining costs, processing any potential ore in the block at the milling cost, and sales of the recovered metals. The underground nominal cutoff grade was determined as the marginal cutoff grade that would at least pay for underground mining and mill processing of underground diluted resource. The underground mining costs includes an estimate of vein development costs. In Maria, longhole stopping was assumed to be the only mining method, while in Concepción mechanized cut and fill was assumed to be the mining method.

Because the objective of the optimization was an open pit design, each block was assigned a value which was the open pit value minus the underground value. A conventional Lerchs-Grossman optimization was applied to the resultant block values. The competition in the optimization was between the low mining cost and low cutoff grade of open pit mining against the assumption of zero waste mining along with higher cutoff grade of the underground mining. Table 20 details the assumptions used in the optimizations. Maximum pit slopes were applied to achieve an overall slope less than the recommended inter-ramp angles from the Golder pit slope study, so as to account for the insertion of ramps during mineable pit design.

Metal pricing and costs were modified after the Maria and Concepción pits were designed. However, these pits are reasonably insensitive to changes in metal prices because both types of mining benefited similarly from the price and mining cost changes. Both underground and open pit mining costs increased significantly between the second phase of project scoping and the feasibility study; therefore, the decision was made to keep the designs for the feasibility study equal to the design developed in the second phase of scoping.

The Karina-Unión pit was designed by conventional means, with no plans to extend underground mining below the pit. A conventional Lerchs-Grossman optimization was applied with the assumptions shown in Table 20, which are close to the final outcome of the feasibility study albeit derived in the second phase of project scoping.

The resultant pit designs were used as templates for the mineable pit designs used in the long term mine plan in this study.

Table 20 Open Pit Optimization Assumptions

Items		Units	K-U Pit Optimization	Maria Pit Optimization	Concepcion Pit Optimization
Au/toz Items	Sales	$/toz	$425.00	$375.00	$375.00
	Refining Factor		0.9975	0.99348	0.99348
	Smelting	$/toz	$0.74	$0.73	$0.73
	Royalty Fraction		0.01155	0.01155	0.01155
	Port Tax Credit Fraction		0.0171	0.0171	0.0171
	Export Tax Net of Reimbursement		0.03	0.03	0.03
	Net Sales	$/toz	$412.85	$362.73	$362.73
Ag /toz Items	Sales	$/toz	$5.50	$5.50	$5.50
	Refining Factor		0.9975	0.9975	0.9975
	Smelting	$/toz	$0.24	$0.23	$0.23
	Royalty Fraction		0.01155	0.01155	0.01155
	Port Tax Credit Fraction		0.0171	0.0171	0.0171
	Export Tax Net of Reimbursement		0.03	0.03	0.03
	Net Sales	$/toz	$5.118	$5.123	$5.123
Recovery	Au Net Recovery to Smelter	%	93.61%	93.50%	93.50%
	Ag Net Recovery to Smelter	%	91.81%	92.50%	92.50%
Ore $/tonne	Overall G&A	$/tonne	$3.53	$2.79	$2.79
	ROM rehandle	$/tonne	$0.00	$0.00	$0.00
	Underground Mining Cost	$/tonne	$0.00	$17.06	$29.03
	Milling	$/tonne	$15.48	$15.36	$15.36
	incremental ore handling misc.	$/tonne	$0.00	$0.22	$0.22
	Total for UG	$/tonne	$19.01	$35.43	$47.40
	Total for Open Pit	$/tonne	$19.01	$18.37	$18.37
Cutoff	Ag:Au ratio		82.248	71.567	71.567
	Longhole Nominal Cutoff Grade	gpt Ag Eq		233	
	Shrink Nominal Cutoff Grade	gpt Ag Eq			
	Mech. Cut & Fill Cutoff Grade	gpt Ag Eq			312
	Open Pit Ag Eq Cutoff Grade	gpt Ag Eq	126	121	121
Model	Dilution		Open Pit	Open Pit and UG	Open Pit and UG
Open Pit Mining Cost	per tonne used	$/tonne	$1.40	$1.21	$1.21
Pit Slopes	Azim1/MaxSlope1	deg/deg	0/43	0/50	0/40
	Azim2/MaxSlope2	deg/deg	45/43	90/52	35/40
	Azim3/MaxSlope3	deg/deg	135/51	180/52	70/45
	Azim4/MaxSlope4	deg/deg	225/51	270/52	105/50
	Azim5/MaxSlope5	deg/deg	315/43		140/60
	Azim6/MaxSlope6	deg/deg			180/60
	Azim7/MaxSlope7	deg/deg			215/50
	Azim8/MaxSlope8	deg/deg			250/45
	Azim9/MaxSlope9	deg/deg			285/40
	Azim10/MaxSlope10	deg/deg			32/40
Re-Block	X	count	4	1	2
	Y	count	4	3	3
	Z	count	1	1	1

The ultimate open pit walls are designed in conformance with design specifications provided in a report prepared for Triton titled "Pit Slope Design for Maria and Karina-Unión Veins, Manantial-Espejo Project" (2004) by Golder of Mississauga, Ontario, Canada. This report is based on structural, stratigraphic, and geotechnical data derived from diamond drilling in these two areas. The major rock types found in the recently defined Concepción area are also characterized in Golder's report, and similar design criteria were applied there as well. The most important design criteria were the specified inter-ramp angle maxima allowed in each design sector. Three inter-ramp slope maxima were utilized. The sectors are summarized Table 21

Table 21 Pit Wall Design Criteria

Design Sector Group	Maximum Inter-Ramp Angle (^{o})	Maximum Bench Face Angle (^{o})	Maximum Bench Height (m)	Bench Berm Width (m)
Uppermost 20-30 meters, All Pit Areas	45	65	10	5.5
Maria SE, SW, NW	57*	75*	20	7.5
Maria NE	50	65	20	7.5
Karina-Unión SE, SW	57*	75*	20	7.5
Karina-Unión NE, NW	50	65	20	7.5
Concepción NE, SE, SW	57*	75*	20	7.5
Concepción NW	50	65	20	7.5
*contingent on good local rock mass quality and good blasting control				

The following list describes some open pit design considerations and opportunities for further optimization:

1. The base of pit for Maria West, Maria Central and Concepción, are at a level that does not exactly follow the Lerchs-Grossman optimization. The pits are in general slightly higher in order to obtain a long pit base that will allow better underground interaction for final pillar extraction and development of open pit ramp access.
2. The change in face angle for various sectors is accommodated by altering the angle over a short face length. This may or may not be practical in-situ, and controlling structures may need to be mapped to find the best location for inter angle change.
3. The footwall angle on some pits such as Concepción are shown as a series of single bench step-stairs where the ore is at a flatter angle than the wall angle design allows and ramps are not passing. In these areas it may be better to use the ore footwall contact as a continuous wall.

4. The pits are designed with the upper 20-30m above the lowest point of elevation access with 45° batters and up to 20m benches and 7.5m berms. In some areas, this means that wall angles commence at surface with steep slopes, but commencing at the lowest elevations. This will need field verification.

5. Nine (9) designs were completed for the Maria area, until the final set of three pits was agreed upon. The final set of pits has the highest value whilst placing access in reasonable locations for underground and open pit access. The Central Pit was included in all design iterations. The West Pit was included in 4 iterations, and the Eastern pit was included in 2 iterations. Some further design improvements to the Eastern Pit may be warranted due to the lower number of iterations.

6. Only two (2) designs were completed for Concepción pit. Some further minor improvements to this design may be warranted.

In general, permanent ramps incorporated into the pit walls were designed to be wider and lower in gradient toward the tops of the pits and narrower and higher in gradient toward the bottoms of the pits. The narrower, lower ramps were designed for late-stage extraction at lower tonnage rates utilizing smaller trucks or one-way traffic, while the wider, upper ramps were designed for two-way traffic. Ramp geometry by pit area and elevation range is shown in Table 22.

Table 22 Open Pit Ramp Design Criteria

Pit	Elevation Range	Item	Quantity	Units
Maria West	Below 330 elev	Width, incl berm	13	m
		Slope	12.5	%
	Above 330 elev	Width, incl berm	18	m
		Slope	10	%
Maria Central Central	Below 290 elev	Width, incl berm	13	m
		Slope	12.5	%
	Above 290 elev	Width, incl berm	18	m
		Slope	10	%
Maria East	Below 345 elev	Width, incl berm	13	m
		Slope	12	%
	345-360 elev	Width, incl berm	18-24	m
		Slope	10-13	%
	Above 360 elev	Width, incl berm	15	m
		Slope	10-13	%
Karina-Unión Union	Below 300 elev	Width, incl berm	13	m
		Slope	12-12.5	%
	Above 300 elev	Width, incl berm	18	m
		Slope	10	%
Concepción	Below 350 elev	Width, incl berm	13	m
		Slope	12	%
	Above 350 elev	Width, incl berm	18	m
		Slope	12	%

The following list describes some ramp design considerations and opportunities for further optimization:

1. Gradients of ramps were designed for maximum grade on the inside radius of curvatures. Centerlines and outside curvatures are of lower gradient. Some minor, local deviation from design parameters has altered the designed ramp angles to accommodate local pit geometry.
2. The ramp widths are based on 2.5 times truck width for one way traffic, and 3.5 times truck width for two-way traffic (rounded up to the nearest meter). Ramp widths are inclusive of drains and berms. The truck width was taken as 5.08m for Caterpillar 773D's.
3. Ramp widths are occasionally wider where opportunities exist.
4. All ramps toe onto the last bench in each pit as it is assumed that front end loaders will be used for material loading.
5. There are 3 switchbacks designed. One in Karina-Unión, one in Concepción and one in Maria East.
    a. The Karina-Unión switchback is within 4 benches of the completion of the pit and has minimal volume remaining. However, the optimization also allowed space for a wide ramp and an internal radius of 5.5m. No redesign is suggested.
    b. The Maria East switch back is within 5 benches of the completion of the pit and again will have minimal open pit traffic, however the pit was assigned as an underground portal. It may be prudent to redesign the pit with a straight access heading south east to better optimize underground traffic flow and road maintenance.
    c. The Concepción switchback is within 6 benches of the base of pit. This was placed at the lowest elevation possible whilst maximizing design value. The switch back has no internal curvature, but since the upper abutting ramp is dual flow, this will have to be utilized for one-way access curvature. No redesign is suggested, but flow of traffic control must be accommodated in practice.
6. The ramp angle above the 350 elevation in Concepción could be reduced to 11% without major alteration of the design, cash flows or dump connections. The ramp also has some changes in direction caused by berm connections that could be smoothed in a final design.

The following list describes some inter-pit road design considerations and opportunities for further optimization:

1. The inter-pit roads have not been optimized for cost, although all dump access points are as close as possible to the ramp egress and centrally radiating. There is not much choice in ore direction, although the road from

Karina-Unión could be taken further south near the pit egress to reduce intermediate rise and fall.

2. The inter-pit road widths shown in working documents are demonstrative only. Final road designs are required for construction.
3. Waste dumps were designed for each of the three open pit mining areas. General location and height were designed to minimize waste haulage. The dumps are designed using 37 degree batters, a final maximum inter berm angle of 25 degrees or less, and a swell factor of 1.35. All dumps include 10% or more additional capacity. Waste dump ramp widths were not designed to a fixed standard and are minor to total volume. The yearly schedule diagrams are constructed within 10% accuracy on yearly mined tonnages. The dumps shown in the final year are similarly within 10% of total dump capacity, however these plans are constructed within designs of larger still capacity. The dumps designs could be optimized for additional value and reduced haul lengths. The bottom and middle layers of the Karina-Unión Dump could be reduced toward the pit on the eastern side. This will lead to a larger upper (final) layer. The bottom and middle layers of the Maria Dump could be reduced toward the pit on the south west edge. This will lead to a larger upper (final) layer. The Karina-Unión Pit was reduced in depth by 5m after the initial waste dump design and dump optimization. The height versus area of the Karina-Unión and Maria Dumps were roughly optimized. A second pass optimization should be performed for these prior to commitment of construction. The cost of the height of the Concepción dump versus its area was not optimized. An optimization should be performed for these prior to commitment of construction. General rules of waste dump location in regards to environmental constraints and potential mineralization location were supplied by Triton personnel. No special order of mining or depositing of waste is shown for acid rock drainage (ARD) control.

Bench summaries were used to create a yearly mine plan schedule, assuming that the pits would be mined by extracting entire benches of ore and waste in sequence from top to bottom. While the final long term mine plan will be further optimized, this whole-bench planning was deemed appropriate for the yearly financial planning process applied in this feasibility study. The underground mine plan was combined with the surface mine plans to form an overall mine plan.

The overall sequence developed for the mine plan involves the following steps:

1. Pre-strip of Karina-Unión and Maria East pits and initiate Maria West and Melissa surface portals and ramps. Ore is stockpiled. Waste from Karina-Unión pre-stripping will be used for construction of the bulk fill zones in the tailings impoundment.

2. Initiate mining in Concepción open pit, continue mining in Karina- Unión open pit, and finish Maria East open pit, so the Maria East portal and ramping can be initiated. At the same time start ore mining in the Maria West and Melissa underground to provide high value mill feed in the early years of the project.
3. Continue mining in Concepción and Karina-Unión open pits and continue mining in Maria West and Melissa underground, while starting to strip Maria West and Central pits. Maria East underground starts to come into production.
4. Complete Melissa, Maria West open pit, and Concepción open pit, while underground production in Maria and Concepción keep up the flow of higher grade ore and Maria Central and Karina-Unión continue to decrease strip ratio.
5. Complete all open pit mining in time for pillar removal in Maria Central area before the ore stockpile runs out.

The general bench advance plan for the open pits is displayed in the following Table 23. Bench advance rates are mild, except for the final year for Maria Central.

Table 23 Open Pit Mining Production Plan Bench Advance

TRITON ARGENTINA
Manantial-Espejo Development Project

Open Pit Mining Production Plan Bench

		Year -1	Year	Year	Year	Year	Year	Year	Year	Year	TOTALS
MARIA WEST OPEN	Start				380						
	End				370						
	Num				3						
MARIA CENTRAL OPEN	Start				385	375	365	345	310		
	End				380	370	350	315	235		
	Num				2	2	4	7	16		
MARIA EAST OPEN	Start	380	365								
	End	370	335								
	Num	3	7								
KARINA-UNIÓN OPEN	Start	390	370	350	330	310	290	260			
	End	375	355	335	315	295	265	240			
	Num	4	4	4	4	4	6	5			
CONCEPCIÓN OPEN	Start		390	380	360						
	End		385	365	320						
	Num		2	4	9						

Mining rates assume a two shift per day, 20 working hour per day, seven day per week operation with a single in-pit 6 bcm capacity loader and up to 6 x 50 tonne capacity trucks. A second loader is required for re-handle and back-up.

One of the key features of the mining plan is the use of low, medium, and high grade categories. All underground ore is termed high grade, and the open pit material has two categories - medium and low grade. The open pit medium grade

cutoff is 250gpt AgEq. The stockpile strategy is to take all high grade first to the mill, then medium grade, and then low grade. However, aside from the first year when the mill is not operating, in each other year the high and medium grade end of period inventories are zero or close to zero. Therefore the main build of stockpile capacity is low grade open cut material. The total ore stockpile end of period inventory is shown in Table 28.

Mine plan tonnes and grade by year and work area are shown in Tables 26 for open pit and Table 27 for underground. Stockpile and mill feed are summarized in Table 28.

25.2 Underground Mine Operations

Underground mine areas and the underground mining method is chosen between shrinkage, mechanized cut & fill, or long hole depending largely on the geometry of the deposit. Ore mined from the underground areas will be deposited outside the portals, rehandled, and delivered to the crusher. In addition, small waste dumps will be developed outside the mine portals.

All main declines were designed to be 3.7 m high, measured to top of arch and 3.8 m wide. A nominal gradient of -15% was used where possible. Reduced gradient sections were designed at all decline intersections. Hydraulic drill jumbos (both one and two boom models), medium capacity (2.7 m^3) load-haul-dump units (LHDs), stoper drills (for rock support) and 15 tonne capacity haulage trucks were assumed for the development of access declines in all areas.

Maria is also sub-divided into three underground mine areas and the underground mining method is chosen between shrinkage, mechanized cut & fill, or long hole depending largely on the geometry of the deposit. Ore mined from the underground areas will be deposited outside the portals, rehandled, and delivered to the crusher. In addition, small waste dumps will be developed outside the mine portals.

Table 24 Typical Geometry and Mining Method by Deposit

	Typical Width	Typical Dip	Recommended Mining Method
Melissa	2.8	75	Shrinkage
Maria – Main Structure	7.0	55	Longhole
Maria – P Vein Splays	2.0	75	Shrinkage
Concepción	2.0	45	Mechanised Cut & Fill

At both Melissa and Maria West, a surface excavated box-cut is proposed and required to allow portal development into solid rock. At both Maria East and Concepción, portals will be developed in the wall of the open pit. Both ore and waste will be loaded into diesel haulage trucks by LHD units. Snowden estimated that one 2.7 m^3 capacity LHD and four 15 tonne capacity (EJC 417) diesel haulage trucks are required for this operation. The haulage crew will move

between all mining areas depending on daily production priorities for the operation. The haulage crew will also be responsible for the movement of waste from surface back underground for use as fill in longhole stope and also cut and fill stopes.

In all areas, underground haulage trucks will dump ore and waste onto surface stockpiles near the associated portal. A front end loader (FEL) will be used to load underground ore from the surface stockpile into haulage trucks for transport to the processing plant. The FEL will also be used to load screened waste material into haulage trucks for transport back underground as un-cemented backfill material.

Mr. Luiz Castro of Golder in Toronto, Canada was involved in the refinement of geotechnical parameters since the inception of the Manantial-Espejo Project. In April 2005, Mr. Castro provided the most recent geotechnical analysis for description of the rock mass and for determination of underground stope size and support requirements. His report, *Preliminary Rock Mechanics Study for the Pre-Production Underground Mining at Manantial-Espejo* is referenced in the report prepared by Snowden entitled "*Portion of Feasibility Study – Underground Mining"* dated December 19, 2005.

Each mining area (Maria West, Maria East, Concepción (two), and Melissa) will require a dedicated ventilation system. Ventilation raises will be developed from workings to surface. Main ventilating fans will be installed at the top of the ventilation raises providing fresh air to the workings below. A review and confirmation of the ventilation system was performed by William Smyth. Both William Smyth and Snowden recommend that ventilation raises be used as fresh air sources and that exhaust air flows exit the workings via the main declines.

Each mining area will require water for drilling operations and dust control. Provision was made for surface operations to install and maintain water pipe networks from the process plant to each of the underground portal locations.

Provision was also made in all mining areas for pumping networks from underground to surface to dewater the operations of service and ground water. Analysis by GWI suggests that some ground water will be encountered in every mining area, with the greatest amount in the Maria West and Maria East areas.

Compressors for each area will be installed outside the portal, with piping networks routed into the underground workings.

Table 25 lists the mobile equipment required at Manantial-Espejo for underground operations.

Table 25 Underground Mobile Equipment Purchase Schedule

		Total Units	Year -1	Year 1	Year 2	Year 3	Year 4	Year 5
Axera 5-126	2 boom jumbo	1	1					
Quasar 1F	1 boom jumbo	2	1		1			
Toro 006	LHD - 2.7m3	4	3		1			
Toro 151	LHD - 1.5 m3	3	1				1	1
Quasar 1L	Longhole Drill	1		1				
EJC 417	Haulage Truck	4	4					
Cat 966	Front End Loader	1	1					
Boart s250	Jackleg Drill	16	16					
Boart s250	Stoper Drill	16	16					
	Transport	5	5					
	Man Carrier	2	2					
	Fuel / Lube Truck	1	1					
	UG Grader	1	1					

Based on numerical modeling, the mine ground water inflows, without predrainage, are estimated to average between 19 and 41 L/s (68 to 150 m3/hr) during the mine life, with a best estimate of 26 L/s (94 m^3/hr). An estimated peak inflow of about 41 L/s (148 m^3/hr) is expected to occur at the end of Mining Year 1, coincident with deep development of the Maria East and Maria West vein areas, along with development of the Melissa vein. Lowest inflows occur at the beginning of the mining operation and in the last few years of mining, as ground water storage is depleted, various mining operations (e.g. Melissa, Concepción, and Karina-Unión) are terminated, and when inflows are controlled by the permeability of the country rock surrounding the higher-permeability vein systems.

The sequence of mine development calls for underground development in advance of most open pit operations. At Maria, these underground operations should dewater the overlying pits to be subsequently developed below the former water table. Concepción is relatively shallow and will extend only about six meters below the pre-mining water table. This pit should not experience inflows as a result of drawdown from the Melissa and Maria underground operations. The Karina-Unión Pit is expected to experience inflows, under the best estimate scenario, only in the last 1.5 years of operation. Without pre-drainage, actual inflows to the mine may vary substantially, particularly early in the mine life, as new portions of fault/fracture systems are intersected and storage is drained from them. Given that the most permeable water-bearing fractures and faults are likely directly associated with the vein systems; there will likely be little benefit to grouting underground to reduce mine inflows. However, a program of cover drilling with some grouting may be considered, when intersecting a permeable vein system at depth for the first time, in order to control inflows.

Without discharge to Karina-Unión Pit, it is estimated that flooding of the base of Maria Central Pit will occur within one year of shutdown of pumps in the Maria Underground. Flooding of the base of Karina-Unión Pit is predicted to occur once pumps are shut down at Maria East. Pit lakes are not expected in Maria West Pit or in Concepción Pit, although these pits will be completed slightly below the pre mining water table because there will be some drawdown associated with evaporation from the Maria Central and Karina-Unión Pits. Final (steady-state) pit lake elevation for Maria Central Pit is estimated at between 312 and 323 masl, with a best estimate of 316 masl, resulting in a lake depth of 81 m. Final (steady state) pit lake elevation for Karina- Unión Pit is estimated at between 316 and 324 masl, with a best estimate of 318 masl, resulting in a lake depth of 58 m.

Owing to the lake depths, small amounts of seepage may occur from these pit lakes, hence overall water quality will likely be slightly better than other lakes in the area. Unassisted (without late mine life discharge to Karina-Unión Pit) water table rebound to within one meter of the final pit lake elevations is estimated to require about 200 years after close of mine.

Table 26 Open Pit Mining Production Plan

Pit	Material	Item	units	Year -1	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	TOTALS
Maria West Open Pit	Medium Grade	Ore Mined	DMT				36,444	107,763					144,207
		Ore Silver Grade	gpt				286.2	260.9					267.3
		Ore Gold Grade	gpt				4.10	2.26					2.72
	Low Grade	Ore Mined	DMT				33,620	110,363					143,983
		Ore Silver Grade	gpt				104.0	109.2					108.0
		Ore Gold Grade	gpt				0.81	0.84					0.83
	Total Ore	Ore Mined	DMT				70,064	218,127					288,191
		Ore Silver Grade	gpt				198.8	184.1					187.7
		Ore Gold Grade	gpt				2.52	1.54					1.78
	Waste and Total Tonnes	All Waste	DMT				362,465	1,707,111					2,069,576
		Total Mined	DMT				432,529	1,925,238					2,357,767
		Strip Ratio	w:o				5.2	7.8					7.2
Maria Central Open Pit	Medium Grade	Ore Mined	DMT				67,104	70,100	114,050	155,744	566,539		973,537
		Ore Silver Grade	gpt				175.7	156.6	124.9	125.8	110.3		122.3
		Ore Gold Grade	gpt				3.93	3.99	3.97	3.46	4.11		3.97
	Low Grade	Ore Mined	DMT				17,865	20,177	51,134	136,060	202,750		427,986
		Ore Silver Grade	gpt				85.8	86.5	62.2	74.9	63.7		69.1
		Ore Gold Grade	gpt				1.56	1.45	1.64	1.29	1.58		1.49
	Total Ore	Ore Mined	DMT				84,969	90,276	165,184	291,805	769,289		1,401,523
		Ore Silver Grade	gpt				156.8	140.9	105.5	102.1	98.0		106.1
		Ore Gold Grade	gpt				3.44	3.43	3.25	2.45	3.44		3.21
	Waste and Total Tonnes	All Waste	DMT				626,502	1,433,831	3,614,812	4,448,913	3,149,029		13,273,087
		Total Mined	DMT				711,471	1,524,107	3,779,996	4,740,718	3,918,318		14,674,610
		Strip Ratio	w:o				7.4	15.9	21.9	15.2	4.1		9.5
Maria East Open Pit	Medium Grade	Ore Mined	DMT	13,311	45,344								58,655
		Ore Silver Grade	gpt	48.7	79.9								72.8
		Ore Gold Grade	gpt	5.49	6.44								6.23
	Low Grade	Ore Mined	DMT	3,617	4,935								8,552
		Ore Silver Grade	gpt	46.3	41.7								43.6
		Ore Gold Grade	gpt	1.81	1.54								1.66
	Total Ore	Ore Mined	DMT	16,928	50,279								67,207
		Ore Silver Grade	gpt	48.2	76.2								69.1
		Ore Gold Grade	gpt	4.70	5.96								5.64
	Waste and Total Tonnes	All Waste	DMT	543,385	504,113								1,047,498
		Total Mined	DMT	560,313	554,392								1,114,705
		Strip Ratio	w:o	32.1	10.0								15.6
Karina-Union Open Pit	Medium Grade	Ore Mined	DMT	33,606	161,998	203,558	195,461	167,464	197,243	72,502			1,031,832
		Ore Silver Grade	gpt	243.0	287.3	336.9	293.4	298.8	286.5	198.8			292.3
		Ore Gold Grade	gpt	2.20	2.43	2.68	2.45	2.95	3.50	3.61			2.85
	Low Grade	Ore Mined	DMT	66,690	237,912	180,676	109,213	109,680	117,781	37,876			859,828
		Ore Silver Grade	gpt	109.4	109.5	115.9	112.7	106.3	93.5	88.0			107.7
		Ore Gold Grade	gpt	0.82	0.83	0.80	0.88	0.93	1.09	1.33			0.90
	Total Ore	Ore Mined	DMT	100,296	399,910	384,234	304,674	277,144	315,024	110,377			1,891,660
		Ore Silver Grade	gpt	154.1	181.5	233.0	228.6	222.6	214.4	160.8			208.4
		Ore Gold Grade	gpt	1.28	1.48	1.80	1.89	2.15	2.60	2.83			1.96
	Waste and Total Tonnes	All Waste	DMT	1,844,085	3,840,477	2,968,491	2,153,329	1,383,236	990,620	57,592			13,237,829
		Total Mined	DMT	1,944,381	4,240,387	3,352,725	2,458,003	1,660,380	1,305,644	167,969			15,129,489
		Strip Ratio	w:o	18.4	9.6	7.7	7.1	5.0	3.1	0.5			7.0
Concepcion Open Pit	Medium Grade	Ore Mined	DMT		2,904	23,993	153,081						179,979
		Ore Silver Grade	gpt		267.9	201.5	283.2						272.0
		Ore Gold Grade	gpt		3.41	2.47	3.33						3.22
	Low Grade	Ore Mined	DMT		478	19,401	28,366						48,245
		Ore Silver Grade	gpt		99.1	103.8	108.1						106.3
		Ore Gold Grade	gpt		1.27	1.11	1.03						1.06
	Total Ore	Ore Mined	DMT		3,382	43,394	181,447						228,223
		Ore Silver Grade	gpt		244.1	157.8	255.8						237.0
		Ore Gold Grade	gpt		3.11	1.86	2.97						2.76
	Waste and Total Tonnes	All Waste	DMT		541,599	2,050,708	1,732,828						4,325,135
		Total Mined	DMT		544,981	2,094,102	1,914,275						4,553,358
		Strip Ratio	w:o		160.1	47.3	9.6						19.0
All Open Pits	Medium Grade	Ore Mined	DMT	46,917	210,246	227,552	452,089	345,328	311,293	228,246	566,539		2,388,210
		Ore Silver Grade	gpt	187.8	242.3	322.7	271.9	258.1	227.3	149.0	110.3		214.6
		Ore Gold Grade	gpt	3.13	3.31	2.66	3.10	2.94	3.67	3.51	4.11		3.41
	Low Grade	Ore Mined	DMT	70,307	243,325	200,077	189,065	240,220	168,915	173,936	202,750		1,488,595
		Ore Silver Grade	gpt	106.1	108.1	114.7	107.9	105.9	84.0	77.8	63.7		96.2
		Ore Gold Grade	gpt	0.87	0.84	0.83	0.95	0.94	1.26	1.30	1.58		1.07
	Total Ore	Ore Mined	DMT	117,224	453,572	427,628	641,154	585,548	480,208	402,182	769,289		3,876,805
		Ore Silver Grade	gpt	138.8	170.3	225.4	223.5	195.7	176.9	118.2	98.0		169.1
		Ore Gold Grade	gpt	1.77	1.99	1.80	2.47	2.12	2.82	2.55	3.44		2.51
	Waste and Total Tonnes	All Waste	DMT	2,387,470	4,886,188	5,019,199	4,875,124	4,524,177	4,605,432	4,506,505	3,149,029		33,953,124
		Total Mined	DMT	2,504,694	5,339,760	5,446,827	5,516,278	5,109,725	5,085,640	4,908,687	3,918,318		37,829,929
		Strip Ratio	w:o	20.4	10.8	11.7	7.6	7.7	9.6	11.2	4.1		8.8

Table 27 Underground Mining Production Plan

Area/Type	Item	units	Year -1	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	TOTALS
MARIA WEST LONGHOLE	Ore Mined	DMT	5,237	75,273	114,800	122,329	119,953	126,144	109,046	80,718	122,378	**875,878**
	Ore Silver Grade	gpt	237.1	321.8	278.4	207.2	273.3	262.5	202.4	139.8	75.1	**218.3**
	Ore Gold Grade	gpt	2.95	4.39	3.28	3.02	2.18	2.15	2.99	2.70	3.93	**3.03**
MARIA WEST SHRINK	Ore Mined	DMT				1,000	2,330	3,656		29,904	4,460	**41,350**
	Ore Silver Grade	gpt				110.6	110.6	167.3		151.5	168.5	**151.4**
	Ore Gold Grade	gpt				3.69	3.69	4.32		3.20	5.39	**3.58**
MARIA EAST LONGHOLE	Ore Mined	DMT			7,781	67,933	73,151	72,012	44,158	12,901	83,180	**361,114**
	Ore Silver Grade	gpt			186.3	190.5	327.4	212.8	123.5	162.7	109.6	**194.8**
	Ore Gold Grade	gpt			2.97	3.56	2.77	2.27	3.33	3.16	2.46	**2.84**
MARIA EAST SHRINK	Ore Mined	DMT				446	7,830	23,597	21,420			**53,293**
	Ore Silver Grade	gpt				37.4	34.4	38.7	31.8			**35.3**
	Ore Gold Grade	gpt				6.77	6.36	8.66	5.15			**6.90**
MELISSA SHRINK	Ore Mined	DMT	3,104	59,775	68,288	66,749	36,300					**234,216**
	Ore Silver Grade	gpt	438.5	495.9	502.0	423.0	275.7					**442.0**
	Ore Gold Grade	gpt	7.51	8.81	7.09	4.99	2.73					**6.26**
CONCEPCION CUT AND FILL	Ore Mined	DMT					2,328	43,737	51,850	50,060		**147,974**
	Ore Silver Grade	gpt					481.7	456.3	291.7	340.4		**359.8**
	Ore Gold Grade	gpt					2.97	2.89	2.86	3.32		**3.03**
TOTAL UNDER GROUND	Ore Mined	DMT	8,341	135,048	190,868	258,456	241,892	269,145	226,474	173,583	210,018	**1,713,825**
	Ore Silver Grade	gpt	312.1	398.9	354.6	257.8	282.7	259.8	191.3	201.3	90.8	**248.8**
	Ore Gold Grade	gpt	4.65	6.35	4.63	3.68	2.60	2.90	3.23	3.00	3.38	**3.56**

Table 28 Stockpiling and Mill Feed Plan

Area	Bin	Item	units	Year -1	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	TOTALS
HIGH GRADE STOCKPILE (ALL UNDERGROUND PRODUCTION)	In from Mining	Ore	DMT	8,341	135,048	190,868	258,456	241,892	269,145	226,474	173,583	210,018	**1,713,825**
		Silver Grade	gpt	312.1	398.9	354.6	257.8	282.7	259.8	191.3	201.3	90.8	**248.8**
		Gold Grade	gpt	4.65	6.35	4.63	3.68	2.60	2.90	3.23	3.00	3.38	**3.56**
		Contained Silver	oz	83,687	1,731,838	2,176,041	2,142,563	2,198,563	2,248,159	1,392,950	1,123,615	613,043	**13,710,459**
		Contained Gold	oz	1,246	27,571	28,430	30,570	20,223	25,134	23,532	16,727	22,799	**196,233**
	Out to Mill	Ore	DMT		143,389	190,868	258,456	241,892	269,145	226,474	173,583	210,018	**1,713,825**
		Silver Grade	gpt		393.8	354.6	257.8	282.7	259.8	191.3	201.3	90.8	**248.8**
		Gold Grade	gpt		6.25	4.63	3.68	2.60	2.90	3.23	3.00	3.38	**3.56**
		Contained Silver	oz		1,815,525	2,176,041	2,142,563	2,198,563	2,248,159	1,392,950	1,123,615	613,043	**13,710,459**
		Contained Gold	oz		28,817	28,430	30,570	20,223	25,134	23,532	16,727	22,799	**196,233**
	Ending Inventory	Ore	DMT	8,341									**0**
		Silver Grade	gpt	312.1									**0.0**
		Gold Grade	gpt	4.65									**0.00**
		Contained Silver	oz	83,687									**0**
		Contained Gold	oz	1,246									**0**
MEDIUM GRADE STOCKPILE (OPEN PIT > 250GPT AGEQ)	In from Mining	Ore	DMT	46,917	210,246	227,552	452,089	345,328	311,293	228,246	566,539		**2,388,210**
		Silver Grade	gpt	187.8	242.3	322.7	271.9	258.1	227.3	149.0	110.3		**214.6**
		Gold Grade	gpt	3.13	3.31	2.66	3.10	2.94	3.67	3.51	4.11		**3.41**
		Contained Silver	oz	283,332	1,637,766	2,360,614	3,951,801	2,865,859	2,275,252	1,093,596	2,008,862		**16,477,081**
		Contained Gold	oz	4,728	22,366	19,433	45,092	32,690	36,720	25,728	74,773		**261,529**
	Out to Mill	Ore	DMT		257,164	227,552	452,089	345,328	311,293	228,246	546,417	20,122	**2,388,210**
		Silver Grade	gpt		232.4	322.7	271.9	258.1	227.3	149.0	110.3	110.3	**214.6**
		Gold Grade	gpt		3.28	2.66	3.10	2.94	3.67	3.51	4.11	4.11	**3.41**
		Contained Silver	oz		1,921,098	2,360,614	3,951,801	2,865,859	2,275,252	1,093,596	1,937,513	71,349	**16,477,081**
		Contained Gold	oz		27,093	19,433	45,092	32,690	36,720	25,728	72,117	2,656	**261,529**
	Ending Inventory	Ore	DMT	46,917							20,122		**0**
		Silver Grade	gpt	187.8							110.3		**0.0**
		Gold Grade	gpt	3.13							4.11		**0.00**
		Contained Silver	oz	283,332							71,349		**0**
		Contained Gold	oz	4,728							2,656		**0**
LOW GRADE STOCKPILE (OPEN PIT 130-250GPT AGEQ)	In from Mining	Ore	DMT	70,307	243,325	200,077	189,065	240,220	168,915	173,936	202,750		**1,488,595**
		Silver Grade	gpt	106.1	108.1	114.7	107.9	105.9	84.0	77.8	63.7		**96.2**
		Gold Grade	gpt	0.87	0.84	0.83	0.95	0.94	1.26	1.30	1.58		**1.07**
		Contained Silver	oz	239,883	845,880	738,038	655,836	818,212	456,349	435,034	414,926		**4,604,158**
		Contained Gold	oz	1,960	6,610	5,345	5,804	7,227	6,825	7,259	10,286		**51,316**
	Out to Mill	Ore	DMT		199,447	301,580	9,454	132,781	139,562	265,280		440,490	**1,488,595**
		Silver Grade	gpt		107.7	112.2	108.2	106.9	98.7	91.5		78.7	**96.2**
		Gold Grade	gpt		0.85	0.84	0.95	0.94	1.05	1.14		1.34	**1.07**
		Contained Silver	oz		690,467	1,087,601	32,877	456,478	442,759	780,012		1,113,963	**4,604,158**
		Contained Gold	oz		5,450	8,123	288	4,017	4,733	9,713		18,991	**51,316**
	Ending Inventory	Ore	DMT	70,307	114,185	12,681	192,292	299,731	329,084	237,740	440,490		**0**
		Silver Grade	gpt	106.1	107.7	112.2	108.2	106.9	98.7	91.5	78.7		**78.7**
		Gold Grade	gpt	0.87	0.85	0.84	0.95	0.94	1.05	1.14	1.34		**1.34**
		Contained Silver	oz	239,883	395,296	45,733	668,691	1,030,425	1,044,015	699,037	1,113,963		**0**
		Contained Gold	oz	1,960	3,120	342	5,857	9,067	11,160	8,705	18,991		**0**
MILL FEED	High Grade	Ore	DMT		143,389	190,868	258,456	241,892	269,145	226,474	173,583	210,018	**1,713,825**
		Silver Grade	gpt		393.8	354.6	257.8	282.7	259.8	191.3	201.3	90.8	**248.8**
		Gold Grade	gpt		6.25	4.63	3.68	2.60	2.90	3.23	3.00	3.38	**3.56**
		Contained Silver	oz		1,815,525	2,176,041	2,142,563	2,198,563	2,248,159	1,392,950	1,123,615	613,043	**13,710,459**
		Contained Gold	oz		28,817	28,430	30,570	20,223	25,134	23,532	16,727	22,799	**196,233**
	Medium Grade	Ore	DMT		257,164	227,552	452,089	345,328	311,293	228,246	546,417	20,122	**2,388,210**
		Silver Grade	gpt		232.4	322.7	271.9	258.1	227.3	149.0	110.3	110.3	**214.6**
		Gold Grade	gpt		3.28	2.66	3.10	2.94	3.67	3.51	4.11	4.11	**3.41**
		Contained Silver	oz		1,921,098	2,360,614	3,951,801	2,865,859	2,275,252	1,093,596	1,937,513	71,349	**16,477,081**
		Contained Gold	oz		27,093	19,433	45,092	32,690	36,720	25,728	72,117	2,656	**261,529**
	Low Grade	Ore	DMT		199,447	301,580	9,454	132,781	139,562	265,280		440,490	**1,488,595**
		Silver Grade	gpt		107.7	112.2	108.2	106.9	98.7	91.5		78.7	**96.2**
		Gold Grade	gpt		0.85	0.84	0.95	0.94	1.05	1.14		1.34	**1.07**
		Contained Silver	oz		690,467	1,087,601	32,877	456,478	442,759	780,012		1,113,963	**4,604,158**
		Contained Gold	oz		5,450	8,123	288	4,017	4,733	9,713		18,991	**51,316**
	Total Mill Feed	Ore	DMT		600,000	720,000	720,000	720,000	720,000	720,000	720,000	670,630	**5,590,630**
		Silver Grade	gpt		229.5	243.0	264.7	238.5	214.5	141.1	132.2	83.4	**193.6**
		Gold Grade	gpt		3.18	2.42	3.28	2.46	2.88	2.55	3.84	2.06	**2.83**
		Contained Silver	oz		4,427,090	5,624,256	6,127,241	5,520,900	4,966,169	3,266,558	3,061,128	1,798,355	**34,791,698**
		Contained Gold	oz		61,361	55,986	75,950	56,930	66,586	58,974	88,844	44,446	**509,077**

25.3 Processing Methods

Process Plant

The design of the Manantial-Espejo precious metals recovery plant utilizes conventional process unit operations, including primary jaw crushing, SABC milling circuit (SAG, Ball and pebble crushing), gravity concentration, cyanide leaching, solid-liquid separation using Counter Current Decantation (CCD), silver/gold recovery by Merrill Crowe, air-SO_2 cyanide destruction, and conventional tailings disposal.

The design basis for the ore processing facility is an average of 2,000 dry metric tonnes per day (DTPD) or 720,000 dry metric tonnes per year (DTPY) on an operating basis of 91% availability over 360 days per year. Design ore grade to the process plant is estimated to average 2.83 gpt gold and 193.6 gpt silver. Based on the metallurgical tests and analyses, the design of the plant follows modern practice.

The plant has been designed to be an agitated leach operation. Reground gravity concentrate will be leached by cyanidation in a series of two agitated leach tanks. The leach tanks will provide 96 hours of retention time at elevated cyanide concentrations. Gravity tailings will be leached in a conventional agitation leach circuit and will combine with leached gravity concentrate prior to entering a conventional counter-current decantation (CCD) circuit for gold and silver recovery.

Due to the high silver to gold ratio in the ore, a Merrill-Crowe (zinc precipitation) process will be used to recover precious metals from the CCD solution. The precipitate will be batch smelted to doré, onsite.

Figure 5 provides the general arrangement for the process facilities and Figure 21 shows the process flow sheet.

25.4 Processing Flowsheet

The design of the Manantial-Espejo Project precious metals recovery plant utilizes conventional process unit operations, including primary jaw crushing, SAG milling associated with pebble crushing, Ball milling, gravity concentration, cyanide leaching, solid-liquid separation using CCD, silver/gold recovery by Merrill Crowe, air-SO2 cyanide destruction, and conventional tailings disposal.

Crushing Plant

Run of Mine (ROM) ore will be trucked from the mine to a stockpile ahead of the primary crusher. A front end loader (FEL) will be used to feed the crusher. Any oversize material will be sorted primarily with the FEL. Any blockages at the crusher will be removed with a mobile crane

Primary crushed ore will be withdrawn from the crusher discharge hopper by a variable speed, hydraulic drive crusher discharge conveyor belt feeder. The crusher discharge conveyor belt feeder will feed a conveyor belt that will discharge to the coarse ore bin. Crushing production rate will be monitored by a belt scale mounted on conveyor.

A reclaim feed hopper will be installed over the coarse ore bin feed conveyor. A front end loader can be used to feed finely selected ore to the bin in the event that the primary crusher is down for maintenance or re-handle any bin overflow material stockpiled.

An electric magnet will be installed over the coarse ore feed bin conveyor to pick up tramp metal.

Coarse Ore Bin

Primary crushed ore will be stored in a covered bin to prevent any dust losses from the strong prevailing winds in the area. Ore will be withdrawn from the bin by two coarse ore belt feeders at a rate of 2,000 tpd or 92 tph. In addition, there is an emergency stockpile discharge from the coarse ore bin to the ground.

The feeders will discharge onto a 36" conveyor belt that will discharge to the SAG mill (defined below). The ore reclaim rate will be monitored by a belt scale mounted on conveyor.

Dust control in the Crushing Area will be by a dust suppression system.

Grinding Plant

Ore will be ground to final product size in a combined semi-autogenous (SAG) mill primary grinding circuit and a ball mill secondary grinding circuit.

The SAG mill will operate in closed circuit with a single deck vibrating screen. Screen undersize will flow by gravity through a sampler to the grinding sump. Screen oversize will be transported by two conveyors to the pebble crushing system. Tramp iron and broken media will be removed using a belt magnet ahead of the pebble crusher. The crusher product will be discharged on the SAG feed conveyor. Belt scale will monitor the SAG mill recycle feed rate.

Secondary grinding will be performed in a ball mill operated in closed circuit with hydrocyclones. Ball mill discharge will be combined with SAG mill discharge screen undersize in a grinding sump and will be pumped to hydrocyclones. Combined slurry will be pumped using variable speed horizontal centrifugal slurry pumps (one operating/one standby) to the primary cyclone cluster. Hydrocyclone underflow reports to the ball mill. Hydrocyclone overflow (final grinding circuit product) will flow by gravity across a trash screen to the pre-leach thickener deaeration feed box. Coarse trash screen oversize will be collected in a bin. The hydrocyclones will be arranged so that a portion of the cyclone underflow can be sent to the SAG mill as desired.

A separate, dedicated slurry pump on the gravity circuit feed sump will feed ball mill discharge to a scalping screen ahead of the continuous gravity machine. The coarse gravity concentrate will feed a vertical regrind mill operated in open circuit. The regrind mill will discharge to the regrind mill sump where lime and cyanide will be added. The reground concentrate is then pumped using variable speed horizontal centrifugal slurry pumps (one operating/one standby) to the concentrate leach circuit. The gravity scalping screen oversize will flow to the ball mill feed and the gravity concentrator tails will flow to the grinding sump.

Agitation Leaching Plant

Test work has shown that gold in the ore dissolves rapidly in cyanide solution; however, silver dissolution is slower with significant extraction continuing through 96 hours.

Reground gravity concentrate at approximately 45% solids will be leached by cyanidation in a series of two agitated leach tanks. The leach tanks will provide 96 hours of retention time at elevated cyanide concentrations.

Cyclone overflow as well as product from the concentrate leach circuit will feed the hi-rate pre-leach thickener ahead of conventional leaching. Underflow from the pre-leach thickener will be pumped using variable speed horizontal centrifugal slurry pumps (one operating/one standby) at approximately 45% solids where it will be cyanide leached in a series of four agitated leach tanks at a reduced cyanide concentration relative to the gravity concentrate leach. The leach tanks will provide 76 hours of retention time. Pre-leach thickener overflow, pregnant solution, will flow by gravity to the process water tank where the solution will be distributed to the grinding circuit as makeup water, to the reagent area, and as feed to the hopper clarifier. Solution is processed through the hopper clarifier to remove solids prior to being pumped to the Merrill-Crowe circuit.

A high pressure rotary screw compressor (one operating/one standby) will be provided to aerate the leach pulp to enhance the leaching reaction.

Slurry will advance by gravity from leach tank to leach tank, exiting the last conventional leach tank and reporting by gravity flow to a series of four counter-current-decantation (CCD) thickeners for washing and solid liquid separation. CCD thickener underflow will be advanced by pumping from thickener to thickener, exiting the last tank and reporting to the cyanide recovery thickener . CCD thickener overflow will flow by gravity between CCD thickeners and will be pumped (one operating/one standby) to the pre-leach thickener feed box.

Overflow from the cyanide recovery thickener will be pumped (one operating/one standby) to the final CCD thickener dilution box to be used as wash water. Underflow from the cyanide recovery thickener will be pumped (one operating/one standby) to the tailing detoxification circuit.

The leach tailings are washed to remove solubilized gold and silver prior to disposal. Slurry, at 50% solids, will be advanced by pumping from thickener to thickener, exiting the last tank and reporting to the cyanide recovery thickener ahead of detoxification. Barren solution, used as wash water, is introduced into the final CCD thickener. Solution is advanced counter-current to the solids. Overall washing efficiency in the circuit is >99%.

Lime, cyanide, and air will be added as needed into both agitated leach circuits.

Tailing Detoxification

In the tailing detoxification tanks, weak acid dissociable residual cyanide will be oxidized to the relatively non-toxic form of cyanate using sulfur dioxide and oxygen, with copper sulfate as a catalyst. Milk of lime will also be added to maintain a slurry pH in the range of 8.0 to 8.5. The more stable iron cyanides are removed from solution as an insoluble ferrocyanide precipitate. The cyanide levels are thereby reduced to an acceptable level for discharge to the tailings impoundment.

The detoxification reactors tanks will provide a residence time of approximately two and a half hours.

Slurry discharged from the detoxification circuit will be final plant tailing and will be pumped (one operating/one standby) to a tailings impoundment.

Tailing Storage

Slurry discharged from the detoxification circuit will be final plant tailing and will be pumped to a tailings impoundment through an 8” diameter line. The water reclaim line from the reclaim pond will also be an 8” diameter line such that in the event of a failure of the 8” tailing line, the 8” water reclaim line will be temporarily switched over to pump tailings without disruption to production.

A comprehensive tailings siting evaluation study was undertaken as part of the feasibility preparation. A total of 6 sites were evaluated with a matrix of 11 parameters. Based on this analysis, the selected tailings disposal site was the collapsed caldera of an ancient volcano that has been designated as the North Volcanic Centre (NVC). It is a low risk site because it is completely contained topographically (there is no external drainage). The centre of the caldera is infilled with a relatively impervious siltstone that is, in part, covered with lacustrine and coluvial clayey material.

Based on piezometric readings from 15 standpipe piezometers and one windmill well installed within the base and ridges of the NVC, and areas surrounding the NVC, a strong upward gradient underlies the base of the NVC, and a strong inward gradient exists within the ridges of the NVC. Flowing artesian conditions have been encountered within exploration drill holes within the NVC. Discharge from the basin is strictly via evapotranspiration, largely from the lower slopes and lower areas of the floor of the NVC, which creates a “hydraulic trap”, or

hydraulic containment. The extent of this trap is estimated at between 6 and 10 m of hydraulic head, based on current piezometric data.

The tailings disposal facility is completely founded on the relatively impervious siltstone that is partly covered with lacustrine clays. This siltstone, which occurs within the NVC, has an estimated maximum thickness of at least 40 m and thins at the edges. A total of nine hydraulic tests were carried out within the North Volcanic Centre siltstone at two wells and on two open boreholes, both within the upper fractured portions and deeper within the lower, less disturbed siltstone, with a slight bias in favor of the fractured siltstone. The geometric mean horizontal hydraulic conductivity was 3×10^{-8} m/s, considered to be of low permeability. As is typical for horizontally-layered formations, vertical hydraulic conductivity is expected to be 2 to 10 times less. The facility has three other elements; the tailings storage area, a reclaim pond and a ditch around the perimeter of the tailings area to collect runoff from the surrounding high ground and also seepage from the tailings.

Tailings water will be pumped or will seep through the main dam into the reclaim pond. The main dam is designed as a leaky dam. The reclaim pond will also collect water from the perimeter ditch. Any water that accumulates in the external pond will also be pumped to the reclaim pond. The water in the reclaim pond will be re-circulated to the mill.

Based on flow model analyses for the basin area where the tailings is stored, it will be necessary to provide an annualized make-up water volume of at least 550,000 m^3 to support the mill. The dam heights necessary to provide for emergency water storage in the main dam and water recovery areas should be sized to support the probable maximum precipitation within the lagoons at their maximum design levels.

Closure considerations include dust control and consideration of progressive closing practices before the end of the operation. A practical method to manage excess dust is to cover the tailings with heavy non mineralized rock from the mine.

Merrill-Crowe -Refinery

Gold and silver will be recovered from pregnant solution by zinc precipitation of metal ions using zinc dust and thereafter smelting the collected silver and gold precipitate into doré bars.

The process of recovering silver and gold by the Merrill-Crowe process includes:

- clarification and filtering of pregnant solution to remove suspended solids;
- deaeration of pregnant solution to reduce dissolved oxygen;
- precipitation of gold and silver metal by addition of zinc dust;
- filtering and drying of precipitate; and

- smelting the precious metal precipitate in a crucible furnace to produce doré bars.

Pregnant solution from the clarifier filter feed tank (will be pumped using a horizontal centrifugal pump (one operating/one standby) to one of two self-cleaning pressure leaf clarifier filters (one operating/one standby). The clarifier filter is a leaf type. The operating filter is pre-coated using diatomaceous earth (DE) as a filter aid and in addition, has a continuous body feed addition of DE to assist filtering as needed. For these purposes, two pumps with a common tank will be provided with the filter units. The pre-coat pump will be a horizontal centrifugal pump. The body feed pump will be a peristaltic type pump which will receive feed from the agitated DE tank and then pump filter aid into the filter feed stream. Pressure for filter operations will be provided by the clarifier filter feed pump. Filtrate, clarified solution, will discharge directly to the deaerator tower.

Clarified solution is passed through the deaerator tower to remove dissolved oxygen to less than 0.5 ppm prior to zinc dust addition. The deaerator tower will be connected through a barometric seal to a vacuum pump.

The clarified, deaerated, pregnant solution will be withdrawn from the bottom of the deaerator tower by a single-stage, vertical, in-line, centrifugal pump, submerged in water to prevent re-entry of air through the pump gland. The pump will discharge to the precipitation filter presses (one operating/one standby). An emulsion of zinc dust and pregnant solution will be added to the pregnant solution at the pump discharge to precipitate the silver and gold.

Zinc dust will be hand loaded into a zinc feeder hopper from as-delivered 45-kg capacity pails, and will discharge via a feeder into a mixing cone which will emulsify the zinc dust with pregnant solution. DE will be hand loaded into the zinc feed hopper as body feed to extend the filter cycle. The mixing cone will be continuously supplied with pregnant solution to prevent air from entering the suction of the progressing cavity type, zinc injection pump. The slurry is then pumped to one of two (one operating and one standby) plate-and-frame filter presses, where the precipitated precious metals are collected. The plate and frame press is manually opened and cleaned with precipitate being collected in carts.

Barren solution (filtrate) exiting the Merrill-Crowe circuit will flow into a barren solution tank. Barren solution will be distributed to CCD as wash water, to the cyanide mix tank, the clarifier filter as backwash, as flocculant dilution, and as gland water.

Refinery

Zinc precipitate is placed in drying ovens prior to fluxing. Dry filter cake will be mixed with fluxing materials and charged to an electric crucible furnace. The melted charge will be poured into conical molds. Doré, gold, and silver will sink to the bottom of the mold, and slag glass containing fused fluxes and impurities,

will float to the top of the mold. Doré will be sampled for gold content using vacuum tube samples during melting or bar drilling after cooling.

After cooling and solidifying, the molds will be dumped and the slag will be knocked off the Doré buttons by hand.

Buttons will be cleaned under a water stream using a needle gun, weighed and stamped with an I.D. number and weight. Doré buttons weighing approximately 20 to 30 kilograms will be the final product of the operation and will be stored in a safe until shipment.

Slag will be crushed and screened to recover high grade prills, which will be returned to the melting furnace. Remaining slag will be collected for proper disposal.

Fumes from the melting furnace will be collected through ductwork and cleaned in a bag house dust collector system before discharging to atmosphere.

Water System

The average mine make-up water requirement is about 15 L/s (54 m^3/hr or about 1300 m^3/day), however, this will vary somewhat depending on the season and special requirements, such as at plant startup. Based on a 10-year mine life, the total water requirement is estimated at about 4.7 million cubic meters (Mm^3), or roughly 4% of the estimated ground water resources practically accessible. With annual recharge and regional throughflow estimated at about 35,000 m^3/year, it is estimated that about 3.2 Mm^3 will be "mined". Most of this water should be replaced within the first 25 years through increased recharge, reduced evaporation from lakes and basins, although full water table recovery around the Maria Central and Karina- Union Pits will require substantially longer.

Fresh water for the Manantial-Espejo Project will be supplied from three to eight mine dewatering wells. Water from the wells will be pumped to a Fresh/Fire water tank located at slight elevation relative to the process area. Water will be distributed from this tank for use at the site.

Potable water for the plant area will be supplied from one fresh water well. A treatment system, chlorination, will be provided to treat fresh water for potable water consumption. The well water will be treated and then stored in a storage tank. Potable water will be pumped from the potable water tank to plant use points.

Reclaim water from the tailings pond will be used as wash water at the cyanide recovery thickener. Two vertical turbine pumps will pump reclaim water from the tailings pond to the cyanide recovery thickener feed box.

Reagents

Reagents requiring handling, mixing, and distribution system include:

- Sodium Cyanide
- Pebble Lime
- Antiscalant
- Diatomaceous Earth
- Flocculant
- Zinc Dust
- Sulfur/Sulfur Dioxide
- Copper Sulfate

Sodium Cyanide (NaCN)

Sodium cyanide solution will be added to the agitated leach circuits.

Pebble Lime (CaO)

Lime will be added to the grinding mill, the concentrate leach circuit, to the conventional leach circuit, and to the detoxification circuit to maintain pH.

Lime will be delivered in bulk trucks equipped with pneumatic unloading systems to discharge to a 100 ton capacity, cone bottom lime storage bin. The bin will be equipped with a bin vent type dust collector.

Pebbled quick lime will be fed to a slaking system via a bin activator and an auger, slaked/degritted, with milk of lime added to the agitated leach circuits and the cyanide destruction circuit.

Antiscalant

Antiscalant will be added at the point of use to various clear water pump suctions using metering pumps directly coupled to suppliers tote boxes.

Diatomaceous Earth (DE)

DE will be added to the clarifier filters and the precipitation filters to aid in filtering.

Flocculant

Flocculant will be added to the preleach thickener, the hopper clarifier, stage added to the CCD thickeners as needed, and to the cyanide recovery thickener.

Zinc Dust

Zinc dust will be added to the clarified, deaerated, pregnant leach solution at the Merrill-Crowe plant.

Cyanide Destruction Reagents

Cyanide destruction in the mill tailings slurry stream will occur using sulfur dioxide made from raw sulfur and oxygen, with copper sulfate as a catalyst.

Copper Sulfate ($CuSO_4$)

Copper Sulfate will be mixed in a mix tank, transferred to a day tank and will be added in liquid form to the tailings detoxification tanks.

Sulfur/Sulfur Dioxide (SO_2)

Raw sulfur will be fed to a sulfur-burning SO_2 plant that will produce SO_2 gas which will be added to the tailings detoxification tanks. The sulfur-burning plant will be sized to burn ~62.5 kg/hr (137.5 lb/hr) of sulfur to produce 125 kg/hr (275 lb/hr) of SO_2 (gas at 15%).

Flux

Flux will be added during the smelting stage to remove contaminants from the precipitate.

Compressed Air

An air compressor and air receiver will be installed for operation and maintenance at the crushing area. Plant air and instrument air will be installed for the processing plant.

25.5 Infrastructure & Ancillaries

During the construction phase, contractors may be responsible for construction water, power, lighting, security services and telephone until those services become available onsite. The plant construction phase is expected to take about two years and will peak at about 800 workers. A majority of the construction workers are employed by various construction contractors. The majority of the contractors' workforce will be housed at a temporary camp erected at the site. Figure 4 is a general arrangement drawing of the planned facilities.

Current planning designates Gobernador Gregores as the primary support community for the Manantial-Espejo Project. Relations with the current Mayor and people of Gobernador Gregores are considered to be excellent and they have strongly supported the efforts to develop the Project. Triton has made an allowance for infrastructure and housing development in Gobernador Gregores to support operational workforce housing needs. Triton is working with the local Government to define what the infrastructure and housing needs are and how these developments will be financed and constructed.

Triton has reached agreement with the Provincial and National Government to share in the cost of construction of a new approximately 200 kilometer 132 kV overhead transmission line and associated components to supply power to the

Manantial-Espejo Project and the community of Gobernador Gregores. The provincial Government will manage the installation of the powerline. This powerline will be fed from an interim natural gas generation facility located 160 kilometers east of the Manantial-Espejo Project near the town of San Julian. It is anticipated a connection to the National power grid will be completed in late 2008 and the interim natural gas generation facility will be decommissioned.

Triton completed 19 exploratory drill holes to define the water supply and mine dewatering requirements for the Manantial-Espejo Project of which long term testing was completed on 3 of the mine dewatering wells. The results of this work indicate that an average of 31 L/sec of water will be produced during mine dewatering which is more than double the 15 L/sec water make-up requirement for the operation. The mine dewatering systems will provide an adequate supply for the Manantial-Espejo Project and excess water can be discharged to several ponds that exist on the property.

The following building ancillaries are anticipated:

Table 29 Building Ancillaries

Tag Number	Building	Description
100 - BD - 02	Electrical Building - Primary Crushing	Pre-Engineered, 4.0m x 8.0m Electrical Building
100 - BD - 03	Electrical Building - Coarse Ore Bin	Pre-Engineered, 4.0m x 8.0m
300 - BD - 01	Grinding Mill Building	28.0m x 34.0m - Steel Building
300 - BD - 02	Electrical Building - Grinding Area	8.0m x 16.0m - Steel Building
300 - BD - 03	Grinding Mill Control Room	5.5m x 6.0m Steel Structure
400 - BD - 01	Leach Area Electrical Building	6.0m x 12.0m Pre-Engineered Steel
600 - BD - 01	Refinery Building	24.0m x 36.5m
600 - BD - 02	Merrill-Crowe/Refinery Electrical Building	6.0m x 12m
800 - BD - 01	Reagent Building	Pre-Engineered Steel - 240 m^2
950 - BD - 01	Administration/Guard Building	650 m^2
950 - BD - 02	Powder Magazine	100 m^2
950 - BD - 03	Detonator Storage Building	16 m^2
950 - BD - 04	Cafeteria Building	325 m^2
950 - BD - 05	Laboratory Building	460 m^2
950 - BD - 08	Truck Shop/Warehouse Building	1000 m^2
950 - BD - 09	Mine Change house	600 m^2
950 - BD - 10	Truck Wash	

Electrical power to the project site will be supplied from a proposed new 132 kV overhead transmission line, tap/step down substation, 132 to 33 kV, and 33 kV overhead distribution line provided by the local Argentinean government electric power utility organization. The installation cost of this power line will be shared three ways between Triton, the Provincial Government, and the National Government. The provincial Government will manage the installation of the

power line. Negotiations are underway to finalize the agreement for the erection of this power line that benefits the Gobernador community as well as the mine.

The new 132 kV overhead transmission line is to be routed along existing Route 25 highway which runs East and West between the existing towns of San Julian and Gregores approximately 5 km just south of the project mine site. This new 132 kV transmission line will be connected into existing substations located at each town sites, namely San Julian to the East and Gregores to the West. The estimated distance of the 132 kV section from San Julian to the tap/step down substation is 155 km, and the section from tap/step down substation to Gregores is 37 km, for a total 132 kV transmission line length of 192 km between the two existing town sites.

A new tap/step down substation will be provided along the 132 kV transmission line at the point at which the new mine road tees towards the mine site and intersects existing Route 25 highway. The tap/step down substation will transform the voltage from 132 kV down to a 33 kV distribution voltage. A ring bus at 132 kV with three (3) gas insulated circuit breakers, isolation air disconnect switches, a single 132 to 33 kV step down transformer, overcurrent protective relaying and 35 kV switchgear lineup in electrical building are to be provided.

A new 33 kV overhead distribution line is to be routed from the tap/step down substation at the intersection of the mine access road and Route 25 highway, due North to the mine's main substation along the West side of the mine access road for approximately 5 km to the mine's main substation.

The estimated connected load for this project is 10.3 mega watts (MW) as determined from the project's preliminary process equipment list.

Project Power Distribution

An Electrical Load Analysis has been performed based on the project equipment list and summarized by mine areas as follows:

Table 30 Electrical Load Analysis

Mine Area Description	Estimated Connected Load (kW)	Comments
Area 050 - Mining	3,186.0	Includes four (4) Mine Portals and Dewatering pumping.
Area 100 – Primary Crushing	333.0	
Area 300 – Grinding, Classification, Recycle	2,981.0	
Area 400 – Cyanidation & Washing	984.0	
Area 500 – Tails	352.0	
Area 600 – Merrill-Crowe & Refinery	662.0	
Area 750 – Tailings Impoundment	120.0	
Area 800 – Reagents	249.0	
Area 900 – General Site	526.0	
Area 950 – Infrastructure	852.0	
Total Electrical Load	10,247.0	

Allowances have been included for the ancillary buildings and services as well as for plant lighting and heating and ventilating loads.

The project electrical single line diagram has been developed to reflect the area electrical loads, and their physical locations, based on information resulting from the equipment list and associated load analysis.

Electrical power will be distributed to the main mine substation and mine pit/tailings area at 33 kV overhead distribution line. Revenue metering will be performed, using local electric utility company instruments, at 33 kV within the mine main substation. The main mine substation and mine pit/tailings unit substations will transformer 33 kV down to 3.3 kV. Local at the main process load areas, 3.3 kV and associated switchgear will distribute power in a combination of overhead lines or in underground ductbank configurations. A second voltage transformation will be made at local process area electrical rooms or outdoor unit substations to 220/380V, 3 phase, 4 wire distribution using motor control centers and small outdoor oil filled transformers.

Project Standby Power Distribution

At the mine's main substation, provisions for temporary connections to portable standby diesel generator(s) will be included in the design and switchgear lineup used to provide limited standby electrical power to process critical loads. The generator connection interface can be made directly at 3.3 kV switchgear using a

manual transfer scheme, or at the 380 Volt level connected via a manual transfer switch and dedicated motor control center to which the critical loads will be served from. The exact configuration will be determined during design once the critical loads are identified and located.

Telecommunications

At the present time there is no land line or cellular telephone coverage in the area of the mine site. Based on the remote mine site location, radio or satellite telecommunication technology using tower type repeater stations will have to be considered. Detailed options to provide voice and data service for the project were not examined, but have been included as allowances in the project's capital cost estimate.

The project plan includes a radio system for on site operations and maintenance communications.

Water

Water for the Manantial-Espejo Project will be supplied from underground mine water and surface mine dewatering wells. Water from the wells will be pumped to a Fresh/Fire water tank located at slight elevation relative to the process area. Water will be pumped and distributed from this tank for use at the site.

Dewatering Well	Pump	Service
DW-01	900-PP-39	$45m^3$ / hr at 30m TDH
DW-06	900-PP-36	$45m^3$ / hr at 30m TDH
DW-07	900-PP-37	$45m^3$ / hr at 30m TDH

Tailings will flow to the tailings pond in an 8" diameter line. The water reclaim line is also an 8" diameter line. In the event of a failure of the 8" tailing line, the second 8" line (normally used for water reclaim) will be pressed into service for tailings. During this emergency condition, water will temporarily not be reclaimed from tailings.

25.6 Markets

The Manantial-Espejo processing facility will produce high quality (greater than 98%) silver-gold doré which is readily marketable. The doré sales will be completed under a contract, or series of contracts, which will be negotiated before the commissioning of the plant is completed. PAS is currently marketing a very similar doré product from the La Colorada mine located in Zacatecas, Mexico. The terms of these agreements specify the methods for shipping and handling, weighing, sampling, payable returns, and refining charges.

25.7 Environmental and Permitting Considerations

MWH Argentina, S.A. ("MWH"), performed an Environmental Impact Study ("EIS") for the Manantial-Espejo Project as required under the laws of the Province of Santa Cruz and the Argentine Republic. The study includes all the items required under Argentine legislation, including a detailed report of the base line and the consulting steps taken with regard to the community and the authorities.

The EIS identifies the main environmental impacts, both positive and negative, arising from the project in such environment, and lists mitigation steps that are necessary in an Environmental Care and Management Plan, which also includes a full Environmental Monitoring and Social Program.

The EIS performed for the Manantial-Espejo Project did not identify any severe environmental impacts that could compromise the project's feasibility from the environmental point of view.

The identified environmental impacts are in almost all cases low to moderate and can be reasonably mitigated by the Environmental Care and Management Plan attached to the Manantial-Espejo Project. The balance between the unwanted effects that could arise by implementing the project, against the local benefits that would be obtained, is favorable to the performance of the Manantial-Espejo Project.

No reclamation bond is currently required for mining operations in Argentina. Triton has allotted funds for reclamation efforts. As the operations begin a detailed reclamation plan will be developed.

The EIS has been submitted and is under government review. The following permit list indicates the current status of major permits associated with the Manantial-Espejo Project.

Table 31 Status of Major Permits

Type of Permit	Enforcement Authority	Permit	Status
ENVIRONMENT	Province Mining Directorate of Santa Cruz (DPM)	EIS: Environmental Impact Study	Presented on 07/11/05. Triton presentation of response to DPM final questions 7/03/06. Waiting formal approval.
		Mining Producer Register	Granted -Annual Renewal
	Water Resources Office of the Province of Santa Cruz	Water extraction and use - Exploration Phase	Presented on 01/09/05 Approved on 27/10/05 by Disposition 011/DPRH/05
	Environment Secretariat of the Province of Santa Cruz	Registration in the "Generation of Hazardous Waste Register"	Requested on 28/October/05.Legal and technical report approved. Waiting for a resolution of the Authority.
	Gobernador Gregores' Municipality	Municipal License- Offices	Granted
CONSTRUCTION and TRANSPORTATION	Commerce and Industry Division of the Province of Santa Cruz	Registration in the Commerce and Industry Activities Register	Granted on 15 December 05
	Registro Nacional de Armas (RENAR)	License as "user who received explosives services"	Granted on 20-January-2006
	National Communications Commission (CNC)	Radios Permit	Granted. Frecuencies habilitated by authorization N° 18401/2005
TAXATION - LABOR	National Mining Secretariat	Tax Stability	In process
		Registration in Law 24 196 (Other benefits: Double Deduction- Accelerated Depreciation- Importation of Equipments	Granted in 1997 - Valid up to January 2006
	Federal Administration of Public Revenues (AFIP)	National taxes registrations (DGI)	Granted
		Importer-Exporter registration. (DGA)	Granted
	Subsecretaria de Recursos Tributarios de Santa Cruz	Tax Provincial Registration	Granted
		Application for exemption over exportations.	To apply when exporting.
	Commerce and Industry Division of the Province of Santa Cruz	Application for Certificates of origin for exportations.	To apply when exporting.
	Secretary of Labor of Santa Cruz -Labor and Union Authorities	Collective Labor Agreement - Mining employees. (AOMA)	Without Collective Labor Agreement by now.

Geomorphology, Relief and Soils

The area directly involved by the Manantial-Espejo Project is about 1,000 ha within a total area of 42,000 ha. The local area soils have very low productivity for agriculture and livestock purposes.

The anticipated impacts to the local geomorphology, relief and soils, are of moderate magnitude, pointlike and reversible. The impacts arise principally from the earthwork needed to extract the ore (open pits and galleries) and from the accumulation of sterile rock in landfills.

Surface Water

There are no permanent water bodies within 6 km of the proposed mine facilities. There are three semi-permanent or permanent ground water-fed lakes within 6 to 8 km of the mine facilities. However, there are certain temporary lagoons (endorreic lowlands) that are often contain water in the spring and summer, when water accumulates from rainfall and/or snow melt. Chemical analysis demonstrates that, typical of the area, the water quality of these temporary lagoons, and the lakes

is generally unsuitable for potable, livestock or irrigation usage, due to elevated contents of total dissolved solids (TDS - approx. 2,000 to 200,000 mg/L), suspended solids, fluoride, nutrients and various metals.

The anticipated supply of water from mine dewatering (about 16 L/s) could partly modify the natural quality of such temporary lagoons, if they are used for discharge of water from dewatering wells, largely through the addition of largely fresh (TDS < 1000 mg/L) water with a low suspended sediment content.

There is a minor potential of drawdown impact on neighboring lakes, however this will be monitored and is easily mitigated, if necessary, through recharge of water from dewatering wells to minimize drawdown impacts.

The drainage from the tailings impoundment to the adjacent lagoon area could carry chemicals that would partly modify the current water quality. Management plans and procedures will be established to limit runoff from the tailings impoundment, or to initiate remedial action should substantial runoff or accidental release of chemicals into a body of surface water occur.

Pit lakes are predicted to form in the Maria Central and Karina-Union Pits after mine closure. The water quality in these lakes is expected to be initially fresh (TDS < 1,000 mg/L) to brackish (TDS between 1,000 mg/L and 10,000 mg/L), but with evaporation will gradually decline to surface water quality similar to other lakes in the area.

The Manantial-Espejo Project does not pose any significant Acid Drainage from Rocks (ADR) hazard. The low concentration of sulfides in the rocks in the development area and the low rainfall values typical of the area indicate that no environmental impact is to be expected from acid drainage from rocks (ADR). The low ADR hazard, together with the lack of surface water bodies in the Manantial-Espejo Project Area, indicate that impacts to surface water will be minimal. Surface water quality monitoring will be undertaken down gradient of waste rock dumps and in the North Volcanic Centre lagoon, when present.

Ground Water

Ground water lies at a depth of between 50 and 75 metres in the mine area, and from about 1 to 30 m in the North Volcanic Centre ("NVC"). The country (Chon Aike) volcanic rock is generally of low to moderate permeability, however, within the mine area, fault and fractures associated with ore-bearing veins possess moderate to high permeability.

The ground water impacts identified are of low magnitude, discrete and partly reversible. One potential impact is minor seepage from the tailings impoundment to underlying ground water. The magnitude of this hazard is considered low

because the bottom of the tailings impoundment consists of more than 40 meters of low permeability siltstones capped by silty clay, and because of hydraulic containment (internal drainage) present within the basin which will host the tailings. The containment is a result of the physiography of the basin, coupled with relatively high levels of evaporation from the base of the North Volcanic Centre.

The studies performed show low horizontal hydraulic conductivity values with a geometric mean of 3×10^{-8} meters/second. The silty clay has a hydraulic conductivity in the order of 10^{-9} metres/second. The geological studies conducted by Triton in the NNVC, where the tailings dam will be located, indicate that the NVC is a basin that is hydraulically-contained.

However, placement of the tailings, coupled with potential drawdown of the water table from the mine to the south could potentially result in minor seepage from the south edge of the tailings impoundment.

If such seepage occurred, it would be limited by the low-permeability silty clay and siltstones. Once the mine work is completed, it is foreseen that the hydraulic containment will gradually be re-established, as the tailings pore water evaporates and drains and as drawdown from the mine decreases. Seepage will be confined within the NVC, with a best estimate maximum seepage distance of 200 m, before being gradually drawn back into shallow ground water in the base of the NVC. We expect that, within 20 years as from the disposal, the concentration of cyanide in ground water in the tailings, and down gradient of the tailings, will fall below the Argentine reference value for drinking water, i.e. 0.1 mg/L. Hence ground water containing cyanide above drinking water criteria should not travel more than 200 m from the southern edge of the tailings impoundment, hence would be confined entirely within ground water underlying the NVC.

Seepage, if any, from the tailings impoundment will be monitored through monthly ground water level monitoring and tri-monthly ground water quality monitoring, in several monitoring wells located down gradient of the tailings. Seepage may be controlled through a variety of measures, including limiting drawdown of the water table by re-injecting fresh water from the mine dewatering system down-gradient of the tailings impoundment.

Minor seepage is expected to occur from the waste rock dumps down to the underlying water table. A portion of this seepage is expected to report to the Maria Central and Karina-Unión pit lakes, and portion will report to the water table. Due to the low rainfall and high evaporation rates and low ADR potential, the quantity of seepage is expected to be minor, and impacts are anticipated to be minimal. Ground water monitoring will be undertaken down gradient of the waste rock dumps, as well as the ore stockpile, present during the mine life only.

Ground water monitoring will also be undertaken in the processing plant area, to safeguard against potential spills or leaks of fuels or other materials. Management plans and procedures will be in place to provide mitigation should releases occur.

Wild Flora and Fauna

The local flora is very scant and the impacts are largely associated with ground clean-up, earthwork and disposal of steriles in landfills. The area directly involved by the Project is about 1,000 ha within a total area of 42,000 ha corresponding to the mining premises.

The local fauna is very scarce and the impacts are largely associated with the habitat changes resulting from the presence of the mine personnel and machinery, operation in the area. Animals which may be affected include *guanacos, ñandúes* and birds.

During the operation of the mine, the tailings impoundment will have a maximum area of approximately 100 hectares and will be fenced in to prevent the entrance of stray animals. Although the concentration of cyanide (CNWAD) will remain below 50 ppm, the process must be controlled in order to avoid deviations that could be detrimental to birds that could eventually use it as a landing area.

Environmental Monitoring Plan

The EIS includes a detailed Environmental Monitoring Plan (EMP), that is integrated into the environmental management for the project. The EMP is the means for evaluating the progress of the Manantial-Espejo Project and to ensure the implementation of mitigation measures and meeting the requirements of regulations.

The Environmental Monitoring Plan requires not only following up on the significant environmental matters concerning the Project, but also on the regulatory permit to ensure that it is used under conditions of suitable accuracy and control of operations (i.e. specialized and duly trained personnel, approved techniques, properly adjusted analysis equipment, data input centers and analyses with official recognition and certificates).

Public Consulting Action

The EIS documents the main citizen consulting and participating actions taken by Triton for the Manantial-Espejo Project. In support of the Environmental Impact studies, and as a part of its Citizen Consulting and Participating Program, Triton conducted various activities in order to present the Manantial-Espejo Project to the community of Gobernador Gregores and to local and provincial authorities.

These activities included meetings with the relevant parties, presentations to the authorities and visits to the mine site.

Triton plans to continue working with the Municipal Authority of Gobernador Gregores, the Ministry for Health and Social Action and the Board of Education of the Province of Santa Cruz, in order to assist them with the timely expansion and/or restructuring of schools and hospitals, as the demand grows from the increase in the population of Gobernador Gregores, which will occur with commencement of development of the Manantial-Espejo Project.

25.8 Employment

The Manantial-Espejo Project area is remarkable for its very low population density, below 1 inhabitant / km^2. For the last ten years there have not been any significant changes in population density reported in the Province of Santa Cruz. Magallanes, the specific municipal region (Communa) where the property resides, reports a density of 0.3 inhabitant / km^2 and Rio Chico show only 0.1 inhabitant / km^2.

Triton has designed and is carrying out a selection and recruitment Human Resources plan that supports the construction and operational stages of the Project. This includes an analysis of the type and amount of labor required, development of a digital Human Resources system, and implementation of training planning.

The nearby community of Gobernador Gregores has a population of 2519 inhabitants and the labor requirements for the project will have a significant impact on Governador Gregores. There are currently no training programs in place and it will be necessary to design and implementation recruitment and selection programs as well as human resources training, not only for Gobernador Gregores, but also for other areas close to the project.

A survey of Santa Cruz employment shows 77% of the working population is employed 53% of whom work for the government and 47% for the private sector. Only 5% of the occupied population is employers, 16% are self-employed workers and only 2% are family workers.

The construction phase of the project is expected to take about two years and manpower will peak at about 1,000 direct and 800 indirect employee positions. A majority of these will be workers employed by the various construction contractors. The construction workers will live at a temporary camp erected at the site.

Indirect employment would include new work positions related to building of houses, subcontracting of services related to the project and due to the

development of local micro-enterprise, such as food provisions or services related to the project (transport and accommodations).

The operating phase of the project will employ 407 direct work positions. Direct labor requirements are estimated as follows:

Administration and Management	63
Plant and Operations	109
Open Pit Mine	105
Underground Mine	130

Indirect employment will continue to be generated much as discussed for the construction phase.

25.9 Taxes and Royalties

The Project financial model recognizes payments of certain taxes and royalties that are off-set to some degree by certain export credits available in Argentina. The model includes provisions for paying a 5% export tax on sales, a 35% corporate tax on taxable income inclusive of a double deduction for exploration expenses, and some additional minor tax considerations including transaction, shareholders, and property taxes.

The financial model includes provisions to pay a Provincial Royalty in the amount of 1.7% on net operating cash flows before corporate taxes. Additionally, the model recognizes two royalties to Barrick who previously held the property in the amounts of $0.60 / tonne on the first 1,000,000 tonnes mined and 0.5% on net smelter returns (NSR).

The financial model includes two available export credits in the amount of 2% on net sales for a Silver Doré Export Credit and a Patagonian Port Export Credit in the amounts of 3% in 2008, 2% in 2009, 1% in 2010 on net sales.

The Project financial model recognizes payments required for third party royalties, taxes, and export credits according to the listing presented below:

Royalties (Defined by PAS & Triton personnel)

There are two distinct royalties due on Manantial-Espejo production as follows:

- Barrick Royalty A: $0.60 / tonne on the first 1,000,000 tonnes mined.
- Barrick Royalty B: 0.5% on net smelter returns (NSR).

Taxes (Defined by PAS & Triton Personnel)

The following list outlines the taxes to be paid on mining the Manantial-Espejo ore bodies:

- **Provincial Royalty:** 1.7% on net operating cash flows before corporate taxes.
- **Export tax:** 5% on net sales.
- **Bank Transaction Tax:** 0.6% on any operating bank transactions.
- **Shareholder's Tax:** 0.5% on accumulated retained earnings.
- **Corporate Tax:** 35% on taxable income.

The Argentinean taxable income calculation is determined based on the following, using the benefits of the law #24196 of the Argentinean mining investment law:

- Depreciation can either be at normal or accelerated rates. Once one method is chosen, it will apply to all assets for the life of mine.
- Loss Carry Forwards expire after five years.
- Exploration expenses prior to construction are allowed to be deduced for tax purposes either immediately or amortized over the life of the mine.
- Double deduction of exploration expenses: Exploration expenses prior to construction are allowed to be deducted twice for taxable income tax calculation. The second deduction has a valid period up to five years after initializing production.

Export Credits (Defined by PAS & Triton Personnel)

The following export credits are allowed in Argentina and included in the financial model:

- Silver Doré Export Credit: 2% on net sales.
- Patagonian Port Export Credit: 3% in 2008, 2% in 2009, 1% in 2010 on net sales.

These credits are reimbursed periodically to Triton against any Federal income tax liability. The income must be associated with the company's operations.

Property Taxes (Defined by PAS & Triton Personnel)

An allowance for property taxes has been included in the cash flow projection.

As the Manantial-Espejo Project qualifies under the Argentinean investment mining law #24196, the project is exempt from all importation taxes based on an evaluation by PAS & Triton personnel. A custom and port duty fee of 2% is payable and is included in the capital cost of the equipment.

The value added tax rate (IVA) in Argentina is 21%. However, the VAT rate for all capital equipment and construction costs is 10.5%. All operating expenses and

capital costs are subject to this tax. Reimbursements for the tax usually take one year after the application is put in place.

IVA is a value-added sales tax at the Federal level. This tax is normally aggregated on purchases on nationally and, possibly, internationally provided goods and services. These monies accumulate to a tax credit account and are reimbursed periodically to Triton against any Federal income tax liability. The income must be associated with the company's operations.

In Argentina the property tax is considered a property maintenance cost, and is included in the operating costs. This payment is made in two parts during the year, and is proportional to the size of the mining concessions. For Manantial-Espejo it amounts to approximately $70,000 per year.

25.10 Capital Cost Estimates

Triton commissioned M3 to complete the feasibility study inclusive of defining and estimating the operating and capital costs for the plant and site infrastructure as well as determining the technical viability of the Manantial-Espejo Project. The total Manantial-Espejo Project capital cost estimate has been developed by a combination of sources and consolidated by PAS. M3 developed an estimate to construct the plant and infrastructure, Snowden provided the capital cost estimate for the owner operated mining equipment and mine development, Golder provided costs for the tailings disposal facility construction, and PAS provided estimates for various owners costs, working capital, and other indirect costs. M3 states the accuracy of their estimate is in the range of plus 15% to minus 15%. The overall Manantial-Espejo Project initial capital cost estimate includes direct costs for the procurement and erection of the mining equipment, the development of the underground and open pit mines, the direct costs for the construction of the plant and infrastructure, construction indirects, owners costs, commissioning, EPCM, spare parts and initial fills of consumables, working capital, and VAT taxes paid during the construction phase of the Manantial Espejo Project. Table 32 summarizes the Initial Capital Costs for the Manantial-Espejo Project stated in 4th quarter 2005 US dollars, include a fixed Argentine Peso to US dollar exchange rate of 3:1, and exclude any considerations for escalation.

Table 32 Initial Capital Cost

Initial Capital	($ in Thousands)	Source
Pre-Stripping/Develop	$ 6,897	PAS
Open Pit Mine	$ 8,984	Snowden
Underground Mine	$ 6,630	Snowden
Plant	$ 47,743	M3
Infrastructure	$ 17,274	M3
Tailings	$ 3,469	Golder
Owners Cost	$ 10,017	PAS
Commissioning	$ 2,671	PAS
EPCM – Administration	$ 2,250	M3
Spare Parts & Initial Fill	$ 3,332	M3
Working Capital	$ 2,810	PAS
Sub-total	$ 112,076	
VAT Tax	$ 18,070	PAS
TOTAL	**$ 130,146**	

NOTE: Capital estimate includes $8,914,000 in contingency.

An additional sustaining capital of $5,673,000 and closure cost of $10,751,000 is spent over the life-of-the-mine off-set with $4,773,000 for equipment salvage. The total initial working capital of $2,810,000 and half of the spare parts $1,666,000 becomes an operating cost at the end of the life. The other half of the spare parts of $1,666,000 is considered obsolete inventory at the end of the mine life.

Over the life of the mine $18,857,000 is paid for VAT taxes (inclusive of the $18,070,000 paid during the initial project capitalization) on capital items and of this $18,480,000 is recovered.

25.11 Operating Costs

PAS commissioned M3 to complete a feasibility level evaluation of the operating and capital costs, as well as the technical viability of the project. In addition, PAS commissioned Snowden to complete the feasibility level engineering and life of mine operating cost estimates for owner operated surface and underground mines.

M3 provided an operating cost estimate for the plant and infrastructure and contributed with Triton and PAS in developing the administration operating cost estimate. Triton's Argentina based staff and consultants provided local and selected consumable costs where appropriate and PAS's staff and consultants sourced a number of the direct and indirect costs for the Manantial-Espejo Project. M3 also estimated the operating and maintenance costs for the plant and infrastructure operations. Cost centers include process plant operations and

general and administration area. Operating costs were determined for a typical year, based on an average annual treatment rate of ore of 720,000 tonnes.

Snowden's costs estimates were developed using first principles, also known as bottom-up estimating, an estimating technique where costs are calculated based on the usage and cost of the resources required to complete a specific task. Underground operating costs for the Manantial-Espejo Project were estimated from development and production schedules for each of the mining areas and from a collection of common unit costs estimated for development, production, and haulage. Operating costs for the surface mine operations were estimated using life cycle costs for maintenance parts, fuel, and lubricant costs and wear parts and consumables.

Triton's Argentina based staff and consultants provided local and selected consumable costs as well as ongoing operating costs for Triton in Argentina. PAS staff and consultants sourced a number of owner specific project related direct and indirect costs and developed the financial analysis for the project. Labor costs were derived from a staffing plan and based on prevailing daily or annual labor rates for both national and expatriate employees. Labor rates and fringe benefits for local national employees were based on prevailing rates in the area and include all applicable social security benefits as well as all applicable payroll taxes.

Power costs were based on obtaining power from an utility company at a rate of $0.046 per kW h. Power consumption was based on the equipment list connected kW, discounted for operating time per day and anticipated operating load level. Reagents consumption rates for the process plant were determined from the metallurgical test data or industry practice. Budget quotations were received for reagents supplied from vendors where available with allowance for freight to site.

The operating cost for the general administration area was determined and summarized by cost element and includes labor, supplies, support infrastructure, services, and other expenses.

The operating cost estimates exclude any consideration for inflation, are based on 4th quarter 2005 US dollars, and assume a flat Argentine Peso to US dollar exchange rate of 3:1 for the life of the Project.

The average life-of-mine operating costs are summarized in Table 33.

Table 33 Life-of-Mine Average Unit Operating Costs

Cost Center	Operating Costs $/t milled	
Underground (U.G.) Mine Costs	$ 8.33	$ 27.16 $ per U.G. ore tonne mined
Open Pit (O.P.) Mine Costs	$ 9.90	$ 1.46 $ per total O.P. tonne mined
Mill Costs	$ 13.78	
G & A Costs	$ 4.26	
TOTAL	**$ 36.27**	

25.12 Economic Analysis

a. Assumed Metals Prices
Silver = $6.25/ounce
Gold = $425/ounce

b. Annual silver and gold production to doré is summarized in the following table.

Table 34 Annual Silver and Gold Production Schedule

Year	2008	2009	2010	2011	2012	2013	2014	2015	2016	TOTALS
Silver, oz	4,142,338	5,262,501	5,733,134	5,165,794	4,646,743	3,056,451	2,864,235	1,682,684	0	32,553,881
Gold, oz	57,830	52,765	71,580	53,655	62,756	55,581	83,733	41,889	0	479,789

c. The financial model recognizes shipping and third party refining costs to refine the site doré production to silver and gold bullion that can be marketed. Costs for shipping and refining are outlined in the following table:

Table 35 Doré Refining

Payable Gold	99.75%
Payable Silver	99.75%
Treatment Charge $/oz	$0.19
Gold Refining Charge $/oz	$0.50
Transportation & Insurance	$0.05

The revenues generated from the silver and gold metal sales following the refining is summarized in the following table:

Table 36 Annual Metal Sales Revenues

Revenues (k-$) at a constant silver price of $6.25/oz and gold price of $425/oz

Year	2008	2009	2010	2011	2012	2013	2014	2015	2016	TOTALS
Rev (K-$)	49,163	53,675	64,455	53,478	54,252	41,752	52,552	27,775	0	397,103

d. The financial model takes into consideration two factors defining the lag between production and monies received.

- Start-up Ramp Schedule

  The plant production is based on a 6 month ramp-up, during which time the plant will average 66% of the designed tonnage. The monthly schedule on a percentage basis is 50-50-60-70-80-90. In the model we have accounted for higher cost per tonne that will result from this reduced tonnage.

- Time Delay Between Doré Production and monies Received

  The financial model has allowed for 22 days of inventory to be carried as working capital. This is further estimated to be broken down into 2 days static plant inventory, shipping every 2 weeks (14 days) and 6 days for shipment and smelting prior to payment.

e. Inflation

The base case economic analysis has been run with no inflation (constant dollar basis). Capital and operating cots are expressed in 4th quarter 2005 United States dollars.

f. Economic Result

This project has a Net Present Value ("NPV") (0% discount) of $40,465,000 and an Internal Rate of Return ("IRR") (100% equity) of 7.0%. Payback on the initial project capital is 4.7 years at the assumed metal prices of $6.25 per silver ounce and $425 per gold ounce.

g. Sensitivities

With the inclusion of some limited accessible inferred resources in the mine plan and raising the metal prices to $4.75 per silver ounce and $475 per gold ounce, the project obtains a Net Present Value ("NPV") (0% discount) of $72.6 million and an IRR (100% equity) of 12.0% with payback on the initial project capital in 3.5 years.

Increasing the metal prices to the prices March 23, 2006 while using the mine plan inclusive of limited accessible inferred resources, the project obtains a Net Present Value ("NPV") (0% discount) of $169 million and an IRR (100% equity) of 25% with payback on the initial project capital in 2.3 years.

26 ILLUSTRATIONS

Figures 1 through 22A are attached to this Technical Report and form part of this Technical Report.

This report has been prepared by Dr. Michael Steinmann, P. Geo., Ph.D., a Qualified Person.

Respectfully submitted this 16 day of March, 2006.

Michael Steinmann, P.Geo.

Figure 1 Project Location in Argentina
(From University of Texas map collection)

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
Dr. M. STEINMANN
#143885
GEO SCIENTIST

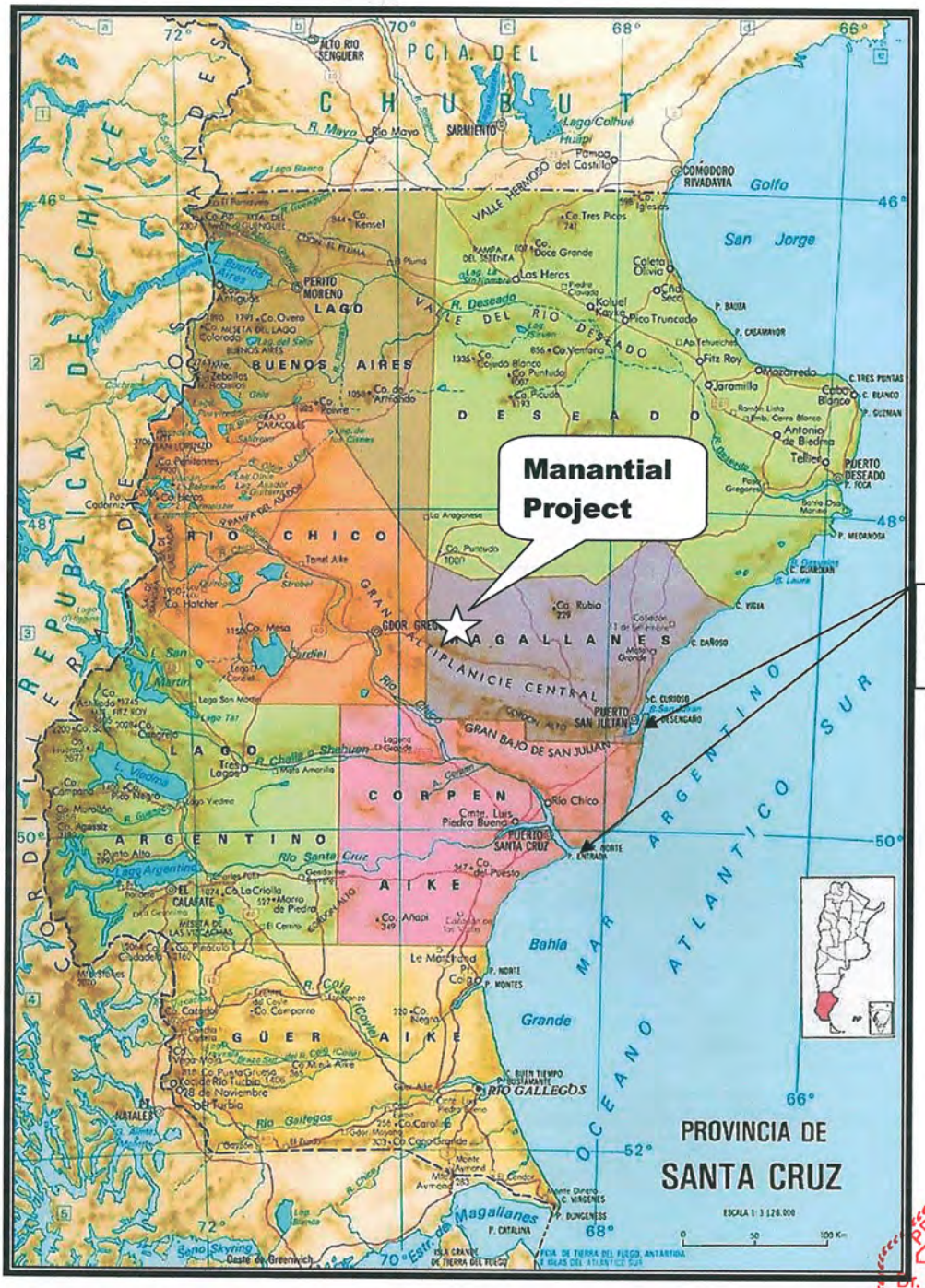


Figure 2 Project Location in Santa CruzProvince
(From University of Texas map collection)

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
Dr. M. STEINMANN
#143885

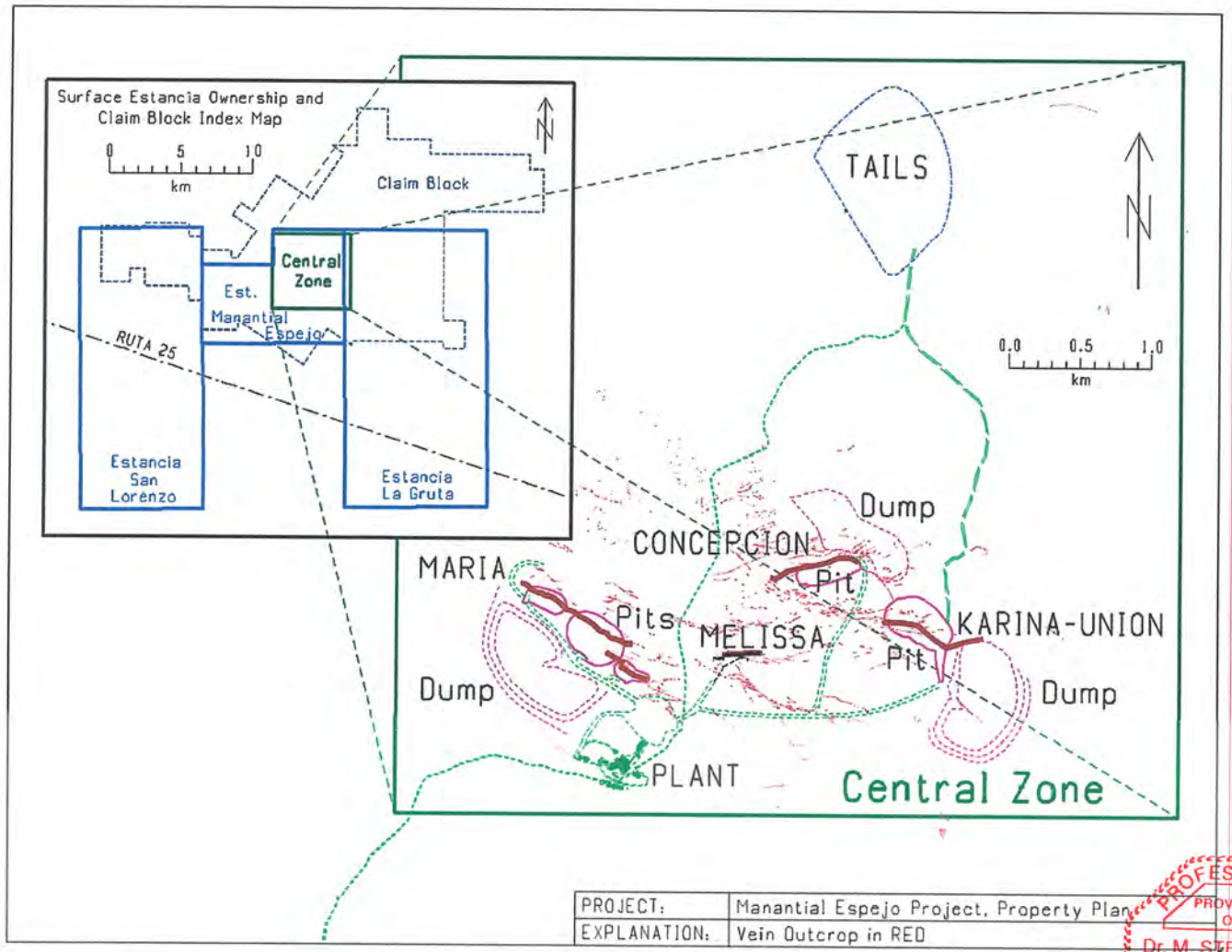


Figure 3 Property Plan

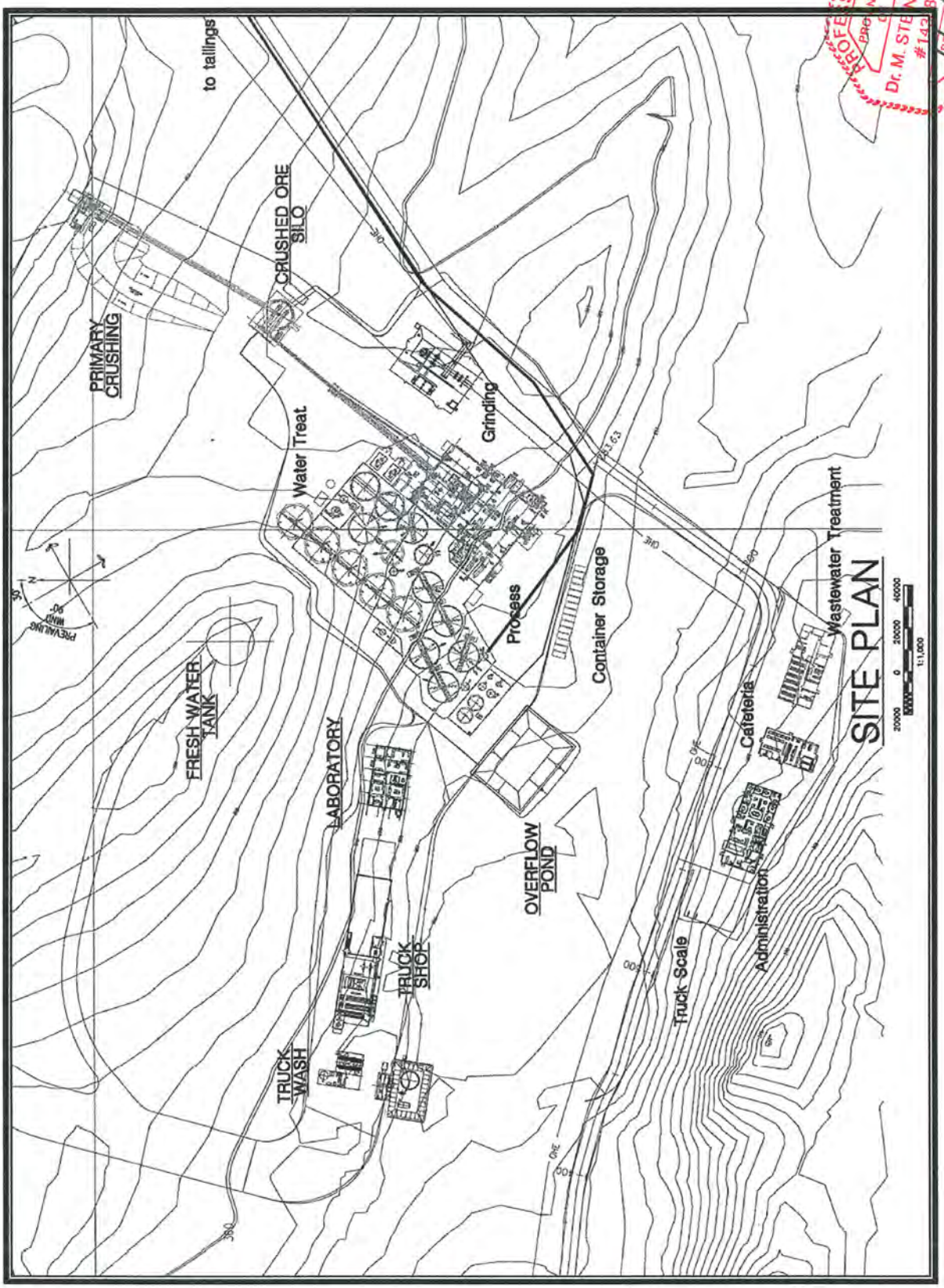


Figure 4 Facilities Site Plan

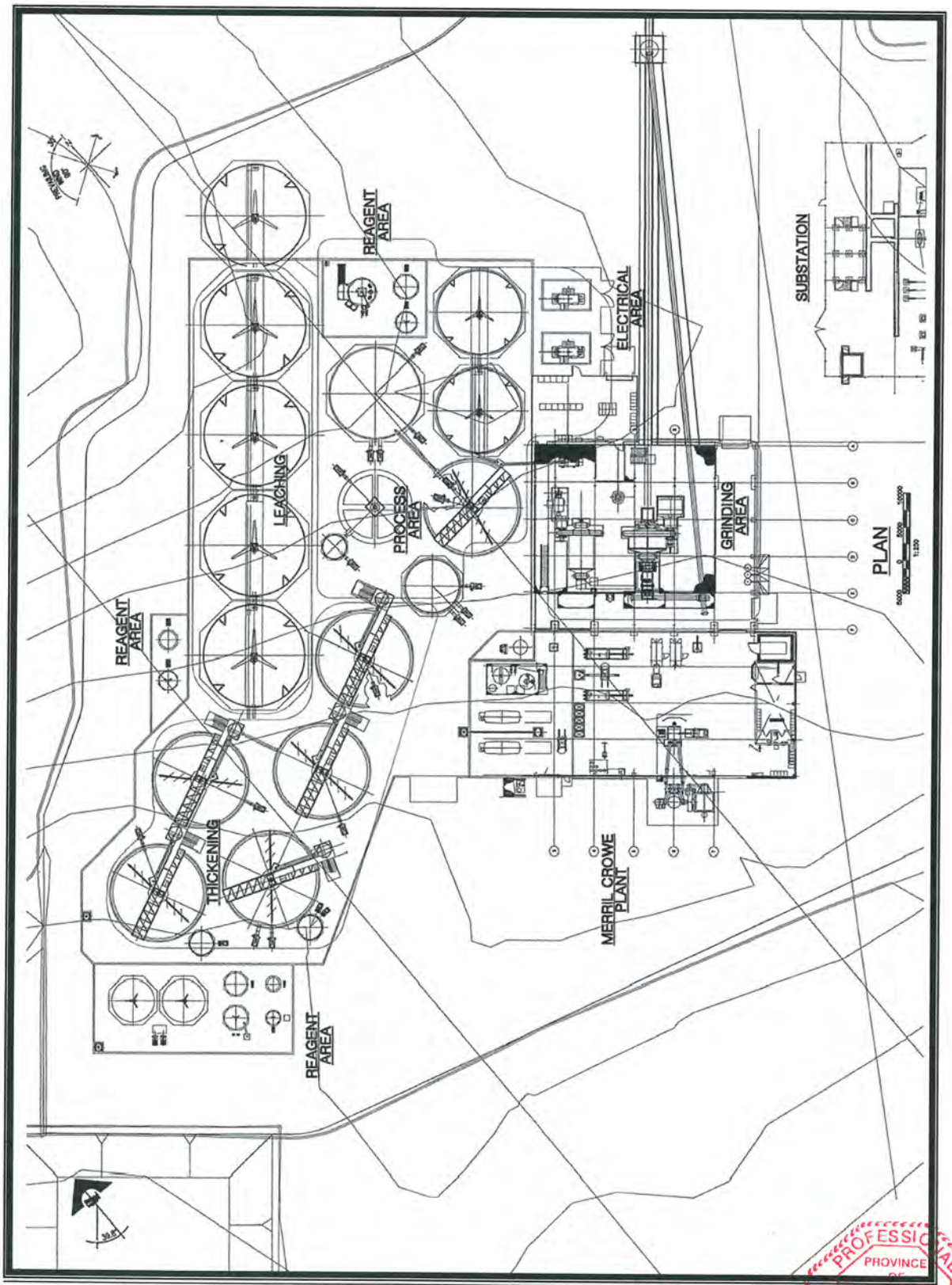
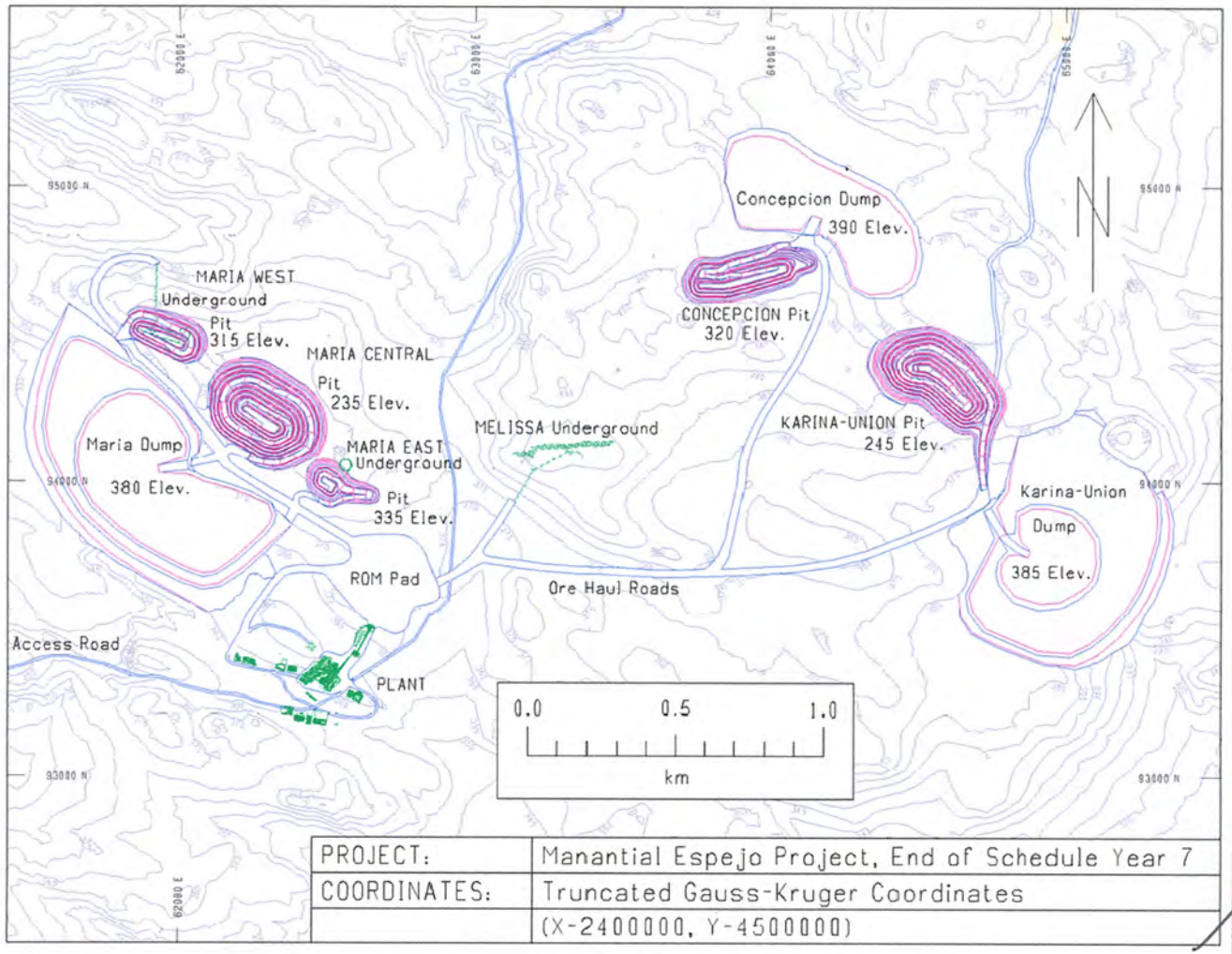


Figure 5 Facilities Process Plan



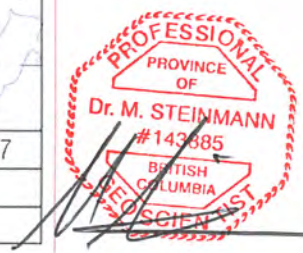


Figure 6 Manantial-Espejo - End of Schedule Year 7

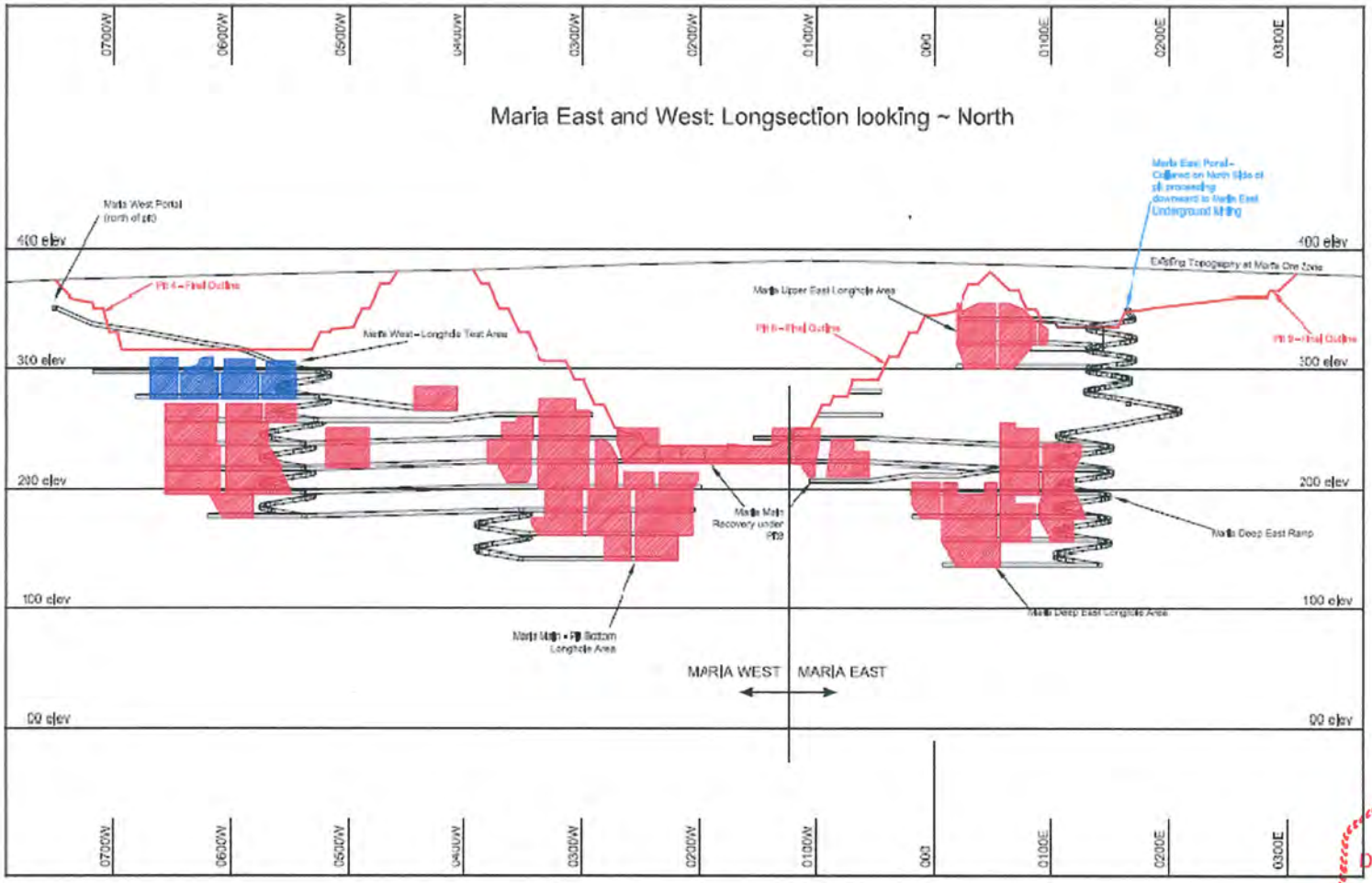


Figure 7 Maria Main Structure – Longhole Stoping

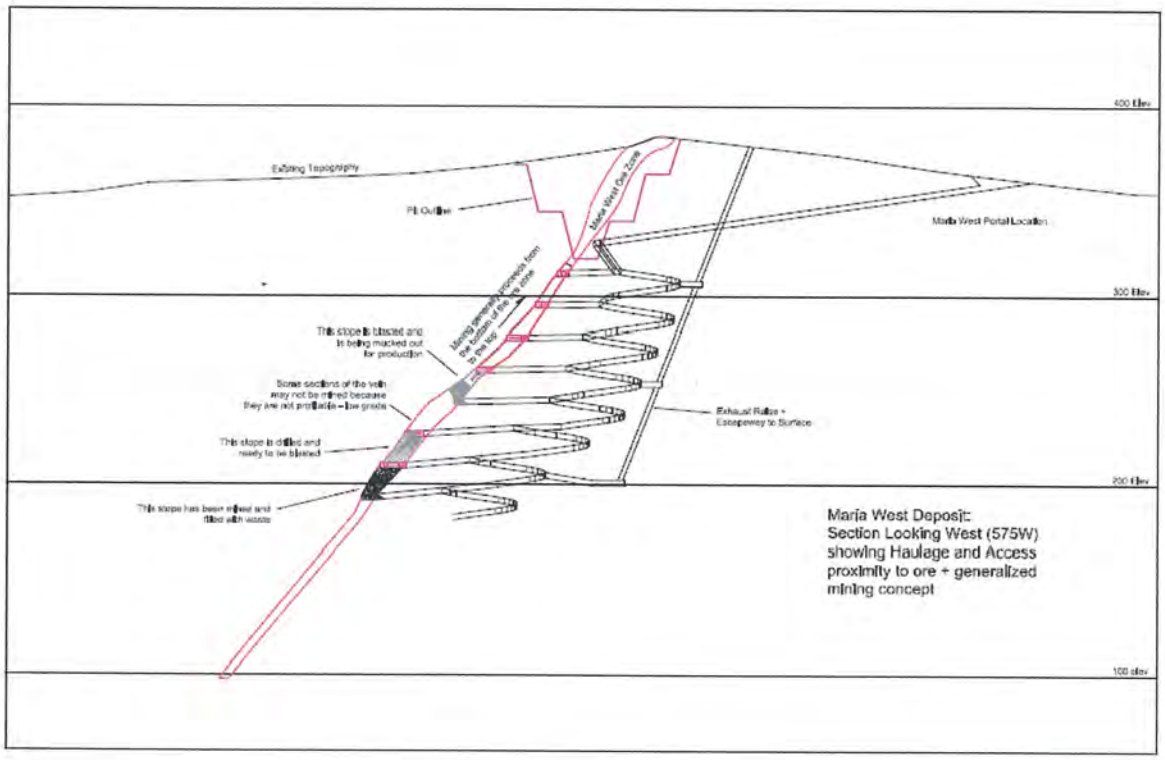


Figure 8 Typical Section Showing Longhole Mining + Access In Maria

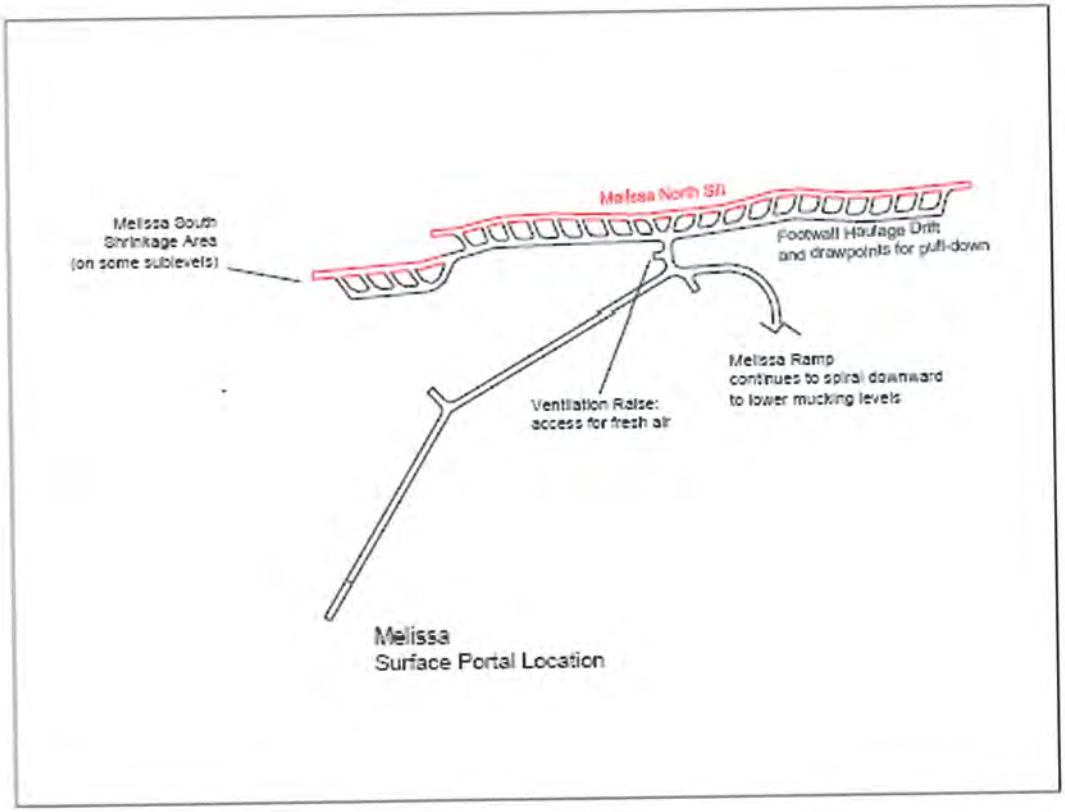


Figure 9 Typical Sub-Level Development Requirements – Shrinkage

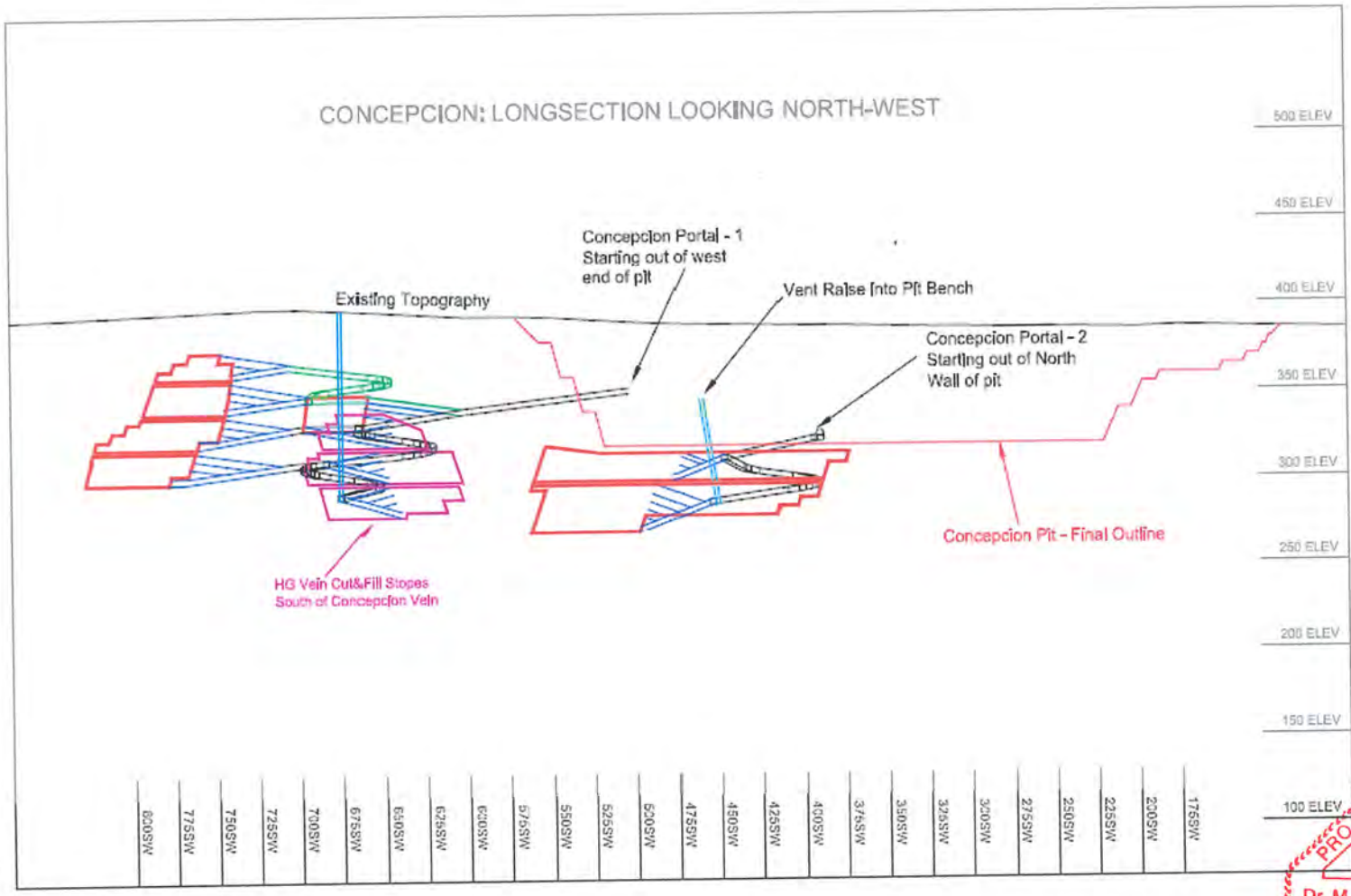


Figure 10 Longitudinal Projection of Concepcion Mining Area

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PROVINCE OF BRITISH COLUMBIA
Dr. M. STEINMANN
#143885
SCIENTIST

Figure 11 Karina-Unión Cross Section

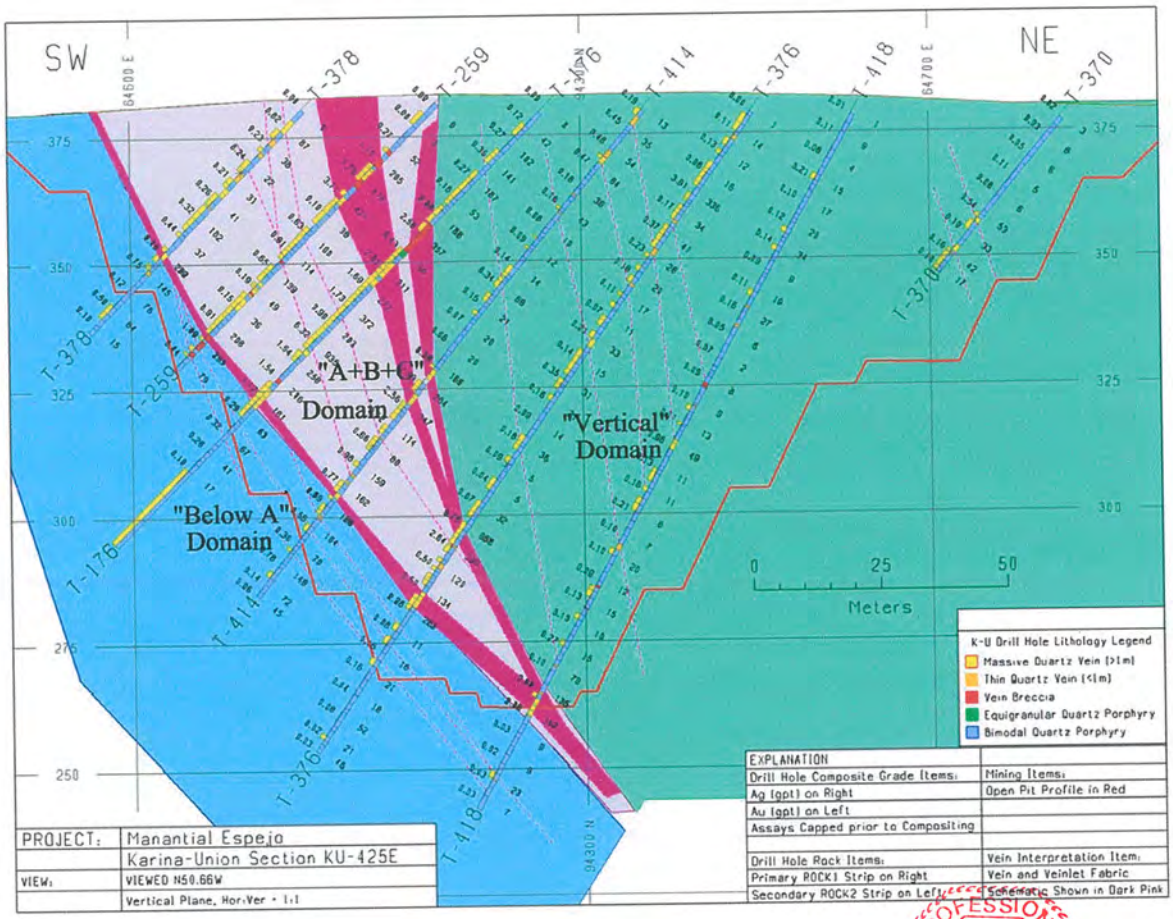


Figure 12 Concepción Cross Section

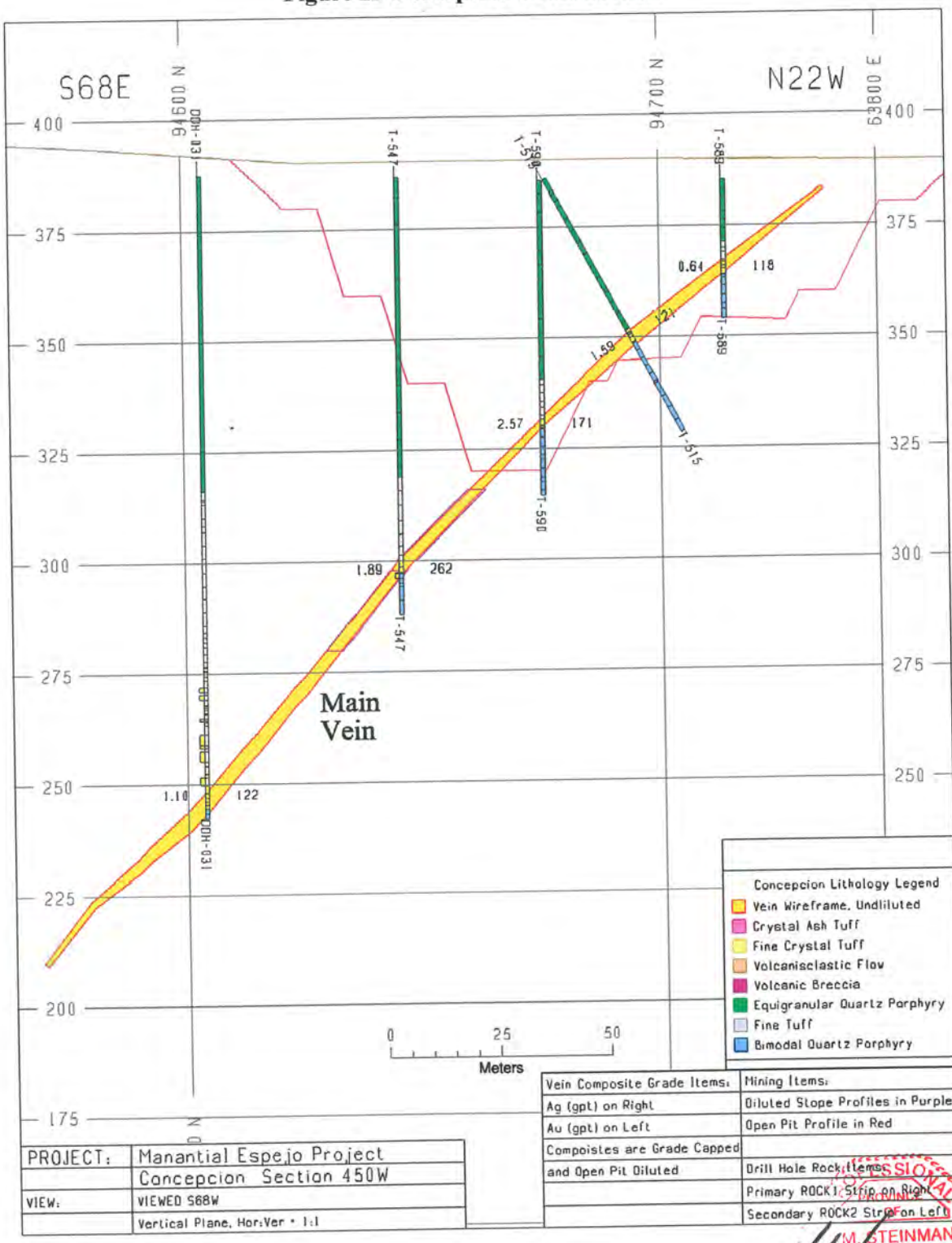


Figure 13 Melissa Cross Section

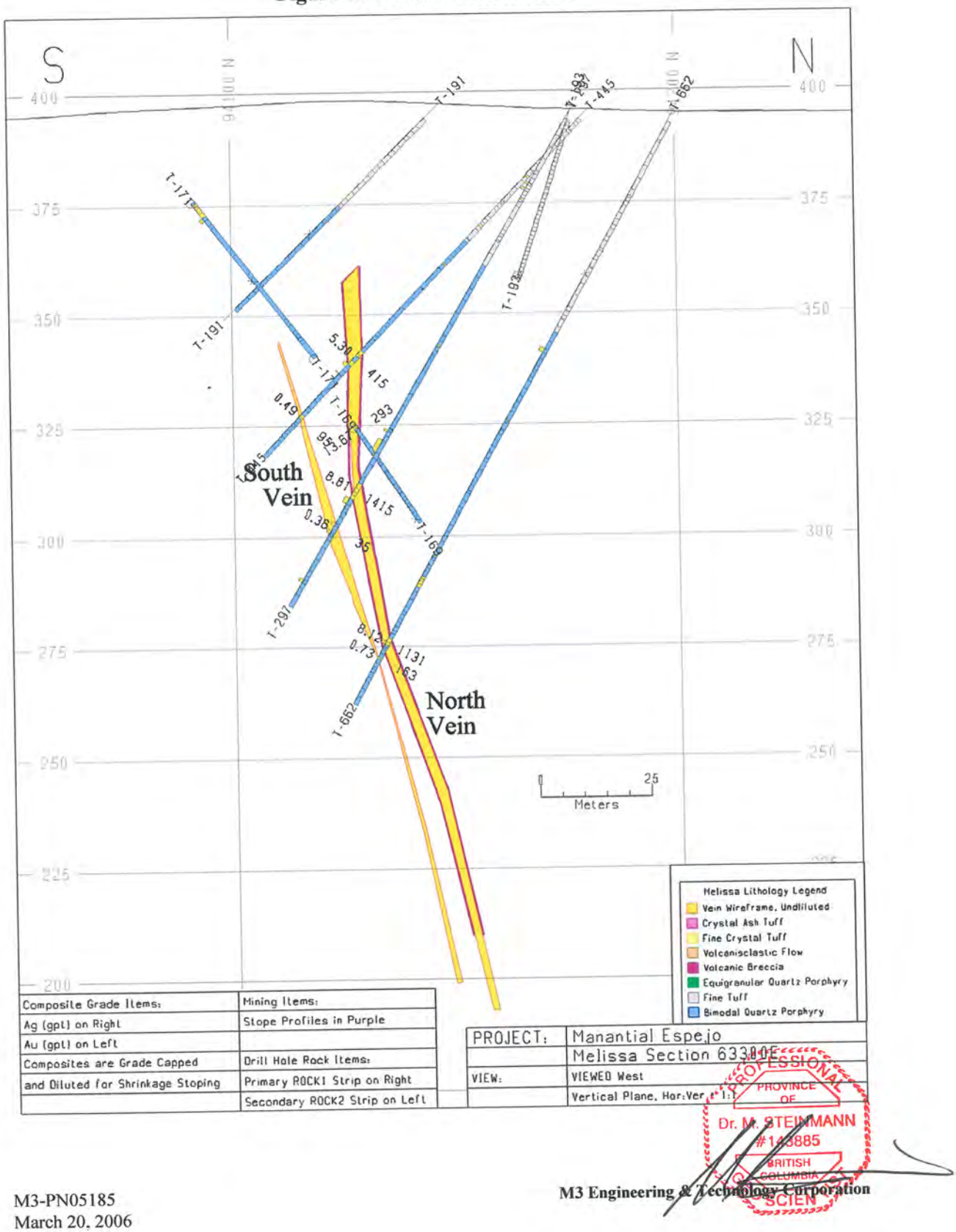


Figure 14 Maria Central Cross Section

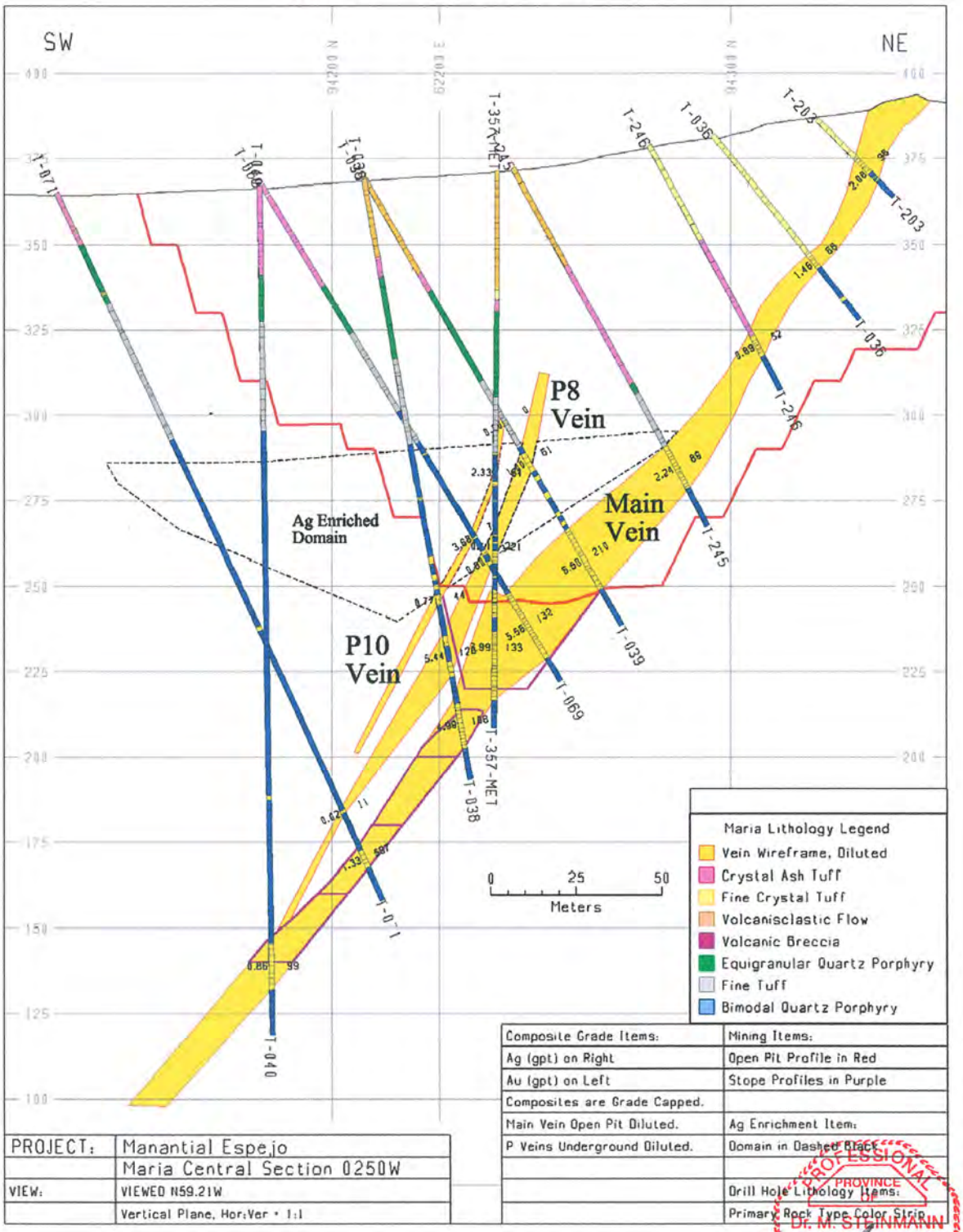


Figure 15 Karina-Unión Vein System Plan View Drill Holes Used for Estimation

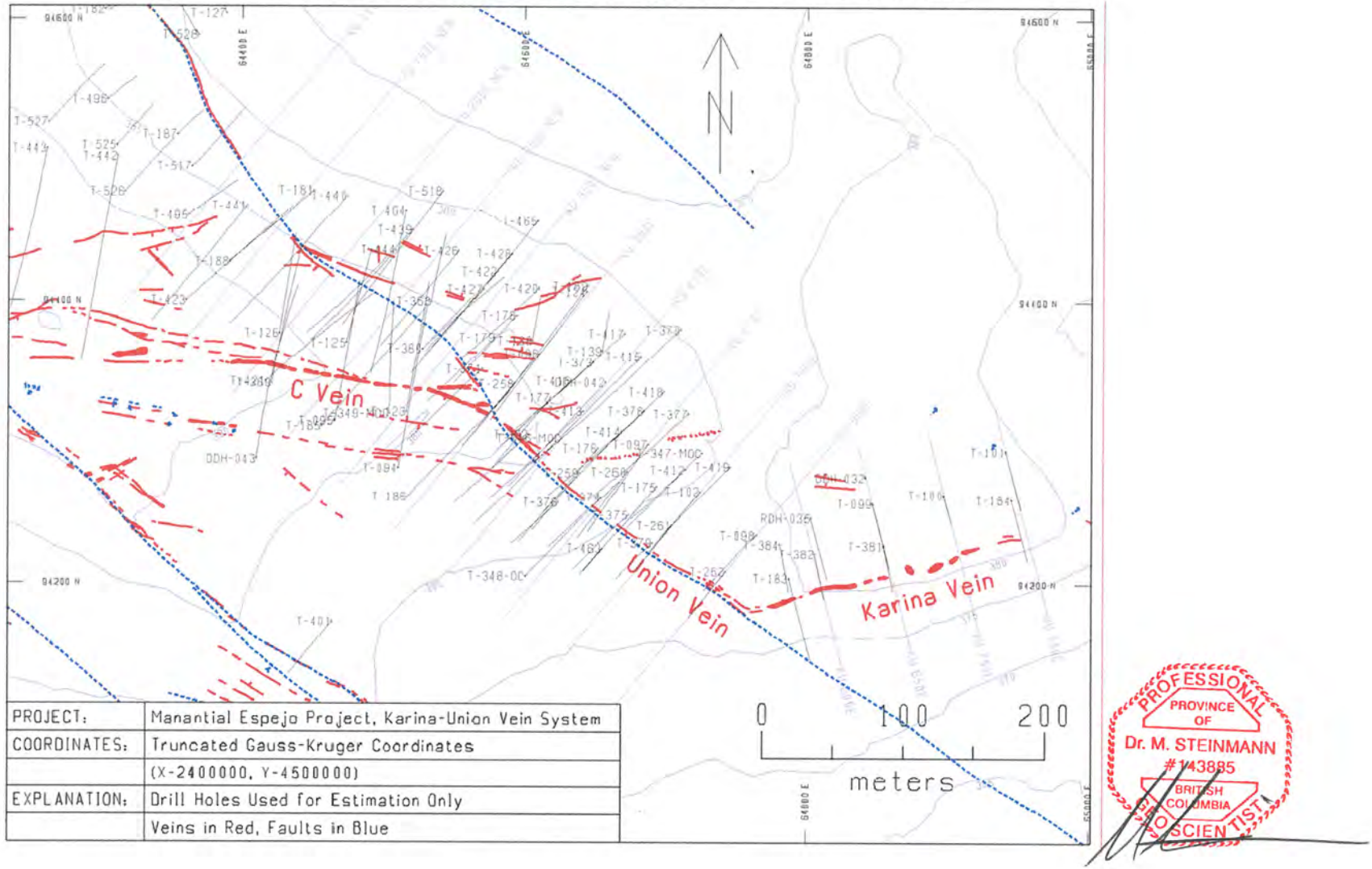
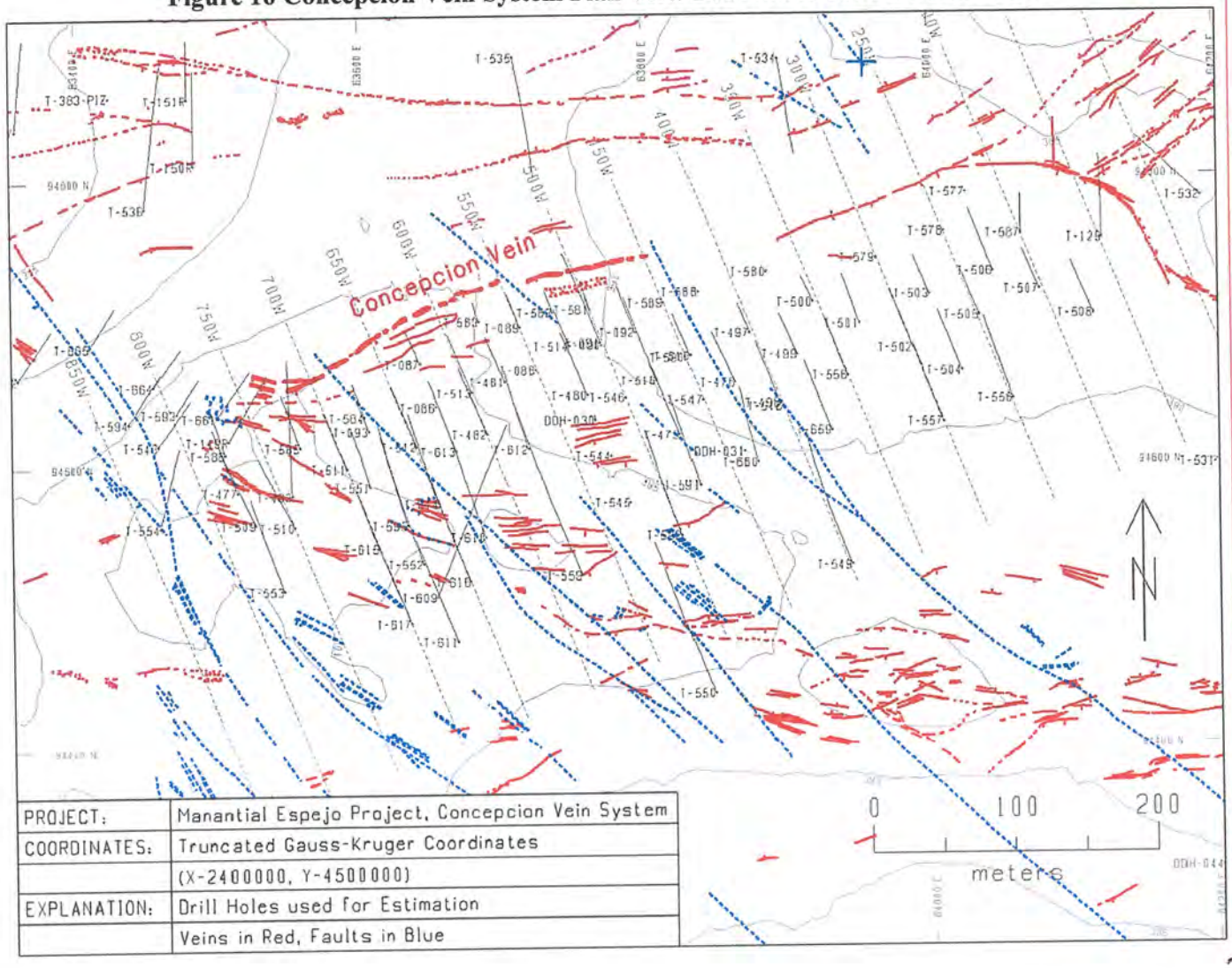


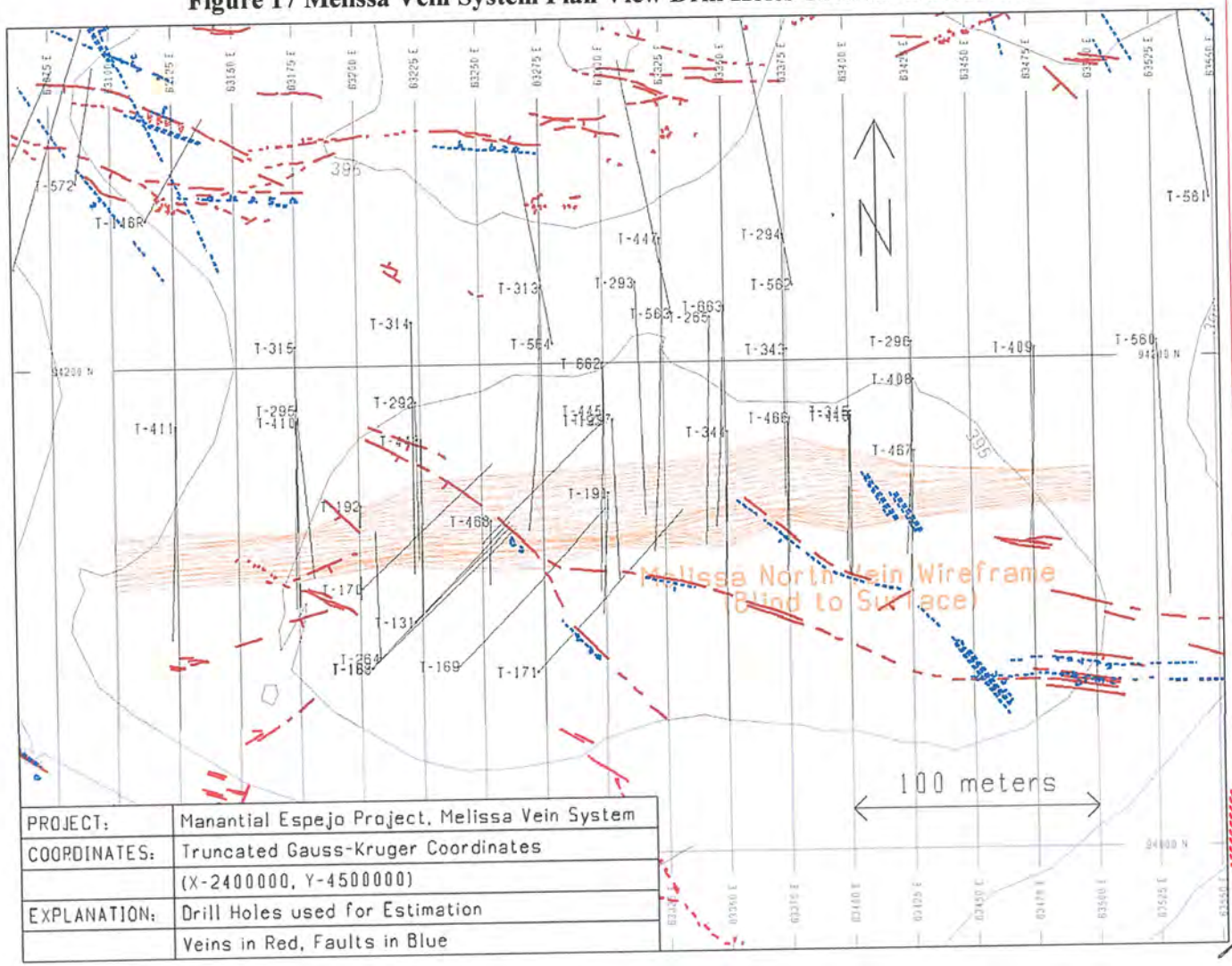
Figure 16 Concepción Vein System Plan View Drill Holes Used for Estimation



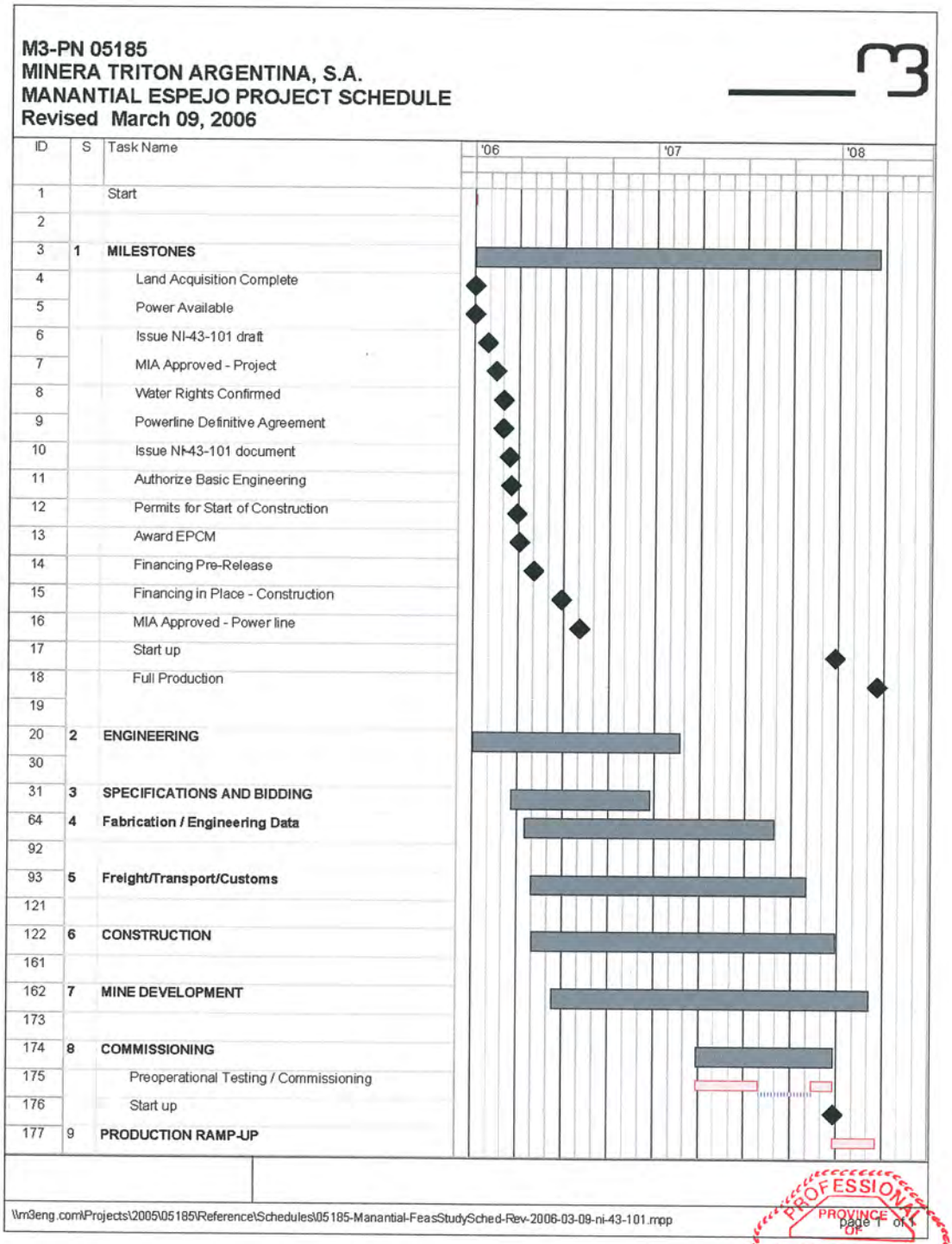
PROJECT:	Manantial Espejo Project, Concepcion Vein System
COORDINATES:	Truncated Gauss-Kruger Coordinates
	(X-2400000, Y-4500000)
EXPLANATION:	Drill Holes used for Estimation
	Veins in Red, Faults in Blue

PROFESSIONAL ENGINEER PROVINCE OF BRITISH COLUMBIA Dr. M. STEINMANN #143885

Figure 17 Melissa Vein System Plan View Drill Holes Used for Estimation



M3-PN 05185
MINERA TRITON ARGENTINA, S.A.
MANANTIAL ESPEJO PROJECT SCHEDULE
Revised March 09, 2006



ID	S	Task Name
1		Start
2		
3	1	**MILESTONES**
4		Land Acquisition Complete
5		Power Available
6		Issue NI-43-101 draft
7		MIA Approved - Project
8		Water Rights Confirmed
9		Powerline Definitive Agreement
10		Issue NI-43-101 document
11		Authorize Basic Engineering
12		Permits for Start of Construction
13		Award EPCM
14		Financing Pre-Release
15		Financing in Place - Construction
16		MIA Approved - Power line
17		Start up
18		Full Production
19		
20	2	**ENGINEERING**
30		
31	3	**SPECIFICATIONS AND BIDDING**
64	4	**Fabrication / Engineering Data**
92		
93	5	**Freight/Transport/Customs**
121		
122	6	**CONSTRUCTION**
161		
162	7	**MINE DEVELOPMENT**
173		
174	8	**COMMISSIONING**
175		Preoperational Testing / Commissioning
176		Start up
177	9	**PRODUCTION RAMP-UP**

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Figure 18 Project Schedule Summary

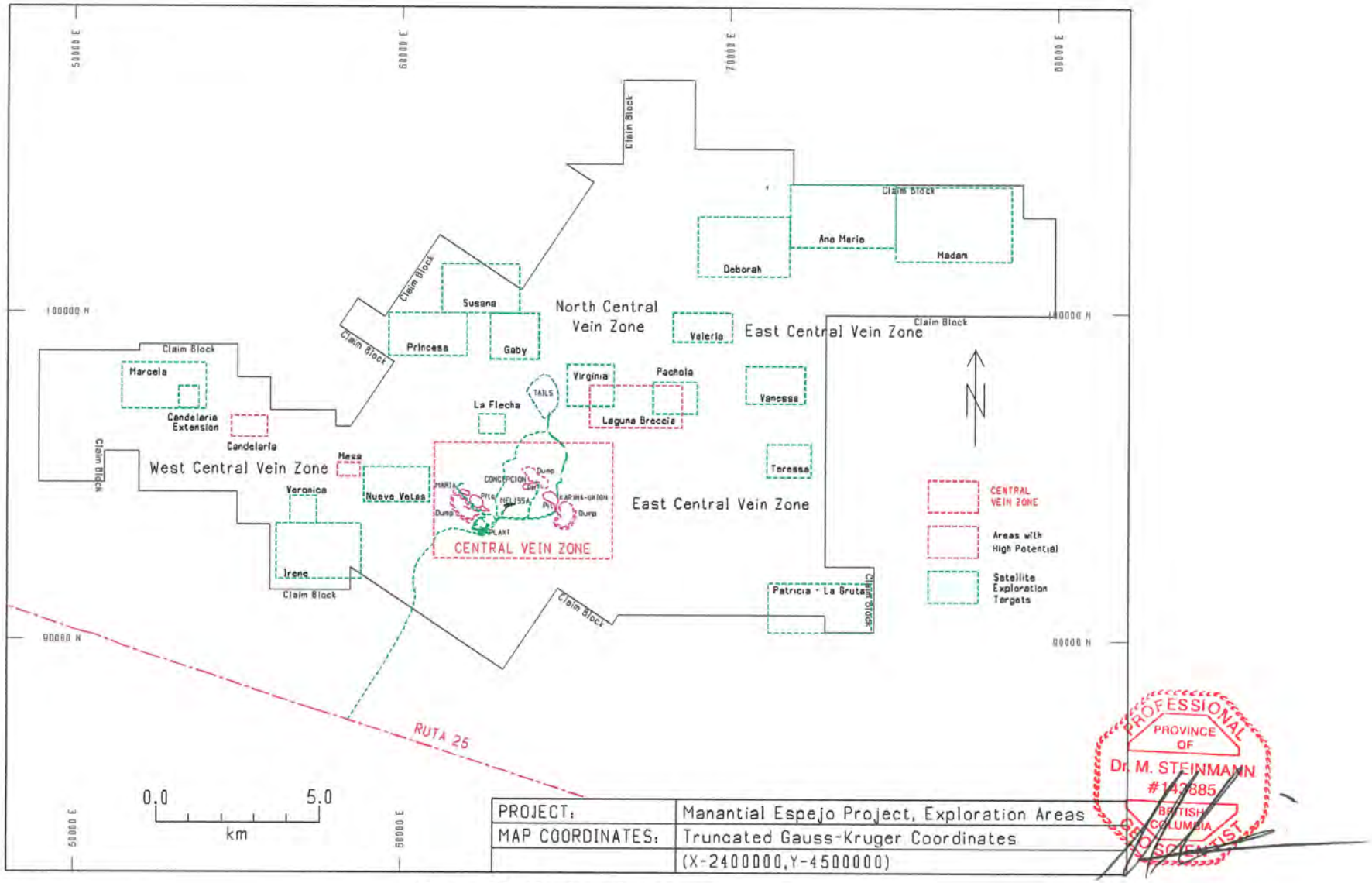
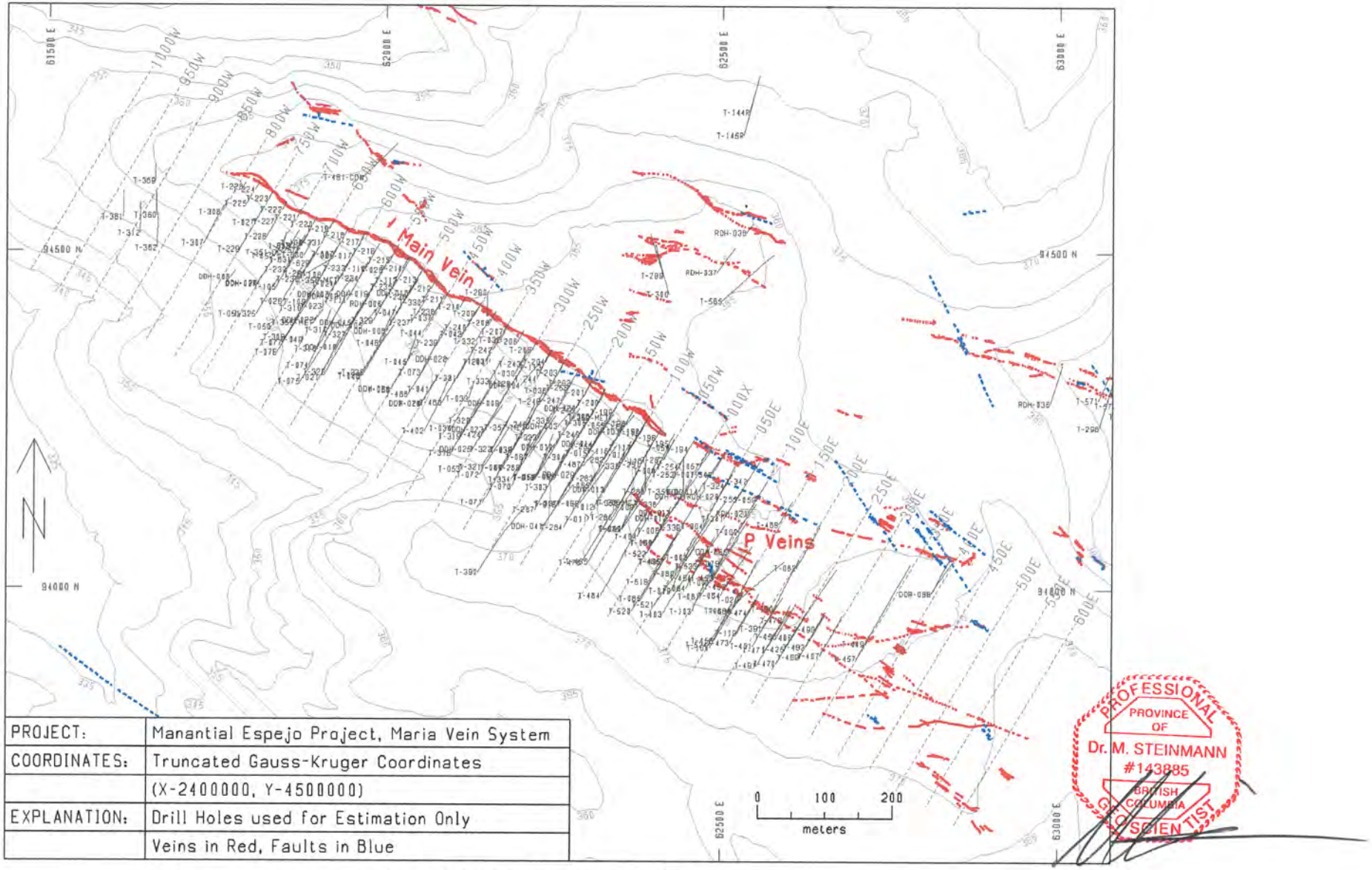


Figure 19 Exploration Areas



PROJECT:	Manantial Espejo Project, Maria Vein System
COORDINATES:	Truncated Gauss-Kruger Coordinates
	(X-2400000, Y-4500000)
EXPLANATION:	Drill Holes used for Estimation Only
	Veins in Red, Faults in Blue

Figure 20 Maria Vein System Plan View

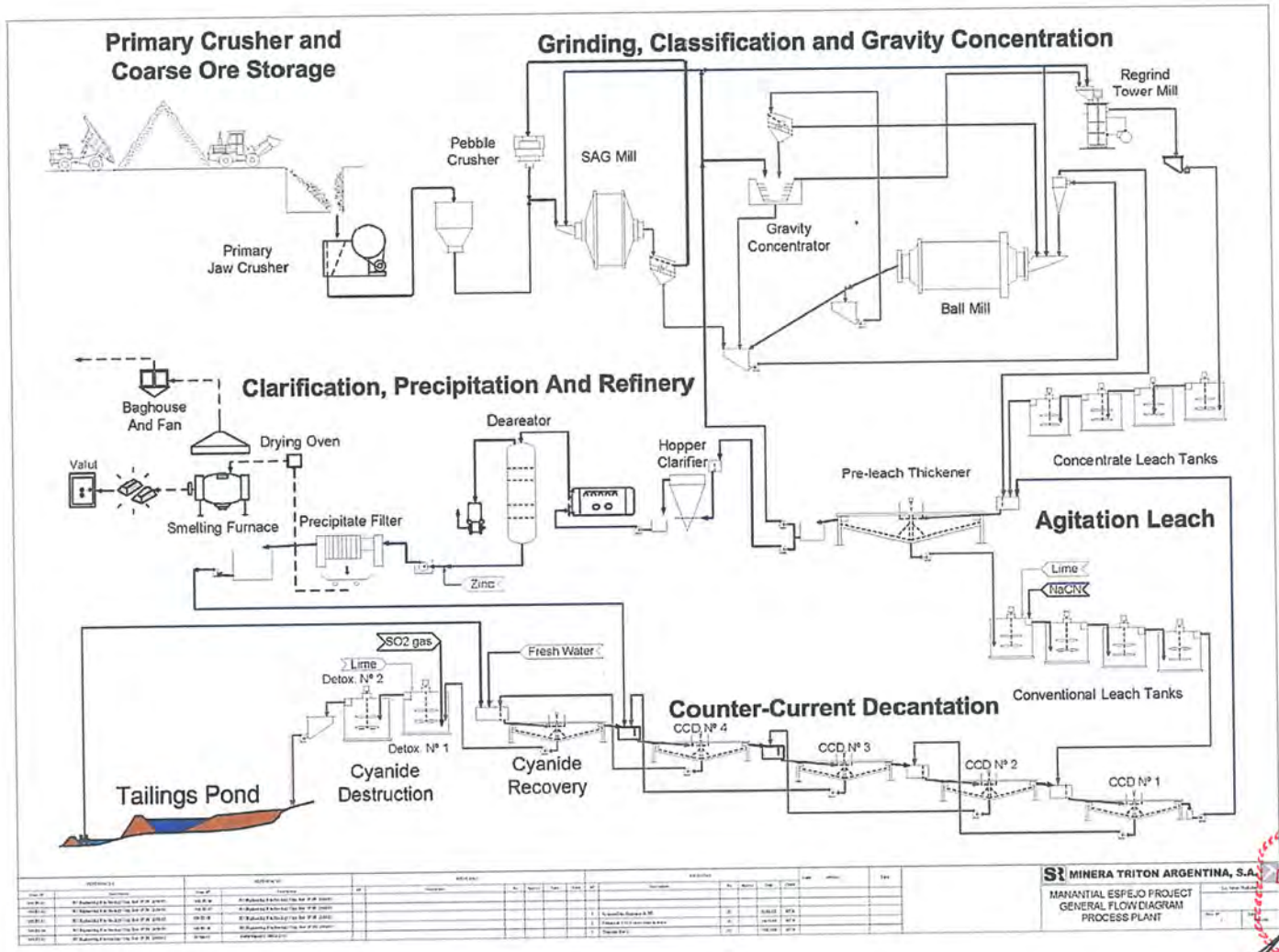


Figure 21 Process Flow Sheet

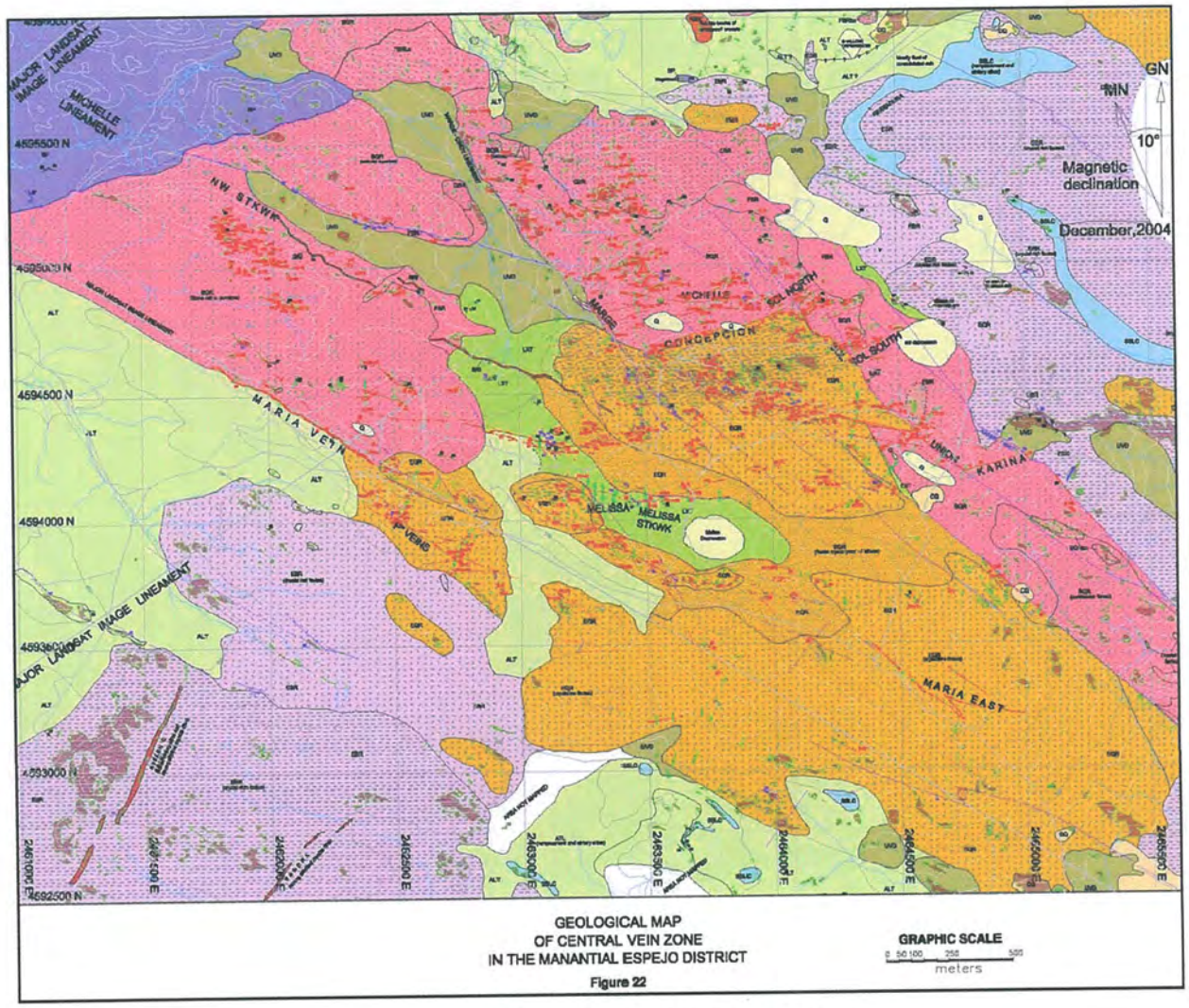


Figure 22 Geological Map

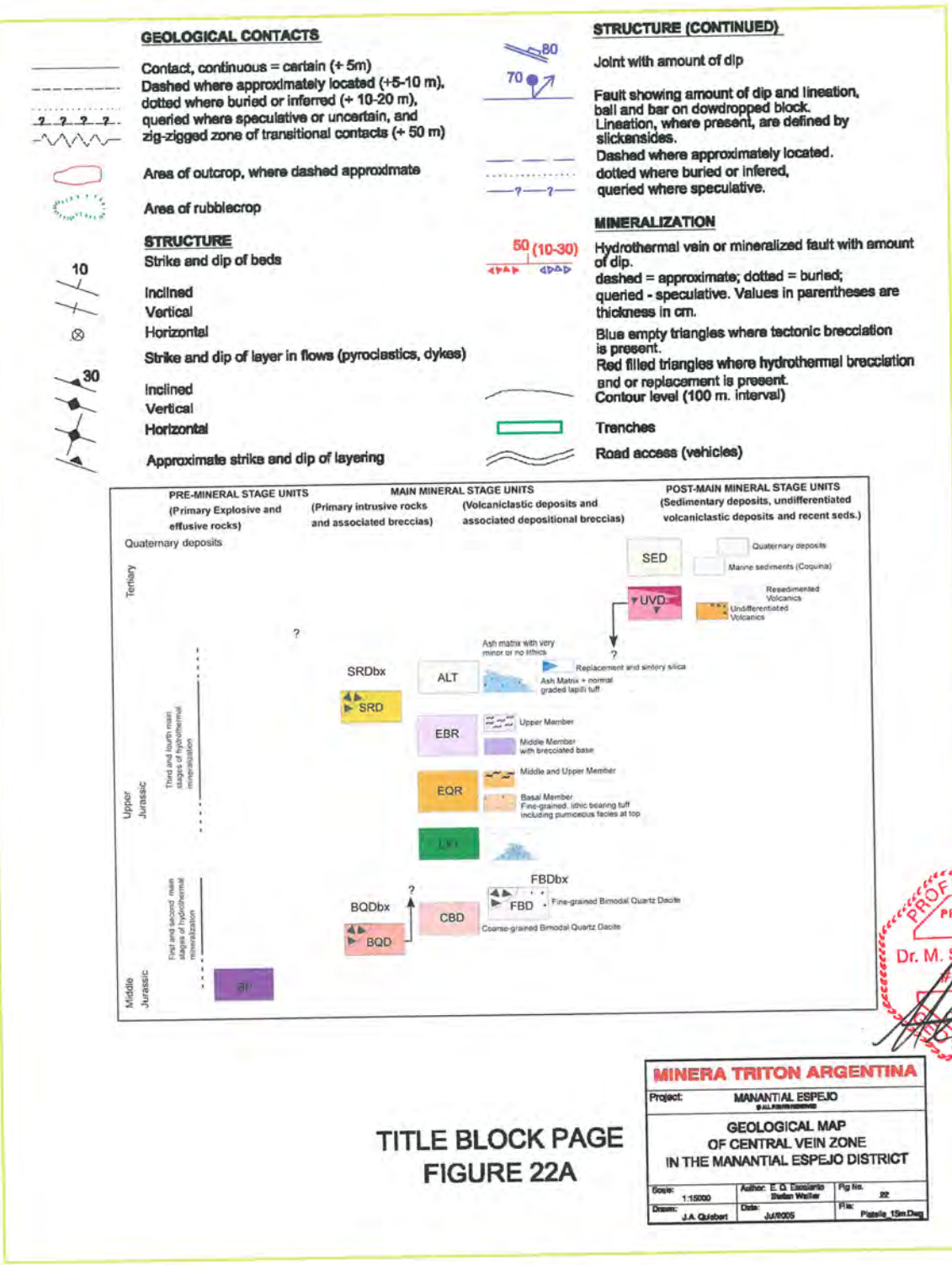


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FIGURE 22A

Figure 22A Title Block Page

MANANTIAL ESPEJO QUALIFIED PERSONS

APPENDIX A

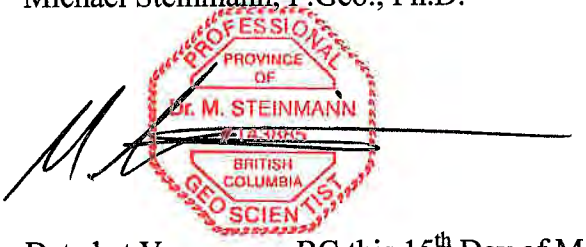
CERTIFICATE OF QUALIFIED PERSON

I, Dr. Michael Steinmann, P.Geo., Ph.D., of Pan American Silver Corp., 625 Howe Street, Suite 1500, Vancouver, British Columbia, Canada V6C 2T6

do hereby certify that:

1. I graduated with a Master's of Science in Geology from the University of Zurich in 1993. In addition, I earned a Doctor of Natural Science in Geology from the Swiss Federal Institute of Technology, Zurich, Switzerland.
2. I am a Professional Geoscientist in good standing in the State of British Columbia in the areas of Mining Geology and Exploration.
3. I am currently employed as Senior Vice President Geology & Exploration for Pan American Silver Corp.
4. I have worked as a Geologist for a total of thirteen years since my graduation from the University of Zurich.
5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
6. Pan American Silver Corp. is a "Producing Issuer" as defined in NI 43-101.
7. I visited the Manantial Espejo Project site from May 26 to 28th, 2004 and from May 16 to 18th, 2005.
8. I am the author of the report dated March 15th , 2006 entitled *NI 43-101 Technical Report for the Manantial Espejo Project.*
9. I am not aware of any material fact or change that has not been disclosed in the documentation provided by Pan American Silver Corporation, which is therefore not reflected in our technical report.
10. National Instrument 43-101 have been read and our report has been prepared in accordance with the requirements specified therein.

Michael Steinmann, P.Geo., Ph.D.



Dated at Vancouver, BC this 15th Day of March 2006.

Michael Steinmann *P.Geo., Ph.D.*
Pan American Silver Corp.
1500 – 625 Howe Street
Vancouver, BC, Canada V6C 2T6
Phone: (604) 684 1175
Fax: (604) 684 0147
Email: msteinmann@panamericansilver.com

CONSENT of QUALIFIED PERSON

TO: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valeurs mobilieres du Quebec
Nunavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

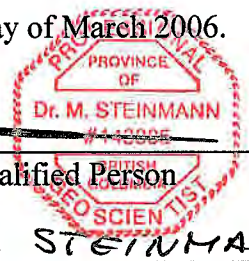
AND TO: PAN AMERICAN SILVER CORPORATION

I, *Michael Steinmann* do hereby consent to the public filing of the technical report for Pan American Silver Corporation titled *NI 43-101 Technical Report for the Manantial-Espejo Project* and dated March *15* of 2006 (the "Technical Report") with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and any extracts from, or a summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of, Volume II of "Manantial-Espejo Feasibility Study" by M3 Engineering & Technology Corp.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated this 15 day of March 2006.



Signature of Qualified Person

MICHAEL STEINMANN

Print name of Qualified Person

Michael Steinmann
Curriculum Vitae

Personal:

Address: 3196 Robinson Road
North Vancouver BC
Canada V7J 3E9
(604) 985 8985
msteinmann@panamericansilver.com

date of birth 24 February 1966
nationality Swiss

Career Progression:

November 2005 – present Senior Vice President Geology & Exploration,, Pan Amercian Silver Corp., Vancouver

- Responsible for all geological aspects of Pan American Silver Corp. production, exploration and projects

March 2004 – October 2005 Vice President Geology-Operations and Projects, Pan Amercian Silver Corp., Vancouver

- Responsible for all geological aspects of Pan American Silver Corp. production and projects

July 2000 – Feb. 2004 Manager of Geology, Glencore Peru, Lima

- Head of the geology departments of the Glencore operations in Peru; Iscaycruz, Yauliyacu and Perubar, with 52 employees (16 geologists, 10 junior geologists, 26 support staff).
- Supervisor of over 40,000 m of diamond drilling per year, responsible for the geological quality control of 8,800 tones of underground production per day and for the exploration inside and around the mine sites. Increased reserves in Peru by 14 Mio tones in the last three years.
- Involved in long term mine planning for the three Peruvian operations.
- Evaluation of 75 base metal mines and projects (geology, reserves, economical situation) in South and Central America, Europe and Asia for the acquisition and trading departments of Glencore.

Sept.1998 - June 2000 Senior Geologist, Glencore Peru, Lima

- Responsible for the generation and supervision of exploration projects in the Glencore base metal operations (Peru), based on structural interpretations, geochemical and geophysical (IP, MAG, EM) surveys as well as underground and surface diamond drilling.
- Reserves mined during this period have been replaced in each operation.
- Involved in production quality control and implementation of new dilution control and sampling methods and supervision of an extensive petrographical and metallurgical study.

June-August 1998 Consulting Exploration Geologist, Cominco Chile Ltda. Santiago, Chile

- Responsible for detailed surface and underground mapping in a sediment hosted copper project in Northern Chile.
- Performed outcrop and underground sampling for geochemical analysis and logged 2000m of diamond drill cores.

1997- March 98 Exploration Geologist, Rio Tinto Mining and Exploration Ltd. Antofagasta, Chile

- Responsible for regional and detailed study of the Monica (II Region) and Vinchuca (III Region) projects. Based on structural, geological, mineralisation and alteration mapping.

- Co-supervisor of RC drilling, open pit and outcrop sampling programs
- Involved in the target generation for the exploration program 1998 by performing structural interpretations of TM + MMI satellite images and aerial photographs of Northern Chile.

1994-1997 ***Ph.D. in Geology at the Swiss Federal Institute of Technology (ETH), Zürich***

- Used variety of techniques and extensive field work to study the inter-arc basin of Cuenca (ca. 4000 km2) including: geological mapping, structural analysis, remote sensing, geochronology by fission-track on zircons, and clastic sedimentology.

Consulting Projects:

- Fission track age determinations for the PICG/GIMP project (Programa de información cartográphica y geológica) of the British geological survey. The work was part of the BGS mapping project of the Western Cordillera of Ecuador to promote mineral exploration activities in the country.

- Organiser of the first International Workshop on sedimentary basins in Southern Ecuador 29 July - 2 August 1996 (Cuenca, Ecuador) including a 3 day fieldtrip attended by 55 geologists.

Education :

2003-2004	Degree in "Corporate Finance" (PADE Finanzas, Advanced Program of Business Administration, 12 month course), ESAN (Escuela superior de administración y negocios), Lima, Peru
2001	Executive training course: "Accounting and Finance for non specialists" 3 month course, ESAN (Escuela superior de administración y negocios), Lima, Peru
1997	Shortcourse on Hydrothermal Systems in Volcanic Arcs: Origin of and Exploration for Epithermal Gold Deposit, Universidad de Concepción (Chile). Instructor: Dr J.W. Hedenquist, Geological Survey of Japan, Tsukuba, Japan
1994-1997	Ph.D. in Geology, Swiss Federal Institute of Technology, Zürich. Thesis topic: "The Cuenca basin of southern Ecuador: tectono-sedimentary history and the Tertiary Andean evolution". Interarc basin analysis and reconstruction of thermotectonic events through fission-track age determinations. Advisors: Prof. Daniel Bernoulli, Dr. Wilfried Winkler, Dr. Diane Seward, Zürich and Prof. Martin Burkhard, Neuenburg
1993	M.Sc. in Geology, University of Zürich, Thesis topic: Intermontane basin analysis. Advisors: Prof. Daniel Bernoulli, Dr. Wilfried Winkler, Dr. Mary Ford
1987	Matura (A-level) in economics, Kantonsschule Wetzikon, Switzerland.

Languages:	German:	native speaker
	English:	fluent, written and spoken
	Spanish:	fluent, written and spoken
	French:	everyday competence

CERTIFICATE OF QUALIFIED PERSON

I, Martin Wafforn, P.Eng, of Pan American Silver Corp., 1500-625 Howe St., Vancouver, British Columbia, Canada V6C 2T6.

do hereby certify that:

1. I graduated with a degree in Bachelor's of Science in Mining from Camborne School of Mines in Cornwall, England in 1980.
2. I am a Professional Engineer in good standing in the Province of British Columbia in the areas of Mining engineering. I am a Chartered Engineer in good standing in the United Kingdom.
3. I am currently employed as Director of Mine Engineering for Pan American Silver Corp.
4. I have worked as an engineer in the mining industry for a total of twenty five years since my graduation from Camborne School of Mines.
5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
6. Pan American Silver Corp. is a "Producing Issuer" as defined in NI 43-101.
7. I visited the Manantial Espejo Project site from May 26 to 28th, 2004 and from April 16 to 18th, 2005.
8. I was a co-author for the March 15th, 2006 report entitled *NI 43-101 Technical Report for the Manantial Espejo Project*.
9. I am not aware of any material fact or change that has not been disclosed in the documentation provided by Pan American Silver Incorporated, which is therefore not reflected in the technical report.
10. National Instrument 43-101 has been read and the report has been prepared in accordance with the requirements specified therein.

Martin G. Wafforn, P.Eng.

Reg. No. 22636

Dated at Vancouver, British Columbia this 15th Day of March 2006.

Martin G. Wafforn P.Eng.
Pan American Silver Corp.
1500 – 625 Howe Street
Vancouver, B.C., V6C 2T6, Canada
Phone: (604) 806 3157
Fax: (604) 684 0147
Email: mwafforn@panamericansilver.com

CONSENT of QUALIFIED PERSON

TO: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valeurs mobilieres du Quebec
Nunavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

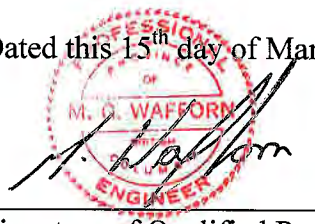
AND TO: PAN AMERICAN SILVER CORPORATION

I, Martin Wafforn P.Eng. do hereby consent to the public filing of the technical report for Pan American Silver Corporation titled *NI 43-101 Technical Report for the Manantial-Espejo Project* and dated March 15th of 2006 (the "Technical Report") with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and any extracts from, or a summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of, Volume II of "Manantial-Espejo Feasibility Study" by M3 Engineering & Technology Corp.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated this 15th day of March 2006.



M. Wafforn Reg No. 22636

Signature of Qualified Person

MARTIN G. WAFFORN

Print name of Qualified Person

Thomas L. Drielick
M3 Engineering & Technology Corporation
2440 W. Ruthrauff Rd., Suite 170
Tucson, Arizona USA 85705
Phone: 520-293-1488 / Fax 520-293-8349
Email: tdrielick@m3eng.com

CERTIFICATE of QUALIFIED PERSON

I, Thomas L. Drielick, do hereby certify that I am a Professional Engineer employed by M3 Engineering & Technology Corporation with an address at 2440 W. Ruthrauff Rd., Suite 170, Tucson, Arizona USA 85705.

I am a Professional Engineer duly registered and in good standing in the State of Arizona with proficiency in Mining Engineering. I graduated with a degree of Bachelor of Science in Metallurgical Engineering from Michigan Technological University in 1970.

I have practiced my profession continually since 1970 and have been involved in the design, and construction of ore beneficiation plants.

As a result of my education, past relevant work experience and qualifications, I fulfill the requirements of a "qualified person" for the purposes of National Instrument 43-101.

I am responsible for the preparation of the technical report titled "NI 43-101 Technical Report for the Manantial-Espejo Project" dated March 10 of 2006 (the "Technical Report"), relating to the flowsheets, process design criteria, and process operating cost estimate for the Manantial-Espejo property located in Santa Cruz, Argentina (the "Property"). I have not visited the Property.

I have had prior involvement with the Property that is the subject of the Technical Report. The nature of my prior involvement is preparation of a "Design, Capital and Operating Cost for Plant and Infrastructure" dated June 2005. I have had no other prior involvement with the Property that is the subject of the Technical Report.

I am independent of Pan American Silver Corporation in accordance with the application of Section 1.4 of National Instrument 43-101.

I have read National Instrument 43-101 and certify that the portions of the Technical Report for which I was responsible as a Qualified Person have been prepared in compliance with that Instrument. I further certify that, as of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at this 20th day of March 2006.

Signature of Qualified Person

Thomas L. Drielick.
Print name of Qualified Person

Thomas L. Drielick
M3 Engineering & Technology Corporation
2440 W. Ruthrauff Rd., Suite 170
Tucson, Arizona USA 85705
Phone: 520-293-1488 / Fax 520-293-8349
Email: tdrielick@m3eng.com

CONSENT of QUALIFIED PERSON

TO: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valeurs mobilieres du Quebec
Nunavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

AND TO: PAN AMERICAN SILVER CORPORATION

I, Thomas L. Drielick, do hereby consent to the public filing of the technical report for Pan American Silver Corporation titled *NI 43-101 Technical Report for the Manantial-Espejo Project* and dated March 10 of 2006 (the "Technical Report") with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and any extracts from, or a summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of, Volume II of "Manantial-Espejo Feasibility Study" by M3 Engineering & Technology Corp.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated this 20th day of March 2006.

Signature of Qualified Person

Thomas L. Drielick
Print name of Qualified Person

CERTIFICATE OF LUIZ CASTRO

As I have been referred to in the Technical Report prepared for NI 43-101 for the Manantial Espejo project in Argentina, I hereby make the following statements:

1. My name is Luiz Castro and I hold the position of Associate and Senior Rock Mechanics Engineer at Golder Associates Ltd. My office address is 2390 Argentia Road, Mississauga, Ontario, L5N 5Z7, Canada.

2. I hold the following academic qualifications:

   - Ph.D. (Rock Mechanics), University of Toronto, 1996
   - M.Sc. (Soil Mechanics), New University of Lisbon, Portugal, 1987
   - B.Sc. (Civil Engineering), Catholic University of Rio de Janeiro, Brazil, 1980

3. I am a registered Professional Engineer in the Province of Ontario (membership number 90517921). As well, I am a member in good standing of several other technical associations and societies, including:

   - The Canadian Institute of Mining, Metallurgy and Petroleum
   - International Society of Rock Mechanics

4. I have worked as a geotechnical engineer since 1980 and as a professional engineer in the Province of Ontario since 1997.

5. I understand that my education, experience and professional registration, fulfill the requirements of a Qualified Person. My work experience includes geotechnical (soil and rock) engineering, field investigations, support design and mining sequence evaluation for underground excavations, 2D and 3D numerical modelling for evaluating excavation, pillar stability and mining sequences and pit slope designs.

6. I was responsible for the preparation of the report titled "*Pit Slope Design for Maria and Karina-Union Veins dated July 2004*" (prepared for Triton Argentina) and technical memorandum titled "*Preliminary Rock Mechanics Study for the Pre-production Underground Mining at Manantial Espejo, dated March 30, 2005*" (prepared for Pan American Silver) both documents prepared for the Manantial Espejo property located in Santa Cruz, Argentina (the "Property"). These reports were used as reference in portions of Section 25 (specifically sub-sections 25.1 and 25.2) of the Technical Report.

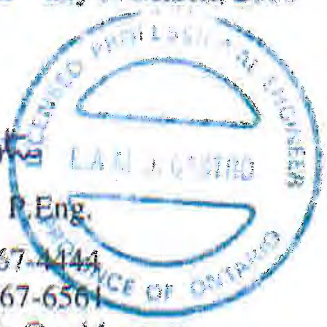
7. I visited the Property in 2001 and 2003.

8. I have had prior involvement with the Property with the preparation of the report titled "*Geotechnical Investigation with Core Orientation at the Veta Maria dated December 2002*". I have had no other prior involvement with the Property that is the subject of the Technical Report.

9. I am independent of Pan American Silver Corporation in accordance with the application of Section 1.4 of National Instrument 43-101.

10. I have read the Technical Report and to the best of my knowledge, the portions of Sections 25.1 and 25.2 of the Technical Report for which the Golder Associates reports were used as reference, reflect the technical information presented in those reference reports.

Dated this 22nd day of March, 2006



Luiz Castro, P.Eng.
Tel: (905) 567-4444
Fax: (905) 567-6561
Email: lcastro@golder.com

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Dr. Conrad E. Huss, P.E., Ph.D.
M3 Engineering & Technology Corporation
2440 W. Ruthrauff Rd., Suite 170
Tucson, Arizona USA 85705
Phone: 520-293-1488 / Fax 520-293-8349
Email: chuss@m3eng.com

CERTIFICATE of QUALIFIED PERSON

I, Dr. Conrad E. Huss, P.E., Ph.D., do hereby certify that I am a Professional Engineer employed as Executive Vice President by M3 Engineering & Technology Corporation with an address at 2440 W. Ruthrauff Rd., Suite 170, Tucson, Arizona USA 85705.

I am a Professional Engineer duly registered and in good standing in the State of Arizona in the areas of Civil and Structural Engineering. I am also registered as a professional engineering in the States of California, Maine, Minnesota, Missouri, Montana, New Mexico, Oklahoma, Oregon, Texas, Utah and Wyoming. I graduated with a degree in Bachelor's of Science in Mathematics and a Bachelor's of Art in English from the University of Illinois in 1963. I graduated with a Master's of Science in Engineering Mechanics from the University of Arizona in 1968. In addition, I earned a Doctor of Philosophy in Engineering Mechanics from the University of Arizona in 1970.

I have practiced my profession continually since 1974 and have been involved in the design, audit and construction of ore beneficiation plants, roads, ancillary facilities, loading complexes, and utility infrastructure.

As a result of my education, past relevant work experience and qualifications, I fulfill the requirements of a "qualified person" for the purposes of National Instrument 43-101.

I am responsible for the preparation of the technical report titled "NI 43-101 Technical Report for the Manantial-Espejo Project" dated March 10 of 2006 (the "Technical Report"), relating to flowsheets, operating cost estimate, capital cost estimates, and concept drawings for the Manantial Espejo property located in Santa Cruz, Argentina (the "Property"). I have not visited the Property.

I have had prior involvement with the Property that is the subject of the Technical Report. The nature of my prior involvement is preparation of a "Design, Capital and Operating Cost for Plant and Infrastructure" dated June 2005. I have had no other prior involvement with the Property that is the subject of the Technical Report.

I am independent of Pan American Silver Corporation in accordance with the application of Section 1.4 of National Instrument 43-101.

I have read National Instrument 43-101 and certify that the portions of the Technical Report for which I was responsible as a Qualified Person have been prepared in compliance with that Instrument. I further certify that, as of the date of this certificate, to the best of my knowledge,

information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at this 20th day of March 2006.

Signature of Qualified Person

Dr. Conrad E. Huss, P.E., Ph.D.
Print name of Qualified Person

Dr. Conrad E. Huss, P.E., Ph.D.
M3 Engineering & Technology Corporation
2440 W. Ruthrauff Rd., Suite 170
Tucson, Arizona USA 85705
Phone: 520-293-1488 / Fax 520-293-8349
Email: chuss@m3eng.com

CONSENT of QUALIFIED PERSON

TO: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valeurs mobilieres du Quebec
Nunavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

AND TO: PAN AMERICAN SILVER CORPORATION

I, Dr. Conrad E. Huss, P.E., Ph.D., do hereby consent to the public filing of the technical report for Pan American Silver Corporation titled *NI 43-101 Technical Report for the Manantial-Espejo Project* and dated March 10 of 2006 (the "Technical Report") with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and any extracts from, or a summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of, Volume II of "Manantial-Espejo Feasibility Study" by M3 Engineering & Technology Corp.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated this 20th day of March 2006.

Signature of Qualified Person

Dr. Conrad E. Huss, P.E., Ph.D.
Print name of Qualified Person

Golder Associates

CERTIFICATE OF DAVID RITCHIE

As I have been referred to in the report prepared for NI 43-101 for the Manantial Espejo project in Argentina, I hereby make the following statements:

1. My name is Dave Ritchie and I hold the position of Associate and Senior Engineer at Golder Associates Ltd. My office address is 2390 Argentia Road, Mississauga, Ontario, L5N 5Z7, Canada.

2. I hold the following academic qualifications:

   M.Eng. (Geotechnical Engineering), University of Western Ontario, London, Ontario, Canada, 2000
   B.Eng. (Civil Engineering), Ryerson Polytechnic University, Toronto, Ontario, Canada, 1995

3. I am a registered Professional Engineer in the Province of Ontario (membership number 90488198). As well, I am a member in good standing of several other technical associations and societies, including:

   The Canadian Dam Association
   Canadian Geotechnical Society

4. I have worked in the field of mine waste engineering since 1995 and as a Professional Engineer in the Province of Ontario since 1998.

5. I understand that my education, experience and professional registration, fulfill the requirements of a Qualified Person. My work experience includes geotechnical (soil mechanics) engineering, field investigations, tailings properties, water management, and dam design.

6. I was responsible for the preparation of the reports titled "*Feasibility Study – Tailings Disposal Facility – Vol. 1*" dated February 2006 and "*Feasibility Study – Tailings Disposal Facility – Vol. 2 Appendices*" dated June, 2005. Both were prepared for Triton Argentina for the Manantial Espejo property located in Santa Cruz, Argentina (the "Property"). These reports were used as reference in portions of the Technical Report, specifically the sub-section Tailings Storage in Section 25.4, based on the Report dated March 16, 2006.

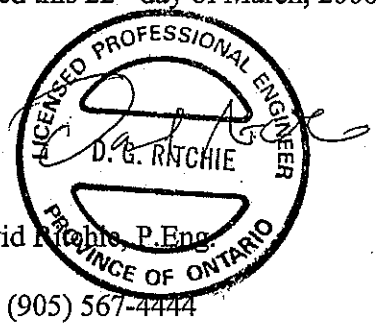
7. I have not visited the Property.

8. I am independent of Pan American Silver Corporation in accordance with the application of Section 1.4 of National Instrument 43-101.

Golder Associates

9. I have read Section 25.4 of the Technical Report and to the best of my knowledge, the portions 25.4 of the Technical Report for which the Golder Associates reports were used as reference, reflect the technical information presented in those reference reports.

Dated this 22rd day of March, 2006



David Ritchie, P.Eng.
Tel: (905) 567-4444
Fax: (905) 567-6561
Email: dritchie@golder.com

Kerry Todd Hamilton, P.Geo., M.App.Sc.
Ground Water International S.A.C.
Calle Trípoli 315, Miraflores
Lima, 18 Perú
Phone: +51 1 241-3041
Fax: +51 1 241-3041
Email: thamilton@gwicorp.com

CONSENT of QUALIFIED PERSON

TO: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valeurs mobilieres du Quebec
Nunavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

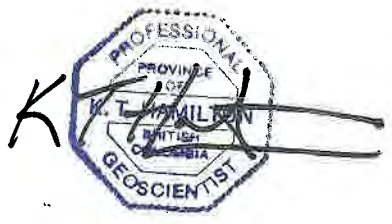
AND TO: PAN AMERICAN SILVER CORPORATION

I, *Kerry Todd Hamilton*, do hereby consent to the public filing of the technical report for Pan American Silver Corporation titled *NI 43-101 Technical Report for the Manantial-Espejo Project* and dated March 10 of 2006 (the "Technical Report") with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and any extracts from, or a summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of, Volume II of "Manantial-Espejo Feasibility Study" by M3 Engineering & Technology Corp.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated this 16th day of March, 2006.



Signature of Qualified Person

KERRY TODD HAMILTON
Print name of Qualified Person

Kerry Todd Hamilton *P.Geo., M.App.Sc.*
Ground Water International S.A.C.
Calle Trípoli 315, Miraflores
Lima, 18 Perú
Phone: +51 1 241-3041
Fax: +51 1 241-3041
Email: thamilton@gwicorp.com

CERTIFICATE of QUALIFIED PERSON

I, *Kerry Todd Hamilton*, do hereby certify that I am a *Professional Geoscientist* employed as *Senior Hydrogeologist* by *Ground Water International* with an address at *Calle Trípoli 315, Miraflores, Lima, 18, Perú.*

I am a *Professional Geoscientist* duly registered and in good standing in the *Province of British Columbia* in the areas of *Hydrogeology*. I am a member of the *Association of Professional Engineers and Geoscientists of British Columbia* and the *International Association of Hydrogeologists*. I graduated with a Bachelor's degree in *Earth Sciences* from the University of *Waterloo* in *1985*. I graduated with a Master's of Applied Science in *Hydrogeology* from the University of *New South Wales* in *1993*.

I have practiced my profession continually since 1984, with a one-year break in 1992-1993 and have been involved in:

- *Mining exploration for mineral exploration companies in Canada and the U.S. (1984-1989);*
- *Hydrogeological and environmental consulting based in Canada, Australia, South Africa and Peru (1989-1992, 1994-present); and*
- *Hydrogeological regulatory work based in Canada (1993-1994).*

As a result of my education, past relevant work experience and qualifications, I fulfill the requirements of a "qualified person" for the purposes of National Instrument 43-101.

I am responsible for the preparation of sections 25.6 "Surface Water" (excluding references to ADR) and "Ground Water" of the technical report titled "NI 43-101 Technical Report for the Manantial-Espejo Project" dated March 10 of 2006 (the "Technical Report"), relating to *site characterization, evaluation of water resources, prediction of mine inflows, drawdown impacts and evaluation of seepage potential from mine waste facilities* for the Manantial Espejo property located in Santa Cruz, Argentina (the "Property"). I visited the Property on *September 15-October 28, November 5-6, 2004 and January 20-February 2, 2005, April 29-May 16, 2005.*

I *have not* had prior involvement with the Property that is the subject of the Technical Report. I have had no other prior involvement with the Property that is the subject of the Technical Report.

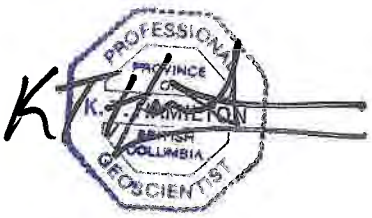
I am independent of Pan American Silver Corporation in accordance with the application of Section 1.4 of National Instrument 43-101.

I have read National Instrument 43-101 and certify that the portions of the Technical Report for which I was responsible as a Qualified Person have been prepared in compliance with that Instrument. I further certify that, as of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Lima, Perú this 16th day of March 2006.

K T Hamilton

Signature of Qualified Person



KERRY TODD HAMILTON

Print name of Qualified Person

Allan Polk *P.Eng.*
Snowden Mining Industry Consultants
550 - 1090 West Pender St.
Vancouver, British Columbia, Canada
Phone: (604) 683-7645
Fax: (604)
Email: apolk@snowdengroup.ca

CONSENT of QUALIFIED PERSON

TO: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valeurs mobilieres du Quebec
Nunavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

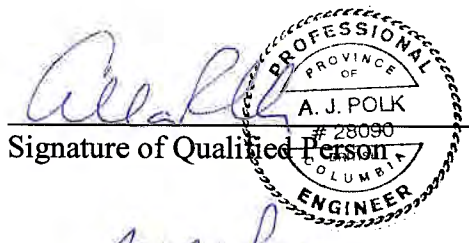
AND TO: PAN AMERICAN SILVER CORPORATION

I, Allan Polk, do hereby consent to the public filing of the technical report for Pan American Silver Corporation titled *NI 43-101 Technical Report for the Manantial-Espejo Project* and dated March 10 of 2006 (the "Technical Report") with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and any extracts from, or a summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of, Volume II of "Manantial-Espejo Feasibility Study" by M3 Engineering & Technology Corp.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated this 17th day of March 2006.



Signature of Qualified Person

ALLAN POLK

Print name of Qualified Person

Allan Polk, *P.Eng.*
Snowden Mining Industry Consultants
550-1090 West Pender St.
Vancouver, British Columbia, Canada
Phone: (604) 683-7645
Fax: (604)
Email: apolk@snowdengroup.ca

CERTIFICATE of QUALIFIED PERSON

I, Allan Polk, do hereby certify that I am a registered professional engineer employed as a Senior Consultant by Snowden Mining Industry Consultants with an address at 550-1090 West Pender St., Vancouver, British Columbia, Canada. V6R 1G8.

I am a registered professional engineer duly registered and in good standing in the province of British Columbia in the area of Mining Engineering. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia (APEG). I graduated with a Bachelor's degree in Mining Engineering from Queens' University in Kingston, Ontario, Canada in 1990.

I have practiced my profession since 1991 and have worked at operating mines as well as having been involved in feasibility study work during this time.

As a result of my education, past relevant work experience and qualifications, I fulfill the requirements of a "qualified person" for the purposes of National Instrument 43-101.

I am responsible for the preparation of underground engineering and cost estimation for the feasibility study related to the Manantial Espejo property, and have provided information to Pan American Silver and M3 Engineering and Technology Corporation for inclusion in the technical report titled "NI 43-101 Technical Report for the Manantial-Espejo Project" dated March 10 of 2006 (the "Technical Report"). Information provided by me has been referenced in the technical report in sections 3.10, 3.11, 3.17, 3.22, 3.23, and 3.25, pertaining to underground mine planning and cost estimation. I have not visited the Manantial Espejo site.

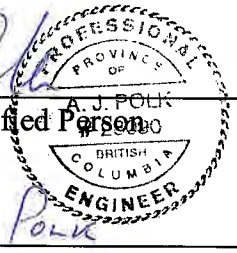
I have not had prior involvement with the Property that is the subject of the Technical Report. I have had no other prior involvement with the Property that is the subject of the Technical Report.

I am independent of Pan American Silver Corporation in accordance with the application of Section 1.4 of National Instrument 43-101.

I have read National Instrument 43-101 and certify that the portions of the Technical Report for which I was responsible as a Qualified Person have been prepared in compliance with that

Instrument. I further certify that, as of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Vancouver, this 17th day of March 2006.



Signature of Qualified Person

ALLAN POLK

Print name of Qualified Person

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CONSENT OF QUALIFIED PERSON

To: British Columbia Securities Commission
Alberta Securities Commission
Saskatchewan Securities Commission
Manitoba Securities Commission
Ontario Securities Commission
Commission des valuers mobilieres du Quebec
Nanavut Legal Registry
Officer of the Administrator, New Brunswick
Nova Scotia Securities Commission
Registrar of Securities, Prince Edward Island
Securities Commission of Newfoundland
Registrar of Securities, Government of the Yukon Territories
Security Registry, Government of the Northwest Territories

And To: Pan American Silver Corporation

I, Michael Lawlor, do hereby consent to the public filing of the Technical Report titled *NI 43-101 Technical Report for Manantial Espejo*, dated March 2006 (the "Technical Report"), with the securities regulatory authorities referred to above.

I further consent to: (i) the publication by the securities regulatory authorities referred to above of the Technical Report and extracts from, or summary of, the Technical Report in the written disclosure being filed; and (ii) the publication of excerpts from, or a summary of *Manantial Espejo Feasibility Study: Open Cut Mining Cost Estimation*, by Snowden Mining Industry Consultants, dated December 2005.

I also confirm that I have read the written disclosure being filed and that it fairly and accurately represents the information in the Technical Report that supports the disclosure.

Dated 21 March, 2006

Michael Lawlor

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CERTIFICATE of QUALIFIED PERSON

I, Michael Lawlor, do hereby certify that:

1. I am the Division Manager, Mining employed by Snowden Mining Industry Consultants of 87 Colin Street, West Peth, Western Australia 6005.

2. I graduated with the following degrees:
   - Graduate Certificate in Project Management – Curtin University, 2005
   - Graduate Certificate in Mineral Economics – Western Australian School of Mines, 1998
   - MEngSc in Mining Geomechanics – James Cook University, 1993
   - BEng(Hons) in Mining Engineering – Western Australian School of Mines, 1985

3. I hold the following professional qualifications:
   - Member of the Australasian Institute of Mining and Metallurgy (MAusIMM)
   - Member and Chartered Professional Engineer of the Institution of Engineers, Australia (MIEAust, CPEng)

4. I have worked as a professional mining engineer for a total of twenty years since my graduation. My experience is primarily in mining and geotechnical engineering and I have worked on scores of consulting assignments in Australia, and also in Indonesia, New Zealand, Central Africa and the former Soviet Union. My expertise is in open pit and underground mine planning and design, mine valuations and project audits, rock slope and underground geotechnical engineering, mining feasibility studies at all levels, and project management.

5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, that I fulfil the requirements to be a "qualified person" for the purposes of NI 43-101.

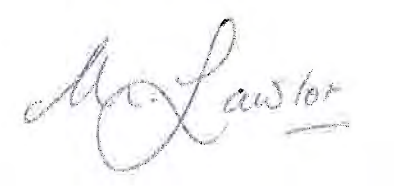
6. Whilst in the employ of Snowden Mining Industry Consultants, I reviewed the preparation for Pan American Silver Corp., of open cut mining cost estimates for the Manantial Espejo Feasibility Study. The title of the Snowden document in which these estimates are reported is "Manantial Espejo Feasibility Study: Open Cut Mining Cost Estimation", dated December 2005. Certain content from this Snowden document has been used for the preparation of Sections 3.22, 3.23, 25.9 and 25.10 of the Technical Report titled "NI 43-101 Technical Report for Manantial Espejo", dated March 2006. This content relates to open pit mining equipment productivity estimates, and open pit mine operating and capital cost estimates.

7. I have read NI 43-101 and Form 43-101F1, and certify that the sections of the Technical Report for which I was responsible as a qualified person have been prepared in compliance with that instrument and form. I further certify that I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.

8. I have not had prior involvement with the property that is the subject of the Technical Report and I am independent of the issuer of the Technical Report, in accordance with the application of section 1.4 of NI 43-101.

9. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them for regulatory purposes, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 21th Day of March, 2006.



Michael Lawlor

MANANTIAL ESPEJO RESOURCE ESTIMATE COMPOSITES

APPENDIX B

Assay Composite Listing - Maria Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Main	DDH-001	62360.55	94247.46	353.31	28.78	41.52	12.74	40	-60	179	3.74
Maria Main	DDH-004	62222.07	94327.11	325.55	55.62	68.09	12.48	40	-58	121	1.11
Maria Main	DDH-007	61942.57	94477.70	305.78	75.66	81.17	5.51	33	-52	908	13.92
Maria Main	DDH-008	62032.17	94436.31	291.72	93.83	105.00	11.17	29	-51	28	1.45
Maria Main	DDH-009	62200.95	94323.42	302.03	88.21	92.74	4.53	33	-52	48	0.29
Maria Main	DDH-010	62286.97	94265.55	292.39	98.95	107.82	8.87	34	-51	28	0.67
Maria Main	DDH-011	62362.50	94207.40	290.69	102.49	117.78	15.30	31	-51	33	1.47
Maria Main	DDH-013	62463.28	94167.96	302.35	103.88	106.87	2.99	36	-52	16	0.19
Maria Main	DDH-014	62334.68	94253.46	325.89	60.03	76.51	16.47	34	-49	51	1.63
Maria Main	DDH-015	61979.08	94443.02	282.54	95.20	107.61	12.41	30	-56	200	0.73
Maria Main	DDH-016	61957.04	94407.88	233.62	136.20	149.43	13.23	30	-66	45	0.85
Maria Main	DDH-017	61960.13	94508.30	353.11	27.00	30.39	3.39	33	-50	73	0.44
Maria Main	DDH-018	62045.17	94456.75	351.29	27.15	39.47	12.32	31	-50	112	1.02
Maria Main	DDH-019	61994.43	94470.83	322.98	55.94	68.78	12.84	30	-50	122	0.30
Maria Main	DDH-020	62297.52	94292.41	347.94	36.94	48.66	11.72	30	-52	47	0.50
Maria Main	DDH-021	62036.08	94343.89	206.20	165.88	175.44	9.56	31	-71	55	0.23
Maria Main	DDH-022	61896.97	94400.70	197.23	160.30	172.39	12.09	0	-90	640	0.54
Maria Main	DDH-023	62144.54	94237.01	178.02	185.00	196.29	11.29	264	-89	580	0.62
Maria Main	DDH-024	62046.64	94275.74	141.60	223.42	233.76	10.34	252	-87	81	0.17
Maria Main	DDH-025	62165.83	94261.47	220.33	153.87	166.78	12.91	35	-67	157	1.30
Maria Main	DDH-026	61826.80	94477.80	272.54	92.28	94.58	2.30	34	-71	36	0.20
Maria Main	DDH-027	61811.27	94449.55	238.15	119.60	125.52	5.92	157	-88	98	0.15
Maria Main	DDH-028	62089.87	94342.71	242.66	122.89	136.31	13.42	292	-89	19	1.06
Maria Main	DDH-029	62310.26	94201.82	249.57	121.61	139.77	18.16	42	-71	79	6.54
Maria Main	DDH-034	62449.46	94138.42	255.82	121.70	136.36	14.66	151	-90	10	0.09
Maria Main	DDH-035	62537.08	94098.47	242.54	147.18	156.12	8.94	33	-70	40	1.84
Maria Main	DDH-041	62270.74	94143.66	159.42	217.70	221.09	3.39	38	-74	22	0.02
Maria Main	RDH-006	62014.31	94451.95	309.91	65.21	76.45	11.24	33	-60	97	0.73
Maria Main	RDH-009	61946.34	94456.01	274.87	92.12	101.33	9.21	34	-73	537	7.35
Maria Main	RDH-014	62490.98	94183.04	331.94	64.12	75.40	11.28	34	-50	123	1.33
Maria Main	RDH-020	62512.11	94164.42	323.47	65.04	73.50	8.46	31	-64	104	11.09
Maria Main	RDH-021	62556.51	94142.13	314.83	74.95	80.50	5.55	29	-65	17	0.15
Maria Main	T-001	62518.22	94065.28	205.67	184.11	195.27	11.16	35	-71	172	3.27
Maria Main	T-002	62546.88	94119.95	273.50	116.85	120.90	4.05	34	-70	29	0.30
Maria Main	T-003	62497.53	94118.20	249.84	156.10	161.23	5.14	36	-58	98	2.13
Maria Main	T-004	62500.94	94146.85	287.66	111.84	116.49	4.65	28	-59	43	0.89
Maria Main	T-005	62397.81	94068.53	144.42	233.96	242.55	8.59	172	-88	80	0.67
Maria Main	T-006	62445.22	94145.68	263.35	134.07	142.67	8.60	31	-61	76	0.67
Maria Main	T-007	62471.64	94188.11	349.44	36.98	45.72	8.74	35	-61	35	0.17
Maria Main	T-008	62415.01	94200.92	334.91	52.30	58.32	6.02	27	-61	309	1.69
Maria Main	T-009	62400.33	94183.35	280.90	116.66	125.13	8.47	26	-56	47	1.84
Maria Main	T-010	62384.63	94156.05	240.92	151.16	160.41	9.25	26	-64	37	0.29
Maria Main	T-011	62299.78	94109.46	147.68	218.77	234.89	16.13	303	-88	95	0.38
Maria Main	T-012	62350.40	94192.74	254.86	136.55	152.26	15.71	29	-56	188	2.30
Maria Main	T-013	62326.80	94147.99	202.93	164.40	182.30	17.90	0	-90	133	1.18
Maria Main	T-014	62371.95	94224.43	334.71	45.53	61.07	15.54	31	-59	77	5.22
Maria Main	T-015	62317.90	94231.76	282.44	93.61	104.41	10.79	30	-70	33	0.98
Maria Main	T-016	62285.21	94177.00	206.49	170.68	179.73	9.05	30	-70	41	0.42
Maria Main	T-017	62246.51	94220.59	229.48	146.10	157.27	11.17	21	-67	39	4.09
Maria Main	T-018	62241.59	94200.11	186.94	183.19	189.41	6.21	25	-80	57	0.26
Maria Main	T-019	62457.05	94072.80	182.45	208.28	218.40	10.11	21	-69	334	10.50
Maria Main	T-020	62588.02	94036.59	202.46	195.36	199.84	4.48	53	-68	10	0.06
Maria Main	T-021	61928.52	94363.73	159.63	207.64	215.35	7.71	26	-75	203	0.15
Maria Main	T-022	61992.70	94363.81	206.88	156.16	180.68	24.52	32	-71	76	1.29

Assay Composite Listing - Maria Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Main	T-023	61907.27	94425.18	238.04	119.70	134.68	14.98	3	-87	115	0.88
Maria Main	T-024	61925.36	94454.67	268.61	96.24	103.33	7.09	14	-88	312	8.67
Maria Main	T-025	61850.63	94428.76	223.70	134.35	142.28	7.93	87	-89	73	1.25
Maria Main	T-026	61867.73	94462.11	264.99	102.89	108.86	5.96	30	-66	128	0.23
Maria Main	T-027	61815.60	94559.15	331.44	38.56	42.35	3.79	31	-61	62	0.17
Maria Main	T-028	62003.41	94484.99	352.05	21.52	37.58	16.07	31	-60	194	2.20
Maria Main	T-029	62186.57	94304.91	270.88	99.96	111.21	11.25	0	-90	99	0.77
Maria Main	T-030	62207.51	94347.14	326.57	57.20	63.67	6.47	29	-59	61	0.30
Maria Main	T-031	62156.27	94341.10	276.59	94.43	105.64	11.21	42	-88	56	0.45
Maria Main	T-032	62178.14	94382.85	356.56	24.46	35.33	10.86	26	-60	39	1.69
Maria Main	T-033	62131.55	94306.65	233.19	134.51	146.97	12.46	16	-79	125	5.15
Maria Main	T-035	62116.79	94269.18	187.98	177.15	192.46	15.31	30	-79	93	0.59
Maria Main	T-036	62256.44	94319.90	344.50	44.50	49.83	5.33	33	-52	66	1.46
Maria Main	T-037	62079.04	94418.64	334.41	42.23	48.94	6.71	31	-65	121	0.22
Maria Main	T-038	62203.58	94231.02	209.70	153.78	169.64	15.87	30	-80	108	4.99
Maria Main	T-039	62217.78	94264.62	257.63	117.85	139.09	21.24	26	-60	210	6.50
Maria Main	T-040	62174.81	94184.13	138.91	220.73	235.58	14.85	0	-89	99	0.86
Maria Main	T-042	62116.13	94381.44	306.33	61.02	79.49	18.47	27	-86	94	2.84
Maria Main	T-043	62126.35	94398.67	331.61	47.09	54.81	7.73	31	-62	47	0.78
Maria Main	T-044	62067.03	94398.83	290.14	81.34	89.23	7.89	30	-75	39	0.56
Maria Main	T-045	62044.22	94369.72	242.00	127.66	135.49	7.83	19	-75	100	0.85
Maria Main	T-046	62012.47	94412.30	251.87	121.13	132.58	11.45	25	-65	127	1.32
Maria Main	T-047	62043.73	94450.03	316.69	67.51	80.63	13.12	34	-48	78	0.30
Maria Main	T-048	61962.45	94314.42	133.15	224.05	240.77	16.72	203	-89	24	0.06
Maria Main	T-049	61877.64	94373.68	162.49	193.12	206.30	13.18	157	-89	64	0.11
Maria Main	T-050	61827.88	94387.39	170.83	186.31	192.04	5.73	276	-89	100	0.10
Maria Main	T-051	61782.89	94401.97	180.86	175.36	178.83	3.47	203	-88	11	0.03
Maria Main	T-052	61841.20	94502.47	297.70	66.97	70.39	3.42	34	-79	112	1.71
Maria Main	T-053	62109.87	94185.33	103.18	258.59	264.03	5.44	292	-88	53	0.29
Maria Main	T-054	62273.80	94248.26	270.36	128.91	145.83	16.92	30	-46	106	2.49
Maria Main	T-055	62338.64	94263.79	355.97	30.89	38.81	7.92	32	-48	123	9.43
Maria Main	T-056	62001.07	94298.61	136.81	224.99	236.66	11.67	302	-88	98	0.13
Maria Main	T-057	62473.37	94194.16	365.43	20.86	27.40	6.54	29	-60	52	0.17
Maria Main	T-058	62427.10	94218.75	371.48	14.04	20.91	6.87	25	-59	180	4.06
Maria Main	T-060	62380.76	94130.22	205.11	178.05	182.63	4.58	35	-74	22	0.20
Maria Main	T-061	62423.64	94119.92	217.75	172.10	177.11	5.01	25	-72	69	0.35
Maria Main	T-062	62418.65	94100.08	193.39	187.13	199.10	11.98	36	-78	391	2.84
Maria Main	T-063	62550.86	94037.14	179.59	211.19	221.08	9.88	27	-69	124	0.90
Maria Main	T-064	62544.08	94061.34	208.00	189.67	197.15	7.49	35	-65	35	0.64
Maria Main	T-065	62338.09	94204.62	266.12	118.73	129.09	10.36	35	-61	133	3.79
Maria Main	T-066	62281.65	94227.77	253.80	127.80	142.36	14.56	23	-61	80	0.74
Maria Main	T-067	62249.46	94251.69	256.06	124.94	138.22	13.27	33	-65	148	7.75
Maria Main	T-068	62325.49	94177.19	236.02	142.41	158.48	16.07	34	-67	202	3.44
Maria Main	T-069	62213.95	94247.68	238.25	138.67	161.71	23.04	30	-59	132	5.56
Maria Main	T-070	62217.03	94221.49	208.95	166.70	183.36	16.65	23	-65	186	6.38
Maria Main	T-071	62186.94	94208.35	170.05	211.10	217.83	6.73	27	-66	597	1.33
Maria Main	T-072	62180.48	94233.48	196.03	181.94	188.34	6.40	33	-66	479	0.96
Maria Main	T-073	62083.00	94376.99	275.09	109.66	117.88	8.22	28	-56	295	0.82
Maria Main	T-074	61916.03	94406.21	218.32	159.57	171.14	11.57	20	-61	73	5.53
Maria Main	T-075	61918.66	94379.87	181.16	196.75	203.11	6.35	29	-65	183	0.14
Maria Main	T-076	61870.22	94400.51	194.16	170.95	181.77	10.82	34	-71	111	0.68
Maria Main	T-077	61878.27	94421.44	219.63	150.20	160.39	10.20	26	-66	412	9.15
Maria Main	T-078	62075.00	94310.35	202.05	166.06	180.06	13.99	33	-76	35	0.22
Maria Main	T-079	62520.93	94087.85	221.94	168.07	175.94	7.87	28	-72	203	5.07

Assay Composite Listing - Maria Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Main	T-080	62478.28	94098.46	220.02	182.95	185.47	2.52	32	-62	65	0.24
Maria Main	T-081	62504.91	94049.15	174.51	212.33	223.50	11.16	31	-71	283	0.43
Maria Main	T-082	62633.89	94070.24	263.35	121.10	131.15	10.06	30	-70	43	0.49
Maria Main	T-084	62487.08	94073.16	194.30	200.15	207.27	7.12	30	-68	55	0.34
Maria Main	T-085	62426.41	94064.29	155.27	236.17	242.16	5.98	28	-69	557	3.31
Maria Main	T-103	62483.25	94024.05	128.16	255.09	262.77	7.68	23	-77	104	0.40
Maria Main	T-104	62514.13	93977.54	95.02	287.44	294.30	6.86	24	-76	101	0.06
Maria Main	T-105	61861.90	94490.38	288.55	87.35	91.27	3.92	29	-56	109	1.75
Maria Main	T-106	61887.55	94530.91	348.12	28.31	34.08	5.77	28	-46	185	2.77
Maria Main	T-107	61935.18	94515.72	348.70	31.77	35.67	3.90	31	-46	126	0.96
Maria Main	T-108	61924.91	94499.37	325.63	57.46	59.86	2.40	30	-47	63	0.16
Maria Main	T-109	61910.29	94472.71	287.41	91.97	97.98	6.01	31	-54	271	7.16
Maria Main	T-110	61981.18	94493.74	351.58	24.79	39.81	15.02	29	-47	442	0.77
Maria Main	T-111	61966.70	94471.21	306.95	75.69	81.82	6.13	28	-52	355	8.83
Maria Main	T-112	62025.56	94470.59	361.05	16.78	30.36	13.58	30	-45	119	0.60
Maria Main	T-113	62241.86	94346.34	364.66	23.72	32.42	8.70	28	-45	39	1.47
Maria Main	T-114	62361.62	94254.45	369.61	14.93	26.75	11.82	32	-45	161	8.71
Maria Main	T-115	62352.12	94240.52	329.61	54.86	71.37	16.51	28	-51	163	3.99
Maria Main	T-116	62383.82	94241.51	375.00	7.90	22.58	14.68	30	-45	265	10.60
Maria Main	T-117	62379.17	94233.75	354.64	31.60	44.45	12.86	30	-46	92	3.77
Maria Main	T-118	62397.90	94219.23	349.57	40.77	50.48	9.71	28	-46	62	1.54
Maria Main	T-190	62607.84	94029.04	199.38	191.11	196.58	5.47	29	-71	23	0.16
Maria Main	T-194	62451.60	94209.96	385.68	0.53	3.60	3.06	31	-45	24	0.06
Maria Main	T-195	62425.21	94223.81	378.34	7.45	16.01	8.56	30	-46	183	1.50
Maria Main	T-196	62406.15	94231.53	379.71	3.51	16.15	12.64	31	-44	279	3.84
Maria Main	T-197	62382.90	94242.55	376.73	5.60	19.94	14.34	30	-45	351	7.15
Maria Main	T-198	62363.11	94256.63	373.88	8.53	23.65	15.12	31	-44	284	2.98
Maria Main	T-199	62342.66	94271.22	375.12	9.34	17.49	8.16	30	-45	143	1.54
Maria Main	T-200	62323.20	94286.87	373.57	10.19	20.46	10.27	30	-45	152	0.50
Maria Main	T-201	62302.66	94302.23	373.04	10.63	23.33	12.71	30	-45	53	3.21
Maria Main	T-202	62283.46	94319.80	370.20	16.65	26.91	10.26	30	-45	93	2.77
Maria Main	T-203	62263.72	94333.82	370.98	16.29	25.69	9.40	30	-45	96	2.08
Maria Main	T-204	62243.57	94347.32	374.64	10.02	23.37	13.35	30	-44	72	1.42
Maria Main	T-205	62223.44	94365.20	373.67	12.38	21.47	9.09	30	-45	80	8.28
Maria Main	T-206	62201.90	94376.70	373.70	10.32	20.78	10.47	30	-45	88	0.67
Maria Main	T-207	62180.16	94389.49	374.63	7.98	18.60	10.62	31	-45	31	3.80
Maria Main	T-208	62160.42	94404.45	371.51	9.44	23.00	13.56	30	-45	53	0.76
Maria Main	T-209	62138.47	94417.45	371.35	9.48	19.95	10.47	30	-45	80	0.49
Maria Main	T-210	62114.90	94425.04	373.06	6.61	15.46	8.84	30	-45	89	0.98
Maria Main	T-211	62089.88	94434.51	373.41	6.30	12.41	6.11	30	-45	8	1.24
Maria Main	T-212	62070.69	94450.16	374.55	4.39	13.53	9.14	29	-45	123	0.63
Maria Main	T-213	62051.89	94468.57	368.77	9.27	23.93	14.66	29	-45	111	0.88
Maria Main	T-214	62028.81	94480.92	373.17	6.06	15.03	8.97	29	-45	60	0.33
Maria Main	T-215	62008.82	94490.36	376.12	0.94	10.61	9.67	30	-45	379	2.12
Maria Main	T-216	61986.90	94505.13	373.54	2.39	14.40	12.01	30	-45	349	9.11
Maria Main	T-217	61964.46	94518.12	372.67	4.88	11.05	6.17	30	-45	158	1.21
Maria Main	T-218	61941.81	94527.92	371.42	5.41	9.96	4.55	29	-45	153	1.56
Maria Main	T-219	61918.70	94538.30	369.41	6.34	12.34	6.00	30	-45	124	0.78
Maria Main	T-220	61894.44	94544.29	368.89	5.58	10.57	4.99	30	-45	66	1.01
Maria Main	T-221	61870.67	94553.75	367.63	5.74	9.14	3.40	29	-45	75	0.89
Maria Main	T-222	61848.68	94565.85	366.35	5.92	10.01	4.09	29	-45	75	1.23
Maria Main	T-223	61829.42	94583.76	364.55	8.54	12.69	4.15	30	-45	59	0.34
Maria Main	T-224	61809.90	94597.59	364.20	8.46	13.76	5.30	30	-45	32	0.12
Maria Main	T-225	61800.20	94582.24	343.89	27.45	29.78	2.33	30	-60	55	0.02

Assay Composite Listing - Maria Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Main	T-226	61834.27	94539.90	328.82	42.42	44.91	2.48	32	-61	45	0.02
Maria Main	T-227	61841.83	94553.58	348.45	22.55	26.75	4.20	30	-60	67	0.12
Maria Main	T-228	61790.49	94599.32	362.36	7.82	12.14	4.32	30	-60	28	0.05
Maria Main	T-229	61799.96	94531.81	301.46	67.14	71.32	4.18	30	-61	213	0.77
Maria Main	T-230	61889.72	94489.96	298.19	74.68	78.41	3.73	29	-61	512	4.49
Maria Main	T-231	61911.24	94524.66	347.58	27.41	31.16	3.75	30	-60	54	0.50
Maria Main	T-232	61870.91	94501.32	305.13	66.35	70.70	4.35	31	-61	61	2.36
Maria Main	T-233	61950.74	94493.88	334.04	41.17	46.87	5.70	29	-60	321	0.41
Maria Main	T-234	61972.88	94482.39	325.29	50.84	56.90	6.07	28	-61	305	1.04
Maria Main	T-235	62019.55	94467.48	330.34	45.25	56.29	11.04	25	-65	66	0.42
Maria Main	T-236	62043.16	94451.98	325.18	46.38	64.71	18.33	30	-66	104	0.58
Maria Main	T-237	62056.74	94424.30	310.16	66.89	75.83	8.94	31	-61	38	0.78
Maria Main	T-238	62084.31	94429.08	354.34	27.92	34.39	6.47	30	-47	21	0.41
Maria Main	T-239	62095.52	94395.30	309.57	66.83	77.62	10.80	29	-62	41	0.24
Maria Main	T-240	62133.20	94409.29	351.78	32.90	40.69	7.79	31	-48	85	0.84
Maria Main	T-241	62161.79	94364.44	319.56	59.02	69.32	10.30	26	-62	34	1.31
Maria Main	T-242	62170.98	94375.01	335.07	44.25	55.20	10.95	30	-61	44	0.55
Maria Main	T-243	62215.11	94355.05	347.81	37.53	46.63	9.10	32	-54	28	1.15
Maria Main	T-244	62236.96	94337.22	350.73	36.84	46.92	10.09	24	-48	31	0.88
Maria Main	T-245	62232.37	94287.38	284.49	92.13	107.11	14.98	25	-62	89	2.24
Maria Main	T-246	62248.79	94305.01	320.16	62.10	70.44	8.34	34	-63	52	0.89
Maria Main	T-247	62274.39	94302.18	335.49	47.97	56.26	8.29	32	-61	39	0.50
Maria Main	T-248	62294.51	94286.90	333.37	44.22	62.38	18.16	34	-63	122	1.65
Maria Main	T-249	62306.92	94261.24	311.64	67.26	81.67	14.41	28	-63	51	0.63
Maria Main	T-250	62328.31	94243.58	307.33	71.82	86.25	14.43	31	-63	70	1.12
Maria Main	T-251	62393.87	94210.76	331.33	51.87	63.89	12.01	29	-61	220	3.26
Maria Main	T-252	62422.31	94207.70	354.17	33.03	36.59	3.56	30	-61	111	3.60
Maria Main	T-253	62441.44	94191.59	342.54	45.40	50.87	5.47	29	-62	165	1.11
Maria Main	T-254	62447.11	94201.26	363.42	29.02	31.93	2.91	29	-46	99	0.41
Maria Main	T-255	62538.00	94159.40	335.13	55.66	60.33	4.67	30	-62	732	0.83
Maria Main	T-256	62279.86	94313.41	357.01	28.83	36.26	7.43	30	-60	122	2.24
Maria Main	T-257	61878.37	94519.60	330.84	40.90	46.44	5.54	30	-61	268	10.43
Maria Main	T-282	62346.63	94228.28	305.98	73.39	91.60	18.21	31	-60	78	2.07
Maria Main	T-283	62336.46	94215.49	276.66	108.48	119.06	10.58	28	-60	35	0.45
Maria Main	T-284	62310.14	94167.37	213.53	176.00	186.88	10.88	31	-62	34	0.77
Maria Main	T-285	62373.81	94171.42	250.21	140.50	152.34	11.84	28	-60	58	1.36
Maria Main	T-286	62380.31	94185.50	268.92	121.60	131.78	10.18	28	-60	31	1.52
Maria Main	T-287	62263.36	94193.96	212.99	172.20	184.52	12.32	27	-62	17	0.35
Maria Main	T-288	62387.90	94195.73	293.34	95.73	108.81	13.07	2	-61	80	1.90
Maria Main	T-289	62238.41	94244.04	244.61	137.07	151.57	14.50	30	-59	250	8.66
Maria Main	T-291	61913.92	94485.08	301.45	72.95	77.35	4.40	58	-61	59	0.17
Maria Main	T-303	62277.81	94215.10	239.78	142.75	156.32	13.57	28	-61	115	7.80
Maria Main	T-304	62294.24	94241.03	280.17	97.58	115.04	17.46	29	-61	94	3.41
Maria Main	T-305	62314.15	94272.21	331.35	48.69	64.44	15.75	31	-59	57	0.86
Maria Main	T-306	62318.42	94281.83	352.55	33.73	47.80	14.06	28	-46	148	2.70
Maria Main	T-307	61746.49	94543.20	298.13	70.46	72.68	2.22	28	-60	56	0.08
Maria Main	T-308	61761.17	94568.79	328.28	37.20	40.13	2.93	29	-71	217	0.05
Maria Main	T-309	61889.05	94431.96	247.14	127.62	141.98	14.36	33	-58	419	7.39
Maria Main	T-310	61902.97	94460.47	270.01	106.10	108.75	2.65	30	-60	503	5.69
Maria Main	T-312	61635.32	94564.02	288.70	74.89	78.58	3.69	0	-60	104	0.03
Maria Main	T-316	61932.84	94417.50	238.71	138.03	150.58	12.55	30	-61	36	2.75
Maria Main	T-317	61942.81	94436.52	258.63	119.98	125.90	5.91	28	-60	250	2.02
Maria Main	T-318	62137.40	94276.34	215.20	165.86	178.99	13.13	25	-62	129	2.05
Maria Main	T-319	62148.56	94288.02	236.21	143.23	156.88	13.65	30	-62	433	11.68

Assay Composite Listing - Maria Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole ID	East	North	Elevation (m	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Main	T-320	62160.60	94304.33	257.34	122.28	135.67	13.39	31	-61	595	5.24
Maria Main	T-321	62183.15	94251.53	218.56	164.74	170.61	5.87	29	-62	35	0.15
Maria Main	T-322	62192.20	94268.25	242.78	137.20	148.54	11.34	27	-62	39	2.21
Maria Main	T-323	62254.52	94272.30	276.52	104.84	115.38	10.54	31	-60	99	2.31
Maria Main	T-324	62519.55	94181.61	353.52	41.75	47.01	5.26	27	-47	215	1.55
Maria Main	T-325	61839.38	94457.42	256.19	116.38	122.78	6.40	35	-59	122	0.35
Maria Main	T-326	61952.18	94395.02	215.60	163.76	176.85	13.10	28	-61	55	2.22
Maria Main	T-327	61971.27	94426.80	257.37	118.73	126.66	7.93	32	-62	183	1.19
Maria Main	T-328	62008.25	94384.74	233.92	142.69	161.69	19.01	35	-61	144	4.06
Maria Main	T-329	62003.80	94436.11	285.68	87.37	100.79	13.42	30	-62	42	1.59
Maria Main	T-330	62061.88	94437.50	349.76	26.34	35.63	9.28	33	-59	84	0.84
Maria Main	T-331	62132.67	94357.15	281.69	99.93	107.92	7.99	31	-61	41	0.27
Maria Main	T-332	62150.25	94392.79	340.56	41.98	53.35	11.37	33	-52	46	0.37
Maria Main	T-333	62173.93	94341.56	303.03	76.22	86.22	10.00	30	-62	45	0.38
Maria Main	T-334	62227.50	94231.00	226.69	153.90	168.99	15.09	34	-62	113	7.75
Maria Main	T-335	62267.93	94287.71	301.45	82.96	87.97	5.01	33	-60	36	0.25
Maria Main	T-336	62367.54	94216.42	312.88	65.06	87.40	22.34	28	-60	128	3.54
Maria Main	T-337	62296.83	94193.30	231.27	153.20	166.44	13.24	30	-62	31	3.10
Maria Main	T-338	62432.00	94170.36	291.77	103.30	107.81	4.51	32	-61	58	1.10
Maria Main	T-339	62473.38	94145.76	274.96	122.89	130.79	7.90	33	-61	49	2.06
Maria Main	T-341	62528.99	94145.17	305.48	90.13	95.85	5.72	34	-59	152	0.44
Maria Main	T-350-OC	62443.70	94182.56	320.85	70.99	76.48	5.49	0	-61	41	0.44
Maria Main	T-351-OC	61850.59	94519.16	319.24	50.44	54.47	4.04	15	-65	287	0.48
Maria Main	T-355-MET	61906.50	94412.54	222.04	136.38	150.16	13.78	36	-81	399	2.26
Maria Main	T-356-MET	61937.16	94466.12	289.06	77.53	85.11	7.58	39	-81	667	8.63
Maria Main	T-357-MET	62206.83	94240.60	232.19	122.86	155.54	32.68	282	-89	133	7.99
Maria Main	T-359-MET	62334.79	94258.49	334.18	36.08	64.79	28.71	29	-85	109	2.68
Maria Main	T-360	61659.20	94581.54	306.94	57.32	61.57	4.25	0	-61	189	0.03
Maria Main	T-361	61610.15	94583.47	296.72	65.19	70.76	5.58	0	-60	52	0.06
Maria Main	T-362	61661.42	94548.04	274.43	88.92	94.10	5.18	2	-62	14	0.01
Maria Main	T-389	61657.64	94619.68	335.27	29.92	34.82	4.90	0	-60	28	0.02
Maria Main	T-390	62207.72	94120.88	94.11	298.42	305.89	7.46	41	-67	60	0.06
Maria Main	T-402	62094.02	94309.97	211.91	169.75	183.14	13.39	24	-62	115	0.85
Maria Main	T-403	62467.80	94047.20	151.11	244.08	250.89	6.81	37	-67	114	0.42
Maria Main	T-424	62172.66	94278.23	241.08	135.93	143.46	7.53	30	-67	132	0.66
Maria Main	T-425	62664.22	94019.52	215.92	205.78	208.35	2.57	34	-52	45	0.24
Maria Main	T-455	62367.40	94146.99	222.19	193.04	201.96	8.92	33	-51	201	1.96
Maria Main	T-475	62359.33	94108.94	169.45	208.00	212.58	4.58	23	-85	94	0.09
Maria Main	T-476	62350.01	94129.98	192.11	208.48	215.73	7.25	35	-60	119	0.62
Maria Main	T-484	62388.09	94115.22	190.03	229.96	235.06	5.10	29	-54	30	0.59
Maria Main	T-485	62443.00	94093.11	194.05	196.03	199.08	3.05	35	-73	19	0.13
Maria Main	T-486	62118.09	94334.96	251.59	132.24	143.42	11.18	29	-61	67	0.59
Maria Main	T-487	62311.70	94217.57	267.69	103.48	122.12	18.64	31	-71	289	2.77
Maria Main	T-488	62065.18	94339.07	225.28	152.10	158.18	6.08	31	-68	66	0.32
Maria Main	T-489	62602.95	94126.48	322.07	67.14	74.51	7.37	31	-61	12	0.17
Maria Main	T-519	62433.92	94082.34	179.49	212.45	219.14	6.69	30	-68	823	4.24
Maria Main	T-520	62415.72	94045.23	128.67	259.77	267.46	7.69	34	-70	120	0.06
Maria Main	T-521	62456.93	94056.15	161.24	232.02	241.48	9.45	35	-67	115	0.53
Maria Main	T-522	62406.61	94081.02	162.84	216.62	224.71	8.09	34	-82	77	0.08
Maria Main	T-523	62503.81	94092.97	225.61	170.00	177.21	7.21	34	-66	555	6.63
Maria Main	T-629	61901.00	94505.19	320.10	53.59	57.73	4.14	30	-61	220	0.69
Maria Main	T-630	61890.34	94514.14	326.87	45.81	50.88	5.07	29	-61	212	1.67
Maria Main	T-631	61873.90	94510.62	317.45	53.38	59.58	6.20	31	-61	148	1.96
Maria Main	T-632	61883.87	94524.86	339.78	33.22	39.41	6.19	32	-56	116	5.37

Assay Composite Listing - Maria Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Main	T-633	61868.09	94524.72	333.05	38.63	43.38	4.75	29	-60	52	0.59

Assay Composite Listing - Maria P1 Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria P1	DDH-010	62276.07	94249.39	316.41	69.78	75.10	5.32	34	-51	210	3.74
Maria P1	DDH-011	62338.38	94167.25	348.53	33.56	37.86	4.30	31	-51	29	1.15
Maria P1	DDH-029	62305.03	94196.06	272.18	101.00	112.56	11.56	43	-71	39	8.88
Maria P1	T-001	62489.51	94018.98	357.74	25.98	30.29	4.31	31	-69	282	14.60
Maria P1	T-003	62453.46	94052.55	376.43	7.10	11.66	4.56	31	-57	75	0.88
Maria P1	T-005	62397.70	94068.99	274.82	100.56	115.04	14.48	124	-88	2	0.57
Maria P1	T-006	62410.58	94091.06	376.75	5.59	10.04	4.44	30	-59	21	0.27
Maria P1	T-009	62375.16	94131.76	366.01	12.64	23.84	11.19	26	-56	131	2.66
Maria P1	T-010	62367.39	94119.53	319.86	62.47	71.74	9.28	27	-62	37	3.00
Maria P1	T-012	62337.80	94170.01	293.39	90.32	105.56	15.25	29	-56	20	1.54
Maria P1	T-013	62326.80	94147.99	229.22	129.72	164.40	34.68	0	-90	145	2.38
Maria P1	T-015	62307.24	94213.29	341.02	32.35	40.99	8.63	30	-70	41	0.30
Maria P1	T-016	62284.14	94175.15	212.37	167.22	170.68	3.46	30	-70	12	0.26
Maria P1	T-019	62441.42	94033.94	289.09	95.79	101.73	5.94	23	-68	31	0.24
Maria P1	T-020	62531.04	93988.59	371.12	8.23	18.12	9.90	49	-65	45	0.64
Maria P1	T-054	62268.23	94238.51	282.20	115.25	126.85	11.60	30	-47	52	1.85
Maria P1	T-060	62366.75	94110.20	290.32	87.69	95.69	8.00	35	-74	26	1.10
Maria P1	T-061	62406.43	94085.25	333.62	49.59	55.28	5.68	28	-71	27	0.57
Maria P1	T-062	62404.01	94078.80	323.04	53.45	68.38	14.93	33	-79	26	0.38
Maria P1	T-063	62523.71	93983.85	335.40	36.62	61.85	25.23	27	-69	73	3.56
Maria P1	T-063A	62523.20	93988.72	334.37	41.24	62.48	21.24	20	-65	0	0.00
Maria P1	T-064	62506.90	94003.71	353.40	29.16	36.13	6.97	31	-65	160	13.13
Maria P1	T-065	62325.09	94185.53	307.80	69.67	82.86	13.19	34	-61	36	1.22
Maria P1	T-066	62278.52	94220.53	267.73	110.36	127.79	17.43	24	-61	42	4.21
Maria P1	T-068	62320.72	94170.21	255.55	117.76	140.56	22.80	35	-66	167	6.53
Maria P1	T-080	62442.48	94042.07	343.52	40.12	47.47	7.34	33	-61	28	1.81
Maria P1	T-081	62479.72	94007.21	317.38	62.93	70.86	7.93	31	-72	40	1.86
Maria P1	T-084	62459.10	94023.16	326.69	56.87	62.03	5.16	29	-66	33	0.73
Maria P1	T-119	62544.10	93970.02	339.09	53.70	58.68	4.98	30	-45	43	0.43
Maria P1	T-283	62323.87	94191.68	323.31	52.92	66.88	13.96	27	-60	160	2.09
Maria P1	T-284	62307.56	94163.10	222.90	165.64	176.00	10.36	31	-62	47	1.42
Maria P1	T-285	62356.54	94139.17	313.56	68.13	78.42	10.30	28	-60	61	5.02
Maria P1	T-286	62359.64	94146.13	345.93	32.48	43.06	10.58	28	-60	72	5.77
Maria P1	T-287	62261.67	94190.58	220.09	168.44	172.20	3.76	27	-62	6	0.21
Maria P1	T-303	62274.76	94209.49	251.31	129.97	142.75	12.78	29	-61	34	2.76
Maria P1	T-304	62287.15	94228.25	306.54	69.12	83.22	14.10	29	-61	75	2.27
Maria P1	T-337	62294.22	94188.85	240.98	145.55	152.10	6.55	31	-62	25	6.56
Maria P1	T-358-MET	62376.30	94130.65	366.13	7.23	23.22	15.99	34	-80	132	1.62
Maria P1	T-391	62570.62	93957.15	362.97	22.18	26.48	4.30	32	-45	39	0.60
Maria P1	T-404	62391.60	94108.72	346.41	46.29	51.56	5.27	28	-46	24	0.62
Maria P1	T-405	62428.09	94070.28	347.03	46.36	50.31	3.95	29	-47	31	0.48
Maria P1	T-406	62609.80	93935.15	372.59	7.79	11.40	3.61	31	-45	18	0.49
Maria P1	T-407	62651.46	93909.55	368.89	10.00	13.37	3.37	30	-45	9	0.12
Maria P1	T-425	62606.85	93932.36	348.68	35.83	40.57	4.74	32	-51	26	0.37
Maria P1	T-450	62591.04	93944.06	361.09	22.06	25.91	3.84	30	-50	37	0.44
Maria P1	T-451	62569.69	93953.74	323.89	66.84	72.18	5.34	32	-51	59	2.45
Maria P1	T-452	62509.48	94007.40	380.43	2.64	8.07	5.42	30	-51	22	0.54
Maria P1	T-453	62492.53	94023.98	375.32	9.01	16.06	7.05	30	-51	41	1.57
Maria P1	T-454	62463.52	94028.88	366.05	19.45	23.84	4.40	30	-51	23	0.25
Maria P1	T-455	62353.66	94125.69	253.75	152.80	161.24	8.44	32	-51	34	8.99
Maria P1	T-456	62523.73	93980.72	297.26	99.04	109.62	10.58	31	-51	37	1.86
Maria P1	T-469	62627.60	93917.99	351.63	31.08	35.25	4.18	31	-51	21	0.23
Maria P1	T-470	62605.78	93929.35	321.47	69.41	74.26	4.85	31	-51	26	0.94

Assay Composite Listing - Maria P1 Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria P1	T-471	62585.32	93943.49	331.17	58.19	62.99	4.81	30	-51	24	0.50
Maria P1	T-473	62541.18	93968.43	312.34	83.74	88.21	4.47	32	-50	24	0.82
Maria P1	T-474	62545.31	93975.34	368.22	15.47	20.02	4.55	30	-51	30	0.54
Maria P1	T-475	62356.96	94102.92	236.80	136.68	148.58	11.90	21	-84	11	0.30
Maria P1	T-476	62341.80	94118.16	217.04	180.66	185.99	5.33	34	-60	34	3.46
Maria P1	T-484	62372.31	94085.92	235.75	174.07	177.84	3.77	27	-54	6	0.86
Maria P1	T-485	62421.29	94059.53	319.70	61.24	70.15	8.91	33	-72	32	2.17
Maria P1	T-487	62304.50	94205.79	307.04	65.56	76.65	11.09	32	-71	37	2.72
Maria P1	T-491	62587.69	93944.41	293.64	103.67	108.36	4.69	33	-52	30	1.05
Maria P1	T-492	62629.22	93921.87	370.67	9.14	12.47	3.33	29	-45	24	0.13
Maria P1	T-519	62413.61	94048.12	277.83	106.94	112.48	5.54	32	-67	14	0.05
Maria P1	T-522	62397.82	94067.92	272.30	105.57	114.60	9.03	32	-82	5	0.12
Maria P1	T-523	62467.01	94037.71	376.77	6.17	10.83	4.66	33	-66	46	0.38
Maria P1	T-524	62523.70	93979.84	265.22	129.80	140.22	10.42	36	-56	19	2.47

Assay Composite Listing - Maria P6 Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria P6	T-005	62397.62	94068.85	156.67	219.54	232.46	12.92	125	-88	11	0.04
Maria P6	T-019	62445.04	94042.56	265.82	118.96	128.72	9.75	22	-68	8	0.38
Maria P6	T-060	62367.77	94111.66	284.12	96.01	100.27	4.26	35	-74	16	2.74
Maria P6	T-062	62406.20	94082.16	301.82	75.59	89.44	13.86	33	-79	6	0.84
Maria P6	T-080	62445.14	94046.17	334.83	52.30	55.22	2.92	33	-61	72	16.48
Maria P6	T-081	62482.11	94011.20	303.38	79.23	84.06	4.83	31	-71	13	1.73
Maria P6	T-084	62462.89	94030.08	308.97	77.13	80.58	3.45	29	-66	25	2.20
Maria P6	T-085	62420.10	94052.80	190.34	196.93	206.51	9.58	29	-70	28	6.01
Maria P6	T-103	62479.08	94015.24	170.40	213.00	218.15	5.15	29	-77	8	0.03
Maria P6	T-403	62456.58	94031.74	195.57	195.01	203.17	8.16	35	-67	10	1.74
Maria P6	T-454	62464.41	94030.41	363.91	23.84	25.00	1.16	30	-50	11	0.11
Maria P6	T-475	62358.45	94106.75	195.14	180.58	188.40	7.82	22	-85	38	2.57
Maria P6	T-476	62345.76	94123.91	204.95	195.28	199.29	4.01	35	-60	34	2.32
Maria P6	T-484	62377.72	94096.13	219.93	192.70	198.39	5.69	28	-54	23	1.38
Maria P6	T-519	62419.98	94058.63	247.95	137.00	147.04	10.04	31	-68	9	0.19
Maria P6	T-520	62414.42	94043.27	135.25	253.49	259.77	6.28	34	-70	20	0.05
Maria P6	T-521	62445.11	94039.32	209.92	180.46	187.34	6.88	36	-67	15	4.31
Maria P6	T-522	62402.63	94075.13	213.09	160.24	179.60	19.36	34	-82	13	0.69

Assay Composite Listing - Maria P8 Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria P8	DDH-023	62144.70	94237.03	184.90	182.53	185.00	2.47	259	-89	20	1.49
Maria P8	DDH-025	62163.16	94257.63	231.05	146.00	151.26	5.26	35	-66	131	0.89
Maria P8	DDH-028	62090.44	94342.46	266.63	104.09	107.14	3.05	300	-88	11	0.07
Maria P8	T-017	62242.96	94211.25	253.00	124.24	128.03	3.79	21	-67	111	1.12
Maria P8	T-018	62239.89	94196.56	208.18	163.24	166.14	2.90	26	-79	18	0.51
Maria P8	T-033	62130.48	94302.97	253.05	118.64	122.41	3.77	16	-79	78	2.52
Maria P8	T-038	62201.84	94228.01	229.42	135.28	148.08	12.80	30	-80	132	6.01
Maria P8	T-039	62210.66	94250.03	285.76	92.67	99.31	6.64	26	-60	50	1.15
Maria P8	T-054	62258.68	94221.91	302.37	92.60	93.84	1.24	30	-46	0	0.00
Maria P8	T-067	62237.83	94233.78	296.21	83.53	88.62	5.10	33	-59	91	0.33
Maria P8	T-069	62208.16	94237.66	257.51	125.11	130.34	5.23	30	-59	36	0.83
Maria P8	T-070	62214.47	94215.32	223.26	155.74	162.74	7.00	22	-65	31	0.32
Maria P8	T-071	62184.20	94202.93	183.61	198.65	200.58	1.93	27	-66	16	0.03
Maria P8	T-072	62177.30	94228.57	209.17	164.49	177.03	12.54	33	-66	275	1.17
Maria P8	T-289	62230.28	94229.96	271.67	111.73	113.76	2.03	30	-59	22	0.07
Maria P8	T-319	62146.53	94284.51	244.00	139.55	143.00	3.45	30	-62	182	2.84
Maria P8	T-320	62155.87	94296.45	273.59	109.36	111.25	1.89	31	-60	236	5.30
Maria P8	T-321	62179.30	94244.59	233.50	148.12	153.41	5.29	29	-62	312	5.95
Maria P8	T-322	62187.50	94259.03	262.66	117.39	123.52	6.13	27	-63	342	4.06
Maria P8	T-334	62222.22	94222.74	244.72	137.65	144.19	6.54	32	-61	27	0.20
Maria P8	T-357-MET	62207.32	94240.49	260.84	105.71	115.40	9.69	284	-89	24	0.12
Maria P8	T-402	62092.52	94306.56	219.06	167.01	169.75	2.74	24	-62	24	0.57
Maria P8	T-424	62168.96	94271.88	257.92	119.43	123.21	3.78	30	-66	259	7.39
Maria P8	T-486	62113.37	94326.57	269.16	116.86	118.74	1.88	30	-61	91	4.07

Assay Composite Listing - Maria PM Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria PM	T-119	62547.94	93976.62	331.42	65.75	68.28	2.54	30	-45	29	6.81
Maria PM	T-190	62581.10	93976.78	366.73	15.05	17.93	2.88	28	-70	85	19.53
Maria PM	T-391	62580.35	93972.63	344.44	48.67	52.05	3.39	33	-46	48	8.10
Maria PM	T-406	62623.40	93958.87	344.69	47.77	49.56	1.80	29	-46	15	3.40
Maria PM	T-407	62672.73	93947.26	323.62	73.35	75.31	1.96	28	-47	5	0.07
Maria PM	T-425	62620.66	93954.32	315.96	78.04	81.87	3.84	33	-52	41	10.95
Maria PM	T-449	62726.22	93941.85	346.16	38.75	40.74	1.99	30	-50	4	0.04
Maria PM	T-450	62602.52	93963.74	333.32	58.16	61.67	3.51	30	-51	65	19.34
Maria PM	T-451	62577.94	93966.94	304.68	92.46	96.01	3.55	32	-51	15	0.30
Maria PM	T-469	62647.39	93950.54	304.61	92.52	94.84	2.32	31	-51	21	1.91
Maria PM	T-470	62620.65	93953.60	286.96	115.39	117.71	2.32	31	-50	62	10.21
Maria PM	T-471	62596.79	93962.69	303.42	94.58	97.89	3.31	31	-51	61	6.95
Maria PM	T-472	62600.59	93971.41	358.70	28.16	30.00	1.84	30	-50	84	29.77
Maria PM	T-473	62545.28	93975.04	303.13	96.80	99.26	2.46	32	-50	48	6.50
Maria PM	T-474	62548.88	93981.48	359.57	28.00	29.89	1.89	30	-50	20	3.58
Maria PM	T-490	62650.43	93958.87	358.41	26.62	30.60	3.98	28	-46	16	5.42
Maria PM	T-491	62598.17	93960.68	268.74	136.22	138.88	2.66	33	-52	44	4.18
Maria PM	T-492	62647.76	93954.76	332.63	63.29	65.51	2.23	30	-45	9	4.29

Assay Composite Listing - Maria Ag Enriched Domain

		Mid-Point Coordinates (Truncated)			Drill Depth Interval				Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Defined Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Ag Enriched	DDH-016	61947.37	94391.09	277.50	92.10	97.60	5.50	1.50	30	-66	1	0.00
Maria Ag Enriched	DDH-016	61948.47	94393.00	272.50	97.60	103.00	5.40	1.60	30	-66	2	0.00
Maria Ag Enriched	DDH-016	61950.67	94396.80	262.50	108.40	113.90	5.50	2.60	30	-66	18	0.11
Maria Ag Enriched	DDH-016	61951.77	94398.70	257.50	113.90	119.40	5.50	5.50	30	-66	60	0.11
Maria Ag Enriched	DDH-016	61952.87	94400.59	252.50	119.40	124.90	5.50	5.50	30	-66	35	0.27
Maria Ag Enriched	DDH-016	61953.97	94402.50	247.50	124.90	130.40	5.50	5.50	30	-66	44	0.17
Maria Ag Enriched	DDH-016	61955.07	94404.40	242.50	130.40	135.80	5.40	1.40	30	-66	153	0.26
Maria Ag Enriched	DDH-021	62020.77	94318.40	292.50	76.70	82.00	5.30	1.70	31	-71	148	0.03
Maria Ag Enriched	DDH-021	62021.67	94319.90	287.50	82.00	87.30	5.30	5.30	31	-71	192	0.02
Maria Ag Enriched	DDH-021	62022.57	94321.40	282.50	87.30	92.60	5.30	5.30	31	-71	25	0.01
Maria Ag Enriched	DDH-021	62023.47	94322.80	277.50	92.60	97.90	5.30	5.30	31	-71	32	0.02
Maria Ag Enriched	DDH-021	62024.37	94324.30	272.50	97.90	103.20	5.30	5.30	31	-71	132	0.01
Maria Ag Enriched	DDH-021	62025.17	94325.80	267.50	103.20	108.50	5.30	3.40	31	-71	58	0.09
Maria Ag Enriched	DDH-021	62026.07	94327.30	262.50	108.50	113.80	5.30	1.00	31	-71	4	0.05
Maria Ag Enriched	DDH-021	62026.97	94328.70	257.50	113.80	119.10	5.30	1.90	31	-71	10	0.09
Maria Ag Enriched	DDH-021	62027.87	94330.20	252.50	119.10	124.30	5.20	2.60	31	-71	59	0.15
Maria Ag Enriched	DDH-022	61895.67	94400.09	287.50	73.60	78.60	5.00	0.80	92	-88	129	0.01
Maria Ag Enriched	DDH-022	61895.87	94400.09	282.50	78.60	83.60	5.00	5.00	92	-88	242	0.01
Maria Ag Enriched	DDH-022	61896.07	94400.09	277.50	83.60	88.60	5.00	5.00	81	-88	56	0.05
Maria Ag Enriched	DDH-022	61896.17	94400.09	272.50	88.60	93.60	5.00	5.00	81	-88	22	0.05
Maria Ag Enriched	DDH-022	61896.37	94400.20	267.50	93.60	98.60	5.00	5.00	69	-89	36	0.03
Maria Ag Enriched	DDH-022	61896.47	94400.20	262.50	98.60	103.60	5.00	5.00	69	-89	124	0.20
Maria Ag Enriched	DDH-022	61896.57	94400.30	257.50	103.60	108.60	5.00	5.00	58	-89	37	0.06
Maria Ag Enriched	DDH-022	61896.67	94400.30	252.50	108.60	113.60	5.00	5.00	58	-89	4	0.03
Maria Ag Enriched	DDH-022	61896.77	94400.40	247.50	113.60	118.60	5.00	5.00	46	-89	4	0.04
Maria Ag Enriched	DDH-022	61896.77	94400.40	242.50	118.60	123.60	5.00	2.80	46	-89	7	0.04
Maria Ag Enriched	DDH-023	62146.27	94237.00	307.50	58.70	63.70	5.00	1.10	307	-90	4	0.00
Maria Ag Enriched	DDH-023	62146.27	94237.00	302.50	63.70	68.70	5.00	2.10	298	-90	55	0.00
Maria Ag Enriched	DDH-023	62146.07	94237.09	267.50	98.70	103.70	5.00	1.50	272	-90	12	0.02
Maria Ag Enriched	DDH-023	62145.97	94237.09	262.50	103.70	108.70	5.00	4.30	271	-89	28	0.02
Maria Ag Enriched	DDH-024	62052.57	94276.20	302.50	65.10	70.10	5.00	1.00	305	-89	4	0.01
Maria Ag Enriched	DDH-024	62052.47	94276.30	297.50	70.10	75.10	5.00	5.00	305	-89	44	0.00
Maria Ag Enriched	DDH-024	62052.37	94276.30	292.50	75.10	80.10	5.00	5.00	298	-89	285	0.02
Maria Ag Enriched	DDH-024	62052.27	94276.40	287.50	80.10	85.10	5.00	5.00	298	-89	130	0.01
Maria Ag Enriched	DDH-024	62052.17	94276.40	282.50	85.10	90.10	5.00	5.00	290	-89	85	0.01
Maria Ag Enriched	DDH-024	62052.07	94276.50	277.50	90.10	95.10	5.00	5.00	290	-89	420	0.01
Maria Ag Enriched	DDH-024	62051.97	94276.50	272.50	95.10	100.10	5.00	5.00	282	-89	302	0.01
Maria Ag Enriched	DDH-024	62051.87	94276.50	267.50	100.10	105.10	5.00	4.10	282	-89	310	0.03
Maria Ag Enriched	DDH-024	62051.67	94276.59	262.50	105.10	110.10	5.00	4.90	279	-88	19	0.02
Maria Ag Enriched	DDH-024	62051.57	94276.59	257.50	110.10	115.10	5.00	3.90	279	-88	2	0.00
Maria Ag Enriched	DDH-025	62145.37	94231.40	302.50	67.70	73.20	5.50	4.00	34	-66	62	0.01
Maria Ag Enriched	DDH-025	62147.87	94235.09	292.50	78.70	84.20	5.50	1.10	34	-66	55	0.03
Maria Ag Enriched	DDH-025	62149.17	94237.00	287.50	84.20	89.60	5.40	2.70	34	-66	38	0.01
Maria Ag Enriched	DDH-025	62150.37	94238.80	282.50	89.60	95.10	5.50	1.50	34	-66	14	0.05
Maria Ag Enriched	DDH-025	62152.87	94242.50	272.50	100.60	106.00	5.40	5.20	34	-66	22	0.09
Maria Ag Enriched	DDH-025	62154.07	94244.30	267.50	106.00	111.50	5.50	5.50	34	-66	56	0.13
Maria Ag Enriched	DDH-025	62155.37	94246.20	262.50	111.50	117.00	5.50	4.90	34	-66	29	0.02
Maria Ag Enriched	DDH-026	61824.87	94475.00	282.50	80.20	85.50	5.30	1.70	35	-71	3	0.00
Maria Ag Enriched	DDH-026	61825.87	94476.40	277.50	85.50	90.80	5.30	5.30	35	-71	31	0.02
Maria Ag Enriched	DDH-026	61826.87	94477.80	272.50	90.80	96.10	5.30	1.20	35	-71	8	0.00
Maria Ag Enriched	DDH-027	61810.47	94450.90	282.50	75.70	80.70	5.00	3.40	140	-88	29	0.00
Maria Ag Enriched	DDH-027	61810.57	94450.70	277.50	80.70	85.70	5.00	5.00	140	-88	15	0.01
Maria Ag Enriched	DDH-027	61810.67	94450.59	272.50	85.70	90.70	5.00	5.00	145	-88	6	0.00
Maria Ag Enriched	DDH-027	61810.77	94450.50	267.50	90.70	95.70	5.00	5.00	145	-88	23	0.00
Maria Ag Enriched	DDH-027	61810.87	94450.30	262.50	95.70	100.70	5.00	5.00	149	-88	61	0.00
Maria Ag Enriched	DDH-027	61810.97	94450.20	257.50	100.70	105.70	5.00	5.00	149	-88	219	0.01
Maria Ag Enriched	DDH-027	61811.07	94450.00	252.50	105.70	110.70	5.00	5.00	153	-88	219	0.10
Maria Ag Enriched	DDH-027	61811.17	94449.80	247.50	110.70	115.70	5.00	1.50	153	-88	175	0.08
Maria Ag Enriched	DDH-028	62090.67	94342.30	277.50	92.20	97.20	5.00	4.50	302	-89	27	0.11
Maria Ag Enriched	DDH-028	62090.57	94342.40	272.50	97.20	102.20	5.00	5.00	299	-89	26	0.07

Assay Composite Listing - Maria Ag Enriched Domain

		Mid-Point Coordinates (Truncated)			Drill Depth Interval				Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Defined Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Ag Enriched	DDH-028	62090.47	94342.40	267.50	102.20	107.30	5.10	2.80	295	-89	9	0.06
Maria Ag Enriched	T-017	62236.67	94195.70	292.50	80.50	85.90	5.40	5.20	23	-67	5	0.01
Maria Ag Enriched	T-017	62237.47	94197.70	287.50	85.90	91.40	5.50	5.40	23	-67	22	0.04
Maria Ag Enriched	T-017	62238.37	94199.59	282.50	91.40	96.80	5.40	5.20	23	-67	10	0.03
Maria Ag Enriched	T-017	62239.17	94201.59	277.50	96.80	102.20	5.40	5.40	22	-67	12	0.04
Maria Ag Enriched	T-017	62239.97	94203.50	272.50	102.20	107.70	5.50	1.90	22	-67	10	0.03
Maria Ag Enriched	T-021	61913.17	94333.70	282.50	81.50	86.70	5.20	0.70	29	-74	12	0.00
Maria Ag Enriched	T-021	61913.87	94334.90	277.50	86.70	91.90	5.20	5.20	29	-74	58	0.01
Maria Ag Enriched	T-021	61914.57	94336.20	272.50	91.90	97.10	5.20	5.20	29	-74	214	0.01
Maria Ag Enriched	T-021	61915.27	94337.40	267.50	97.10	102.30	5.20	0.10	29	-74	96	0.01
Maria Ag Enriched	T-022	61976.67	94338.00	292.50	74.90	80.20	5.30	2.50	32	-70	244	0.01
Maria Ag Enriched	T-022	61977.67	94339.50	287.50	80.20	85.60	5.40	5.30	32	-70	82	0.01
Maria Ag Enriched	T-022	61978.67	94341.09	282.50	85.60	90.90	5.30	5.30	32	-70	96	0.01
Maria Ag Enriched	T-022	61979.57	94342.59	277.50	90.90	96.20	5.30	5.30	32	-70	53	0.00
Maria Ag Enriched	T-022	61980.57	94344.20	272.50	96.20	101.50	5.30	5.30	32	-70	87	0.02
Maria Ag Enriched	T-022	61981.57	94345.70	267.50	101.50	106.80	5.30	5.30	32	-70	55	0.04
Maria Ag Enriched	T-022	61982.47	94347.20	262.50	106.80	112.20	5.40	5.30	32	-70	210	0.10
Maria Ag Enriched	T-022	61983.47	94348.80	257.50	112.20	117.50	5.30	0.60	32	-70	20	0.01
Maria Ag Enriched	T-023	61907.07	94423.30	277.50	85.20	90.20	5.00	1.60	7	-87	11	0.01
Maria Ag Enriched	T-023	61907.17	94423.50	272.50	90.20	95.20	5.00	5.00	7	-87	33	0.01
Maria Ag Enriched	T-023	61907.17	94423.80	267.50	95.20	100.20	5.00	5.00	6	-87	29	0.05
Maria Ag Enriched	T-023	61907.17	94424.00	262.50	100.20	105.20	5.00	4.90	6	-87	17	0.30
Maria Ag Enriched	T-023	61907.17	94424.30	257.50	105.20	110.20	5.00	5.00	5	-87	119	0.11
Maria Ag Enriched	T-023	61907.27	94424.50	252.50	110.20	115.20	5.00	2.80	5	-87	72	0.04
Maria Ag Enriched	T-024	61925.37	94454.50	272.50	93.40	98.40	5.00	3.70	15	-88	81	0.01
Maria Ag Enriched	T-025	61849.37	94427.90	277.50	82.00	87.00	5.00	2.80	45	-88	2	0.03
Maria Ag Enriched	T-025	61849.47	94428.00	272.50	87.00	92.00	5.00	0.30	45	-88	1	0.01
Maria Ag Enriched	T-025	61849.77	94428.40	257.50	102.00	107.00	5.00	3.30	54	-88	62	0.03
Maria Ag Enriched	T-025	61849.97	94428.50	252.50	107.00	112.00	5.00	3.00	54	-88	11	0.01
Maria Ag Enriched	T-026	61864.97	94457.30	277.50	89.40	94.90	5.50	0.30	30	-66	12	0.01
Maria Ag Enriched	T-026	61866.07	94459.20	272.50	94.90	100.40	5.50	3.50	30	-66	15	0.01
Maria Ag Enriched	T-026	61867.17	94461.09	267.50	100.40	105.90	5.50	2.40	30	-66	19	0.04
Maria Ag Enriched	T-029	62186.57	94304.90	297.50	76.50	81.50	5.00	0.70	331	-90	10	0.06
Maria Ag Enriched	T-029	62186.57	94304.90	292.50	81.50	86.50	5.00	5.00	331	-90	63	0.21
Maria Ag Enriched	T-029	62186.57	94304.90	287.50	86.50	91.50	5.00	5.00	322	-90	18	0.09
Maria Ag Enriched	T-029	62186.57	94304.90	282.50	91.50	96.50	5.00	3.50	312	-90	20	0.23
Maria Ag Enriched	T-033	62128.57	94296.80	287.50	82.90	88.00	5.10	3.20	18	-80	24	0.06
Maria Ag Enriched	T-033	62128.87	94297.70	282.50	88.00	93.10	5.10	5.10	18	-80	85	0.39
Maria Ag Enriched	T-033	62129.17	94298.59	277.50	93.10	98.20	5.10	5.10	18	-79	206	0.41
Maria Ag Enriched	T-033	62129.37	94299.50	272.50	98.20	103.30	5.10	5.10	18	-79	76	0.27
Maria Ag Enriched	T-033	62129.67	94300.40	267.50	103.30	108.40	5.10	5.10	17	-79	9	0.05
Maria Ag Enriched	T-033	62129.97	94301.30	262.50	108.40	113.40	5.00	2.90	17	-79	29	0.15
Maria Ag Enriched	T-034	62099.17	94239.59	312.50	54.40	59.40	5.00	1.20	0	-89	13	0.03
Maria Ag Enriched	T-034	62099.17	94239.70	307.50	59.40	64.40	5.00	5.00	0	-89	30	0.01
Maria Ag Enriched	T-034	62099.17	94239.80	302.50	64.40	69.40	5.00	1.00	0	-89	24	0.01
Maria Ag Enriched	T-034	62099.17	94240.00	292.50	69.40	79.40	10.00	1.70	0	-89	18	0.01
Maria Ag Enriched	T-034	62099.17	94240.09	287.50	79.40	84.40	5.00	2.70	0	-89	219	0.01
Maria Ag Enriched	T-035	62105.17	94249.09	307.50	60.50	65.60	5.10	2.50	30	-79	146	0.01
Maria Ag Enriched	T-035	62105.67	94249.90	302.50	65.60	70.70	5.10	2.20	30	-79	212	0.01
Maria Ag Enriched	T-035	62106.17	94250.70	297.50	70.70	75.80	5.10	3.90	30	-79	14	0.00
Maria Ag Enriched	T-035	62108.07	94254.09	277.50	91.10	96.20	5.10	2.40	30	-79	37	0.02
Maria Ag Enriched	T-035	62108.57	94255.00	272.50	96.20	101.30	5.10	0.90	30	-79	196	0.15
Maria Ag Enriched	T-038	62196.07	94218.09	292.50	75.00	80.10	5.10	1.10	30	-80	33	0.04
Maria Ag Enriched	T-038	62196.47	94218.90	287.50	80.10	85.20	5.10	5.10	30	-80	12	0.01
Maria Ag Enriched	T-038	62196.97	94219.70	282.50	85.20	90.30	5.10	5.10	30	-80	24	0.01
Maria Ag Enriched	T-038	62197.47	94220.50	277.50	90.30	95.40	5.10	5.10	30	-80	12	0.02
Maria Ag Enriched	T-038	62197.87	94221.30	272.50	95.40	100.40	5.00	5.00	31	-80	7	0.01
Maria Ag Enriched	T-038	62198.37	94222.09	267.50	100.40	105.50	5.10	5.10	31	-80	9	0.01
Maria Ag Enriched	T-038	62198.87	94222.80	262.50	105.50	110.60	5.10	5.10	30	-80	10	0.02
Maria Ag Enriched	T-038	62199.27	94223.59	257.50	110.60	115.70	5.10	5.10	30	-80	52	0.29

Assay Composite Listing - Maria Ag Enriched Domain

		Mid-Point Coordinates (Truncated)			Drill Depth Interval				Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Defined Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Ag Enriched	T-038	62199.77	94224.40	252.50	115.70	120.80	5.10	5.10	30	-80	48	0.06
Maria Ag Enriched	T-038	62200.27	94225.20	247.50	120.80	125.90	5.10	2.70	30	-80	26	0.09
Maria Ag Enriched	T-039	62208.97	94246.50	292.50	85.30	91.10	5.80	1.20	26	-60	52	0.11
Maria Ag Enriched	T-039	62210.27	94249.09	287.50	91.10	96.90	5.80	1.90	26	-60	148	0.25
Maria Ag Enriched	T-039	62211.47	94251.70	282.50	96.90	102.60	5.70	3.60	26	-60	25	0.29
Maria Ag Enriched	T-039	62212.77	94254.30	277.50	102.60	108.40	5.80	5.80	26	-60	50	0.40
Maria Ag Enriched	T-039	62213.97	94256.90	272.50	108.40	114.20	5.80	5.80	26	-60	41	0.19
Maria Ag Enriched	T-039	62215.27	94259.50	267.50	114.20	120.00	5.80	0.10	26	-60	89	0.34
Maria Ag Enriched	T-040	62174.77	94181.50	287.50	77.00	82.00	5.00	1.30	0	-89	107	0.05
Maria Ag Enriched	T-040	62174.77	94181.59	282.50	82.00	87.00	5.00	4.80	0	-89	92	0.01
Maria Ag Enriched	T-040	62174.77	94182.09	257.50	107.00	112.00	5.00	1.90	0	-89	14	0.00
Maria Ag Enriched	T-041	62073.07	94308.00	287.50	81.40	86.50	5.10	3.20	31	-81	636	0.05
Maria Ag Enriched	T-041	62073.47	94308.70	282.50	86.50	91.60	5.10	5.10	31	-81	871	0.18
Maria Ag Enriched	T-041	62073.97	94309.40	277.50	91.60	96.60	5.00	5.00	31	-81	798	0.49
Maria Ag Enriched	T-041	62074.37	94310.00	272.50	96.60	101.70	5.10	2.00	31	-81	268	0.24
Maria Ag Enriched	T-041	62074.77	94310.70	267.50	101.70	106.80	5.10	5.10	31	-81	16	0.17
Maria Ag Enriched	T-041	62075.17	94311.40	262.50	106.80	111.80	5.00	5.00	31	-81	30	0.12
Maria Ag Enriched	T-041	62075.57	94312.00	257.50	111.80	116.90	5.10	5.10	31	-81	33	0.27
Maria Ag Enriched	T-041	62075.87	94312.70	252.50	116.90	121.90	5.00	0.10	30	-81	40	0.53
Maria Ag Enriched	T-045	62041.47	94361.90	272.50	97.40	102.60	5.20	3.50	20	-75	33	0.08
Maria Ag Enriched	T-045	62041.87	94363.20	267.50	102.60	107.70	5.10	4.80	20	-75	17	0.10
Maria Ag Enriched	T-045	62042.37	94364.50	262.50	107.70	112.90	5.20	5.20	20	-75	18	0.09
Maria Ag Enriched	T-045	62042.87	94365.80	257.50	112.90	118.10	5.20	5.20	20	-75	37	0.16
Maria Ag Enriched	T-048	61962.77	94314.70	292.50	70.60	75.60	5.00	2.40	0	-90	21	0.01
Maria Ag Enriched	T-048	61962.77	94314.70	287.50	75.60	80.60	5.00	3.50	0	-90	10	0.00
Maria Ag Enriched	T-048	61962.77	94314.70	282.50	80.60	85.60	5.00	5.00	0	-90	34	0.01
Maria Ag Enriched	T-048	61962.77	94314.70	277.50	85.60	90.60	5.00	2.90	0	-90	37	0.00
Maria Ag Enriched	T-049	61877.17	94371.09	277.50	82.10	87.10	5.00	1.80	354	-88	12	0.00
Maria Ag Enriched	T-049	61877.17	94371.30	272.50	87.10	92.10	5.00	5.00	354	-88	43	0.01
Maria Ag Enriched	T-049	61877.07	94371.40	267.50	92.10	97.10	5.00	5.00	354	-88	331	0.21
Maria Ag Enriched	T-049	61877.07	94371.59	262.50	97.10	102.20	5.10	5.00	352	-88	226	0.01
Maria Ag Enriched	T-049	61877.07	94371.80	257.50	102.20	107.20	5.00	5.00	352	-88	106	0.00
Maria Ag Enriched	T-049	61877.07	94371.90	252.50	107.20	112.20	5.00	0.70	352	-88	9	0.00
Maria Ag Enriched	T-050	61829.27	94388.00	277.50	80.00	85.00	5.00	2.60	262	-90	108	0.01
Maria Ag Enriched	T-050	61829.27	94388.00	272.50	85.00	90.00	5.00	3.70	262	-90	19	0.01
Maria Ag Enriched	T-051	61783.47	94404.80	262.50	92.90	97.90	5.00	1.90	192	-88	53	0.01
Maria Ag Enriched	T-051	61783.37	94404.59	257.50	97.90	102.90	5.00	1.20	192	-88	3	0.01
Maria Ag Enriched	T-053	62112.87	94180.20	292.50	69.40	74.40	5.00	0.90	0	-88	4	0.01
Maria Ag Enriched	T-053	62112.87	94180.40	287.50	74.40	79.40	5.00	2.90	4	-88	7	0.03
Maria Ag Enriched	T-053	62112.97	94180.50	282.50	79.40	84.40	5.00	3.70	4	-88	18	0.02
Maria Ag Enriched	T-053	62112.97	94180.59	277.50	84.40	89.40	5.00	1.80	8	-88	38	0.03
Maria Ag Enriched	T-053	62112.97	94180.80	272.50	89.40	94.40	5.00	5.00	8	-88	26	0.03
Maria Ag Enriched	T-053	62112.97	94180.90	267.50	94.40	99.40	5.00	1.00	12	-89	11	0.01
Maria Ag Enriched	T-053	62112.97	94181.00	262.50	99.40	104.40	5.00	2.60	12	-89	35	0.03
Maria Ag Enriched	T-053	62113.07	94181.20	257.50	104.40	109.40	5.00	1.00	6	-88	30	0.05
Maria Ag Enriched	T-054	62263.37	94230.00	292.50	103.40	110.30	6.90	5.90	30	-47	48	0.08
Maria Ag Enriched	T-054	62265.77	94234.09	287.50	110.30	117.20	6.90	4.00	30	-47	8	0.03
Maria Ag Enriched	T-056	62006.47	94296.70	302.50	62.50	67.50	5.00	0.20	299	-88	47	0.01
Maria Ag Enriched	T-056	62006.37	94296.80	297.50	67.50	72.50	5.00	5.00	299	-88	14	0.01
Maria Ag Enriched	T-056	62006.17	94296.90	292.50	72.50	77.50	5.00	5.00	292	-88	46	0.02
Maria Ag Enriched	T-056	62005.97	94296.90	287.50	77.50	82.50	5.00	2.50	292	-88	38	0.01
Maria Ag Enriched	T-056	62005.87	94297.00	282.50	82.50	87.60	5.10	3.20	282	-88	22	0.01
Maria Ag Enriched	T-056	62005.67	94297.00	277.50	87.60	92.60	5.00	2.40	282	-88	65	0.01
Maria Ag Enriched	T-056	62004.87	94297.20	252.50	112.60	117.60	5.00	0.90	282	-88	135	0.21
Maria Ag Enriched	T-056	62004.67	94297.20	247.50	117.60	122.60	5.00	2.80	282	-88	66	0.08
Maria Ag Enriched	T-066	62273.87	94210.30	287.50	93.40	99.20	5.80	3.70	25	-61	26	0.08
Maria Ag Enriched	T-066	62275.07	94212.90	282.50	99.20	105.00	5.80	2.90	24	-61	16	0.08
Maria Ag Enriched	T-067	62240.67	94238.09	287.50	93.40	99.10	5.70	2.50	33	-61	89	0.11
Maria Ag Enriched	T-067	62242.17	94240.50	282.50	99.10	104.80	5.70	5.70	33	-61	33	0.13
Maria Ag Enriched	T-067	62243.67	94242.80	277.50	104.80	110.50	5.70	4.30	33	-62	37	0.09

Assay Composite Listing - Maria Ag Enriched Domain

		Mid-Point Coordinates (Truncated)			Drill Depth Interval				Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Defined Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Ag Enriched	T-069	62199.17	94222.09	287.50	89.80	95.70	5.90	1.40	30	-59	34	0.04
Maria Ag Enriched	T-069	62202.17	94227.30	277.50	101.50	107.30	5.80	0.50	30	-59	49	0.08
Maria Ag Enriched	T-069	62206.67	94235.09	262.50	119.00	124.80	5.80	2.00	30	-59	14	0.32
Maria Ag Enriched	T-069	62208.17	94237.70	257.50	124.80	130.70	5.90	0.90	30	-59	54	0.67
Maria Ag Enriched	T-070	62206.77	94196.09	267.50	107.70	113.20	5.50	4.20	22	-65	6	0.03
Maria Ag Enriched	T-070	62207.67	94198.30	262.50	113.20	118.70	5.50	5.50	22	-65	18	0.16
Maria Ag Enriched	T-070	62208.57	94200.50	257.50	118.70	124.20	5.50	1.30	22	-65	7	0.05
Maria Ag Enriched	T-071	62162.97	94160.20	287.50	82.50	88.00	5.50	1.50	27	-65	39	0.02
Maria Ag Enriched	T-071	62163.97	94162.20	282.50	88.00	93.50	5.50	5.30	27	-65	28	0.02
Maria Ag Enriched	T-071	62165.07	94164.30	277.50	93.50	99.10	5.60	4.10	27	-65	12	0.02
Maria Ag Enriched	T-071	62166.17	94166.40	272.50	99.10	104.60	5.50	2.90	26	-65	19	0.02
Maria Ag Enriched	T-071	62167.17	94168.50	267.50	104.60	110.10	5.50	2.20	26	-65	16	0.04
Maria Ag Enriched	T-072	62158.37	94199.30	287.50	82.30	87.80	5.50	1.20	34	-66	21	0.03
Maria Ag Enriched	T-072	62159.67	94201.09	282.50	87.80	93.20	5.40	5.40	34	-66	6	0.01
Maria Ag Enriched	T-072	62160.87	94202.90	277.50	93.20	98.70	5.50	5.50	34	-66	23	0.01
Maria Ag Enriched	T-072	62162.17	94204.80	272.50	98.70	104.20	5.50	5.50	34	-66	10	0.01
Maria Ag Enriched	T-072	62163.37	94206.70	267.50	104.20	109.60	5.40	0.80	33	-66	4	0.01
Maria Ag Enriched	T-072	62164.57	94208.50	262.50	109.60	115.10	5.50	1.60	33	-66	33	0.05
Maria Ag Enriched	T-072	62165.77	94210.40	257.50	115.10	120.60	5.50	4.40	33	-66	54	0.05
Maria Ag Enriched	T-073	62080.67	94372.59	282.50	101.70	107.80	6.10	1.30	28	-56	5	0.04
Maria Ag Enriched	T-073	62082.27	94375.59	277.50	107.80	113.90	6.10	2.80	28	-56	63	0.50
Maria Ag Enriched	T-074	61902.57	94367.70	292.50	77.90	83.60	5.70	1.00	20	-61	1	0.01
Maria Ag Enriched	T-074	61903.57	94370.40	287.50	83.60	89.30	5.70	5.70	19	-61	333	0.21
Maria Ag Enriched	T-074	61904.47	94373.00	282.50	89.30	95.00	5.70	5.70	19	-61	144	0.02
Maria Ag Enriched	T-074	61905.37	94375.59	277.50	95.00	100.80	5.80	5.50	18	-61	19	0.01
Maria Ag Enriched	T-074	61906.17	94378.30	272.50	100.80	106.50	5.70	5.70	18	-61	13	0.01
Maria Ag Enriched	T-074	61907.07	94380.90	267.50	106.50	112.20	5.70	5.70	18	-61	19	0.02
Maria Ag Enriched	T-074	61907.97	94383.50	262.50	112.20	117.90	5.70	5.70	19	-61	141	0.09
Maria Ag Enriched	T-074	61908.87	94386.09	257.50	117.90	123.60	5.70	5.70	19	-61	36	0.07
Maria Ag Enriched	T-074	61909.77	94388.70	252.50	123.60	129.30	5.70	5.70	19	-61	8	0.03
Maria Ag Enriched	T-074	61910.67	94391.30	247.50	129.30	135.00	5.70	0.00	19	-61	11	0.01
Maria Ag Enriched	T-075	61892.47	94335.80	287.50	79.10	84.60	5.50	3.90	33	-65	56	0.01
Maria Ag Enriched	T-075	61893.77	94337.80	282.50	84.60	90.20	5.60	2.20	33	-64	52	0.00
Maria Ag Enriched	T-075	61895.07	94339.80	277.50	90.20	95.70	5.50	1.40	33	-64	32	0.00
Maria Ag Enriched	T-075	61896.37	94341.80	272.50	95.70	101.30	5.60	1.50	33	-64	25	0.01
Maria Ag Enriched	T-076	61852.47	94372.70	287.50	74.70	80.00	5.30	0.50	31	-70	31	0.00
Maria Ag Enriched	T-076	61853.47	94374.20	282.50	80.00	85.30	5.30	0.70	31	-70	13	0.01
Maria Ag Enriched	T-076	61854.37	94375.80	277.50	85.30	90.70	5.40	1.20	31	-70	49	0.02
Maria Ag Enriched	T-076	61855.27	94377.40	272.50	90.70	96.00	5.30	2.40	31	-70	320	0.01
Maria Ag Enriched	T-076	61856.17	94378.90	267.50	96.00	101.30	5.30	0.50	31	-70	99	0.01
Maria Ag Enriched	T-076	61858.07	94382.00	257.50	106.60	111.90	5.30	0.50	32	-70	16	0.00
Maria Ag Enriched	T-076	61859.07	94383.59	252.50	111.90	117.20	5.30	1.20	32	-70	152	0.02
Maria Ag Enriched	T-077	61865.17	94395.80	282.50	83.40	88.90	5.50	3.70	28	-65	20	0.01
Maria Ag Enriched	T-077	61866.27	94397.90	277.50	88.90	94.40	5.50	5.50	28	-65	23	0.01
Maria Ag Enriched	T-077	61867.27	94400.00	272.50	94.40	99.90	5.50	4.50	28	-65	98	0.03
Maria Ag Enriched	T-077	61868.37	94402.00	267.50	99.90	105.50	5.60	3.00	28	-65	43	0.01
Maria Ag Enriched	T-077	61869.47	94404.00	262.50	105.50	111.00	5.50	5.00	27	-65	21	0.04
Maria Ag Enriched	T-078	62062.27	94290.20	297.50	72.10	77.30	5.20	0.80	32	-76	35	0.00
Maria Ag Enriched	T-078	62062.97	94291.30	292.50	77.30	82.40	5.10	1.40	32	-76	236	0.01
Maria Ag Enriched	T-078	62063.57	94292.30	287.50	82.40	87.60	5.20	1.20	32	-76	14	0.00
Maria Ag Enriched	T-078	62064.27	94293.40	282.50	87.60	92.70	5.10	3.20	32	-76	29	0.02
Maria Ag Enriched	T-078	62064.97	94294.50	277.50	92.70	97.90	5.20	5.20	32	-76	71	0.02
Maria Ag Enriched	T-078	62065.57	94295.50	272.50	97.90	103.00	5.10	5.10	32	-76	167	0.03
Maria Ag Enriched	T-078	62066.27	94296.59	267.50	103.00	108.20	5.20	5.20	32	-76	27	0.02
Maria Ag Enriched	T-078	62066.97	94297.59	262.50	108.20	113.30	5.10	5.10	32	-76	25	0.07
Maria Ag Enriched	T-078	62067.57	94298.70	257.50	113.30	118.50	5.20	5.20	32	-76	25	0.05
Maria Ag Enriched	T-078	62068.27	94299.70	252.50	118.50	123.60	5.10	1.30	32	-76	2	0.02
Maria Ag Enriched	T-245	62229.37	94281.09	297.50	82.00	87.70	5.70	0.30	26	-62	25	0.04
Maria Ag Enriched	T-245	62230.57	94283.50	292.50	87.70	93.40	5.70	5.10	26	-62	96	0.14
Maria Ag Enriched	T-289	62225.47	94221.70	287.50	91.40	97.20	5.80	1.80	30	-59	56	0.06

Assay Composite Listing - Maria Ag Enriched Domain

		Mid-Point Coordinates (Truncated)			Drill Depth Interval				Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Defined Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Ag Enriched	T-289	62228.57	94226.90	277.50	103.00	108.90	5.90	4.60	30	-59	37	0.11
Maria Ag Enriched	T-289	62230.07	94229.50	272.50	108.90	114.70	5.80	4.10	30	-59	13	0.02
Maria Ag Enriched	T-303	62266.47	94194.30	282.50	97.90	103.60	5.70	4.60	29	-61	61	0.10
Maria Ag Enriched	T-309	61877.07	94413.40	282.50	90.10	96.00	5.90	3.70	33	-58	12	0.04
Maria Ag Enriched	T-309	61878.67	94416.00	277.50	96.00	101.90	5.90	5.90	33	-58	43	0.06
Maria Ag Enriched	T-309	61880.37	94418.70	272.50	101.90	107.80	5.90	4.10	33	-58	38	0.08
Maria Ag Enriched	T-309	61882.17	94421.30	267.50	107.80	113.70	5.90	3.10	33	-58	70	0.14
Maria Ag Enriched	T-309	61883.87	94423.90	262.50	113.70	119.60	5.90	5.30	33	-58	111	0.05
Maria Ag Enriched	T-310	61900.77	94456.70	277.50	96.00	101.70	5.70	0.90	31	-60	74	0.00
Maria Ag Enriched	T-310	61902.27	94459.20	272.50	101.70	107.40	5.70	2.80	31	-60	146	0.05
Maria Ag Enriched	T-316	61922.17	94398.80	277.50	97.10	102.80	5.70	3.00	29	-61	1	0.00
Maria Ag Enriched	T-316	61923.47	94401.20	272.50	102.80	108.50	5.70	5.70	30	-61	70	0.02
Maria Ag Enriched	T-316	61924.87	94403.59	267.50	108.50	114.20	5.70	5.70	30	-61	52	0.04
Maria Ag Enriched	T-316	61926.27	94406.09	262.50	114.20	120.00	5.80	5.70	30	-61	101	0.16
Maria Ag Enriched	T-316	61927.67	94408.50	257.50	120.00	125.70	5.70	5.70	30	-61	67	0.23
Maria Ag Enriched	T-316	61929.07	94410.90	252.50	125.70	131.40	5.70	0.60	30	-61	15	0.02
Maria Ag Enriched	T-318	62119.77	94241.00	287.50	87.20	92.90	5.70	2.90	28	-61	46	0.01
Maria Ag Enriched	T-318	62121.07	94243.50	282.50	92.90	98.70	5.80	5.70	28	-61	60	0.02
Maria Ag Enriched	T-318	62122.47	94246.00	277.50	98.70	104.40	5.70	5.70	28	-61	13	0.00
Maria Ag Enriched	T-318	62123.67	94248.50	272.50	104.40	110.10	5.70	1.60	28	-61	5	0.01
Maria Ag Enriched	T-318	62124.97	94251.00	267.50	110.10	115.90	5.80	4.90	28	-61	69	0.02
Maria Ag Enriched	T-318	62126.27	94253.40	262.50	115.90	121.60	5.70	5.70	27	-61	28	0.04
Maria Ag Enriched	T-318	62127.57	94255.90	257.50	121.60	127.30	5.70	5.70	27	-61	58	0.07
Maria Ag Enriched	T-318	62128.77	94258.40	252.50	127.30	133.00	5.70	1.50	27	-61	42	0.01
Maria Ag Enriched	T-319	62135.17	94264.80	287.50	89.40	95.00	5.60	3.60	30	-62	25	0.05
Maria Ag Enriched	T-319	62136.47	94267.09	282.50	95.00	100.70	5.70	5.70	30	-62	22	0.04
Maria Ag Enriched	T-319	62137.77	94269.40	277.50	100.70	106.30	5.60	3.20	30	-62	15	0.12
Maria Ag Enriched	T-319	62139.07	94271.59	272.50	106.30	112.00	5.70	1.00	30	-62	5	0.04
Maria Ag Enriched	T-319	62140.37	94273.90	267.50	112.00	117.60	5.60	3.90	30	-62	14	0.08
Maria Ag Enriched	T-319	62141.77	94276.20	262.50	117.60	123.20	5.60	2.50	30	-63	7	0.09
Maria Ag Enriched	T-319	62143.07	94278.40	257.50	123.20	128.90	5.70	4.90	30	-63	89	0.11
Maria Ag Enriched	T-319	62144.37	94280.70	252.50	128.90	134.50	5.60	4.70	30	-63	52	0.12
Maria Ag Enriched	T-320	62151.77	94289.70	287.50	91.40	97.20	5.80	2.80	31	-61	71	0.14
Maria Ag Enriched	T-320	62153.27	94292.09	282.50	97.20	102.90	5.70	5.70	31	-61	105	0.29
Maria Ag Enriched	T-320	62154.77	94294.59	277.50	102.90	108.70	5.80	1.80	31	-61	53	0.18
Maria Ag Enriched	T-320	62156.17	94297.00	272.50	108.70	114.40	5.70	5.10	31	-61	25	0.25
Maria Ag Enriched	T-320	62157.67	94299.40	267.50	114.40	120.20	5.80	2.30	31	-61	38	0.39
Maria Ag Enriched	T-321	62165.47	94219.20	287.50	86.70	92.30	5.60	1.40	28	-62	176	0.03
Maria Ag Enriched	T-321	62166.67	94221.59	282.50	92.30	98.00	5.70	0.70	28	-62	21	0.01
Maria Ag Enriched	T-321	62170.57	94228.70	267.50	109.40	115.10	5.70	2.50	29	-62	60	0.05
Maria Ag Enriched	T-321	62171.87	94231.00	262.50	115.10	120.70	5.60	0.70	29	-62	52	0.02
Maria Ag Enriched	T-321	62173.07	94233.40	257.50	120.70	126.40	5.70	3.90	29	-62	123	0.08
Maria Ag Enriched	T-321	62174.37	94235.80	252.50	126.40	132.10	5.70	1.30	29	-62	42	0.02
Maria Ag Enriched	T-322	62179.97	94244.80	292.50	83.70	89.40	5.70	2.70	29	-61	93	0.03
Maria Ag Enriched	T-322	62181.27	94247.20	287.50	89.40	95.10	5.70	3.10	29	-61	39	0.02
Maria Ag Enriched	T-322	62182.67	94249.70	282.50	95.10	100.80	5.70	4.90	28	-62	47	0.10
Maria Ag Enriched	T-322	62183.87	94252.00	277.50	100.80	106.50	5.70	4.60	28	-62	37	0.18
Maria Ag Enriched	T-323	62249.77	94264.40	292.50	88.70	94.50	5.80	4.40	31	-60	32	0.05
Maria Ag Enriched	T-323	62251.27	94266.90	287.50	94.50	100.30	5.80	1.90	31	-60	117	0.12
Maria Ag Enriched	T-325	61830.47	94444.40	282.50	86.00	91.80	5.80	4.40	33	-59	29	0.01
Maria Ag Enriched	T-325	61832.17	94446.90	277.50	91.80	97.60	5.80	5.80	33	-59	14	0.01
Maria Ag Enriched	T-325	61833.77	94449.40	272.50	97.60	103.50	5.90	5.80	34	-59	25	0.01
Maria Ag Enriched	T-325	61835.47	94451.90	267.50	103.50	109.30	5.80	4.70	35	-59	24	0.01
Maria Ag Enriched	T-325	61837.17	94454.30	262.50	109.30	115.10	5.80	5.80	35	-59	62	0.11
Maria Ag Enriched	T-325	61838.97	94456.80	257.50	115.10	121.00	5.90	0.70	35	-59	144	0.11
Maria Ag Enriched	T-326	61932.87	94359.20	287.50	84.80	90.60	5.80	0.70	29	-60	22	0.01
Maria Ag Enriched	T-326	61934.27	94361.70	282.50	90.60	96.30	5.70	5.70	29	-60	538	0.01
Maria Ag Enriched	T-326	61935.67	94364.20	277.50	96.30	102.10	5.80	5.80	29	-60	337	0.02
Maria Ag Enriched	T-326	61937.07	94366.70	272.50	102.10	107.90	5.80	5.80	29	-60	376	0.10
Maria Ag Enriched	T-326	61938.37	94369.20	267.50	107.90	113.60	5.70	5.70	29	-60	181	0.11

Assay Composite Listing - Maria Ag Enriched Domain

		Mid-Point Coordinates (Truncated)			Drill Depth Interval				Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Defined Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Maria Ag Enriched	T-326	61939.77	94371.70	262.50	113.60	119.40	5.80	5.80	28	-60	286	0.14
Maria Ag Enriched	T-326	61941.17	94374.20	257.50	119.40	125.10	5.70	5.70	28	-60	68	0.05
Maria Ag Enriched	T-326	61942.47	94376.70	252.50	125.10	130.90	5.80	0.80	28	-61	58	0.05
Maria Ag Enriched	T-331	62126.67	94347.20	302.50	77.30	83.00	5.70	1.70	31	-61	47	0.04
Maria Ag Enriched	T-331	62128.17	94349.59	297.50	83.00	88.70	5.70	5.60	31	-61	31	0.12
Maria Ag Enriched	T-334	62208.67	94199.20	292.50	83.10	88.80	5.70	0.80	30	-61	18	0.01
Maria Ag Enriched	T-334	62210.17	94201.59	287.50	88.80	94.60	5.80	5.70	30	-61	19	0.01
Maria Ag Enriched	T-334	62211.57	94204.09	282.50	94.60	100.30	5.70	5.70	29	-60	36	0.06
Maria Ag Enriched	T-334	62212.97	94206.59	277.50	100.30	106.10	5.80	3.10	29	-60	57	0.14
Maria Ag Enriched	T-334	62214.37	94209.09	272.50	106.10	111.80	5.70	0.90	29	-60	7	0.03
Maria Ag Enriched	T-334	62215.77	94211.59	267.50	111.80	117.60	5.80	2.40	29	-60	15	0.07
Maria Ag Enriched	T-334	62217.17	94214.09	262.50	117.60	123.40	5.80	4.80	30	-60	22	0.01
Maria Ag Enriched	T-334	62218.57	94216.59	257.50	123.40	129.10	5.70	4.00	30	-60	84	0.04
Maria Ag Enriched	T-355-MET	61900.07	94404.00	287.50	74.40	79.50	5.10	2.10	37	-81	1	0.00
Maria Ag Enriched	T-355-MET	61900.57	94404.70	282.50	79.50	84.50	5.00	5.00	37	-81	36	0.00
Maria Ag Enriched	T-355-MET	61901.07	94405.40	277.50	84.50	89.60	5.10	5.10	37	-81	40	0.01
Maria Ag Enriched	T-355-MET	61901.57	94406.09	272.50	89.60	94.70	5.10	5.10	37	-81	11	0.02
Maria Ag Enriched	T-355-MET	61902.07	94406.70	267.50	94.70	99.80	5.10	5.10	38	-81	56	0.03
Maria Ag Enriched	T-355-MET	61902.57	94407.40	262.50	99.80	104.80	5.00	5.00	38	-81	84	0.05
Maria Ag Enriched	T-355-MET	61903.07	94408.00	257.50	104.80	109.90	5.10	5.10	38	-81	102	0.21
Maria Ag Enriched	T-355-MET	61903.57	94408.70	252.50	109.90	115.00	5.10	5.10	38	-81	34	0.25
Maria Ag Enriched	T-355-MET	61904.07	94409.30	247.50	115.00	120.00	5.00	5.00	37	-81	57	0.32
Maria Ag Enriched	T-355-MET	61904.57	94410.00	242.50	120.00	125.10	5.10	2.20	37	-81	21	0.02
Maria Ag Enriched	T-357-MET	62207.87	94240.30	292.50	76.40	81.40	5.00	2.40	275	-89	31	0.05
Maria Ag Enriched	T-357-MET	62207.77	94240.40	287.50	81.40	86.40	5.00	5.00	287	-89	70	0.12
Maria Ag Enriched	T-357-MET	62207.67	94240.40	282.50	86.40	91.40	5.00	2.60	287	-89	10	0.03
Maria Ag Enriched	T-357-MET	62207.57	94240.40	277.50	91.40	96.40	5.00	4.10	287	-89	13	0.17
Maria Ag Enriched	T-357-MET	62207.47	94240.40	272.50	96.40	101.40	5.00	5.00	286	-89	10	0.06
Maria Ag Enriched	T-357-MET	62207.47	94240.50	267.50	101.40	106.40	5.00	4.90	286	-89	14	0.05
Maria Ag Enriched	T-402	62074.37	94265.90	302.50	70.90	76.60	5.70	0.90	26	-62	21	0.01
Maria Ag Enriched	T-402	62075.57	94268.30	297.50	76.60	82.30	5.70	5.70	26	-62	25	0.01
Maria Ag Enriched	T-402	62076.77	94270.80	292.50	82.30	88.00	5.70	5.70	25	-62	34	0.00
Maria Ag Enriched	T-402	62077.87	94273.20	287.50	88.00	93.70	5.70	5.70	25	-62	64	0.01
Maria Ag Enriched	T-402	62079.07	94275.70	282.50	93.70	99.40	5.70	5.70	25	-62	29	0.01
Maria Ag Enriched	T-402	62080.17	94278.09	277.50	99.40	105.10	5.70	5.70	25	-62	25	0.02
Maria Ag Enriched	T-402	62081.27	94280.59	272.50	105.10	110.70	5.60	5.60	24	-62	165	0.01
Maria Ag Enriched	T-402	62082.37	94283.00	267.50	110.70	116.40	5.70	5.70	24	-62	32	0.02
Maria Ag Enriched	T-402	62083.37	94285.50	262.50	116.40	122.10	5.70	5.70	24	-62	42	0.04
Maria Ag Enriched	T-402	62084.47	94287.90	257.50	122.10	127.70	5.60	5.60	24	-62	30	0.03
Maria Ag Enriched	T-402	62085.47	94290.40	252.50	127.70	133.40	5.70	4.40	23	-62	67	0.05
Maria Ag Enriched	T-424	62158.87	94254.80	302.50	69.80	75.30	5.50	3.00	31	-66	24	0.01
Maria Ag Enriched	T-424	62159.97	94256.70	297.50	75.30	80.70	5.40	5.40	31	-66	52	0.02
Maria Ag Enriched	T-424	62161.17	94258.59	292.50	80.70	86.20	5.50	5.50	31	-66	42	0.03
Maria Ag Enriched	T-424	62162.27	94260.59	287.50	86.20	91.70	5.50	3.00	31	-66	19	0.11
Maria Ag Enriched	T-424	62163.47	94262.50	282.50	91.70	97.20	5.50	5.50	31	-66	5	0.01
Maria Ag Enriched	T-424	62164.57	94264.40	277.50	97.20	102.70	5.50	5.50	31	-66	25	0.11
Maria Ag Enriched	T-424	62165.67	94266.30	272.50	102.70	108.10	5.40	5.40	30	-66	31	0.14
Maria Ag Enriched	T-424	62166.87	94268.20	267.50	108.10	113.60	5.50	3.90	30	-66	36	0.22
Maria Ag Enriched	T-486	62109.67	94320.20	282.50	99.70	105.40	5.70	3.90	30	-61	18	0.10
Maria Ag Enriched	T-486	62111.07	94322.59	277.50	105.40	111.10	5.70	5.70	30	-61	51	0.19
Maria Ag Enriched	T-486	62112.47	94325.00	272.50	111.10	116.80	5.70	0.50	30	-61	12	0.05
Maria Ag Enriched	T-488	62054.47	94321.20	277.50	96.20	101.60	5.40	2.00	31	-68	389	0.04
Maria Ag Enriched	T-488	62055.47	94323.00	272.50	101.60	107.00	5.40	1.90	31	-68	21	0.08
Maria Ag Enriched	T-488	62056.57	94324.70	267.50	107.00	112.40	5.40	5.40	31	-68	9	0.12
Maria Ag Enriched	T-488	62057.57	94326.40	262.50	112.40	117.80	5.40	5.40	31	-68	13	0.07
Maria Ag Enriched	T-488	62058.57	94328.09	257.50	117.80	123.20	5.40	5.40	31	-68	8	0.09
Maria Ag Enriched	T-488	62059.67	94329.80	252.50	123.20	128.60	5.40	0.40	31	-68	10	0.04

Assay Composite Listing - Melissa North Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Melissa N	T-131	63252.34	94124.70	357.92	55.39	61.12	5.73	46	-44	798	21.15
Melissa N	T-167	63252.95	94127.31	318.30	97.06	113.56	16.50	44	-48	612	8.63
Melissa N	T-169	63287.66	94127.09	324.19	99.19	102.30	3.11	43	-48	293	13.67
Melissa N	T-170	63213.56	94121.32	380.88	20.05	27.91	7.86	47	-44	5	0.05
Melissa N	T-171	63323.34	94130.04	324.54	102.59	107.70	5.11	43	-44	676	11.64
Melissa N	T-192	63200.02	94118.81	370.73	33.29	37.51	4.22	179	-49	13	0.15
Melissa N	T-193	63259.60	94136.91	273.57	132.85	136.40	3.55	225	-66	257	3.73
Melissa N	T-264	63206.58	94123.86	321.58	81.15	92.78	11.62	358	-60	441	8.83
Melissa N	T-265	63342.01	94138.09	311.82	112.61	117.79	5.18	181	-46	297	9.44
Melissa N	T-292	63224.15	94130.78	301.13	107.19	110.19	3.01	179	-60	1217	17.77
Melissa N	T-293	63316.89	94146.91	240.35	174.38	179.14	4.76	178	-61	365	1.66
Melissa N	T-294	63374.16	94160.18	236.09	180.72	184.12	3.40	180	-60	239	1.29
Melissa N	T-295	63174.90	94129.81	301.25	104.22	106.94	2.72	179	-60	37	0.45
Melissa N	T-296	63424.79	94145.62	290.70	119.28	121.80	2.52	183	-60	135	1.74
Melissa N	T-297	63305.70	94126.88	310.51	96.73	101.49	4.76	178	-60	1415	8.81
Melissa N	T-313	63270.40	94145.45	241.56	174.41	176.64	2.23	185	-61	603	1.71
Melissa N	T-314	63222.05	94141.69	259.97	151.67	156.40	4.72	180	-61	209	1.08
Melissa N	T-343	63375.51	94144.61	288.97	117.10	126.33	9.23	180	-61	775	12.27
Melissa N	T-344	63349.92	94129.46	352.58	59.29	61.20	1.91	182	-47	397	7.58
Melissa N	T-345	63399.60	94139.35	327.98	76.62	80.07	3.45	182	-59	323	3.50
Melissa N	T-408	63424.31	94138.72	332.33	80.97	83.31	2.34	183	-50	950	10.91
Melissa N	T-409	63474.88	94144.63	323.23	89.51	92.25	2.75	183	-49	12	0.05
Melissa N	T-410	63174.04	94121.97	325.80	85.26	89.08	3.82	180	-50	3	0.02
Melissa N	T-411	63123.71	94119.54	321.31	86.57	90.24	3.67	182	-50	12	0.33
Melissa N	T-445	63298.57	94127.36	340.58	74.37	79.14	4.77	181	-46	415	5.30
Melissa N	T-446	63400.89	94133.94	350.19	61.25	64.13	2.89	180	-47	314	4.95
Melissa N	T-447	63321.55	94136.49	273.24	165.13	168.15	3.02	183	-46	330	1.64
Melissa N	T-448	63225.68	94125.82	351.20	61.15	64.31	3.16	181	-46	164	2.48
Melissa N	T-466	63374.87	94137.56	354.66	54.90	58.34	3.44	181	-47	571	5.96
Melissa N	T-468	63253.18	94119.31	381.82	20.69	27.42	6.73	181	-45	98	3.97
Melissa N	T-662	63300.17	94133.57	276.28	134.53	137.76	3.23	181	-61	1131	8.12
Melissa N	T-663	63346.44	94139.41	278.58	141.28	144.64	3.36	183	-55	183	4.69

Assay Composite Listing - Concepción Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Concepcion Main	DDH-030	63764.55	94633.74	290.61	99.97	104.01	4.04	0	-89	409	5.26
Concepcion Main	DDH-031	63868.92	94608.26	247.72	139.77	146.69	6.92	0	-90	122	1.10
Concepcion Main	T-086	63651.91	94641.70	305.26	89.81	93.60	3.79	344	-89	61	0.72
Concepcion Main	T-087	63638.04	94679.84	371.85	23.15	30.06	6.91	337	-70	15	0.38
Concepcion Main	T-088	63722.61	94666.67	315.78	73.39	80.93	7.54	270	-89	222	1.51
Concepcion Main	T-089	63707.21	94709.01	369.40	23.12	32.16	9.04	338	-61	58	0.78
Concepcion Main	T-090	63769.09	94683.50	339.00	48.39	54.11	5.72	281	-89	348	6.83
Concepcion Main	T-091	63759.41	94708.41	364.30	33.43	38.81	5.38	338	-46	134	1.35
Concepcion Main	T-092	63789.26	94702.37	358.57	29.66	34.83	5.17	339	-70	54	0.55
Concepcion Main	T-093	63597.54	94644.12	345.81	51.31	63.45	12.14	339	-68	199	2.85
Concepcion Main	T-129	64121.18	94767.18	376.26	15.32	17.58	2.26	359	-45	169	1.73
Concepcion Main	T-477	63499.33	94614.76	344.82	64.81	68.09	3.28	338	-58	187	1.67
Concepcion Main	T-478	63850.37	94683.17	336.45	57.64	61.37	3.73	335	-61	478	4.39
Concepcion Main	T-479	63807.41	94660.20	315.55	85.86	89.37	3.51	338	-60	251	2.07
Concepcion Main	T-480	63746.37	94679.07	332.84	64.54	70.86	6.32	337	-61	126	0.95
Concepcion Main	T-481	63689.24	94686.35	340.24	60.48	63.61	3.13	337	-61	142	1.44
Concepcion Main	T-482	63670.55	94663.35	318.54	88.17	91.01	2.84	336	-60	124	1.39
Concepcion Main	T-483	63549.07	94632.94	347.04	72.78	79.13	6.35	358	-45	47	1.81
Concepcion Main	T-497	63866.22	94708.21	354.11	36.44	39.06	2.62	338	-61	164	1.67
Concepcion Main	T-498	63880.82	94675.86	325.13	71.66	74.08	2.42	338	-60	519	4.85
Concepcion Main	T-499	63896.22	94699.05	342.61	49.64	52.82	3.18	336	-61	500	5.27
Concepcion Main	T-500	63911.02	94726.99	359.58	30.40	32.91	2.51	336	-60	132	0.67
Concepcion Main	T-501	63942.67	94718.78	347.38	44.11	47.16	3.06	340	-60	94	0.79
Concepcion Main	T-502	63975.73	94710.36	329.37	62.87	69.70	6.83	338	-60	136	3.99
Concepcion Main	T-503	63990.85	94738.81	347.94	44.35	47.35	3.00	338	-60	381	3.00
Concepcion Main	T-504	64007.03	94701.92	314.74	81.91	84.82	2.91	338	-60	151	1.06
Concepcion Main	T-505	64023.63	94729.45	336.45	55.88	61.06	5.18	338	-60	386	3.97
Concepcion Main	T-506	64036.58	94753.05	351.22	41.09	44.65	3.56	338	-60	397	3.55
Concepcion Main	T-507	64068.02	94741.69	347.73	45.40	47.66	2.26	337	-59	150	2.99
Concepcion Main	T-508	64106.78	94721.81	353.17	39.74	41.87	2.13	337	-60	9	0.13
Concepcion Main	T-509	63504.97	94601.11	326.17	87.31	90.29	2.98	334	-58	446	5.17
Concepcion Main	T-510	63528.57	94602.00	312.37	100.18	103.40	3.22	332	-60	62	0.34
Concepcion Main	T-511	63575.52	94631.89	338.03	69.63	74.01	4.38	338	-59	182	1.36
Concepcion Main	T-512	63623.77	94648.95	331.49	71.84	82.29	10.45	337	-60	56	0.96
Concepcion Main	T-513	63666.30	94678.83	341.39	57.50	65.80	8.31	338	-61	70	1.22
Concepcion Main	T-514	63739.38	94700.76	356.79	35.98	43.64	7.66	337	-61	30	1.08
Concepcion Main	T-515	63823.75	94694.51	350.10	41.16	45.51	4.35	338	-62	121	1.59
Concepcion Main	T-516	63798.11	94683.17	341.38	53.29	56.73	3.43	339	-61	774	8.44
Concepcion Main	T-543	63472.33	94636.46	350.80	51.81	54.37	2.56	35	-60	3	0.06
Concepcion Main	T-544	63775.37	94605.87	263.24	128.07	134.62	6.55	0	-90	152	1.54
Concepcion Main	T-545	63788.78	94572.96	233.15	160.03	165.58	5.55	0	-90	82	0.67
Concepcion Main	T-546	63785.79	94646.60	301.82	86.23	91.86	5.63	0	-90	620	6.01
Concepcion Main	T-547	63839.98	94644.41	298.24	88.24	93.62	5.38	0	-90	262	1.89
Concepcion Main	T-548	63896.04	94639.43	278.05	107.62	113.15	5.53	0	-90	93	1.33
Concepcion Main	T-549	63915.23	94608.45	246.13	169.58	172.19	2.61	345	-60	22	0.22
Concepcion Main	T-550	63807.17	94539.96	197.33	223.38	226.65	3.27	340	-60	43	0.43
Concepcion Main	T-551	63594.93	94619.29	297.47	106.58	110.46	3.88	341	-72	13	0.08
Concepcion Main	T-552	63618.01	94603.95	265.77	153.50	156.29	2.79	343	-60	34	0.47
Concepcion Main	T-553	63522.09	94575.02	283.60	132.88	135.80	2.92	341	-61	219	0.55
Concepcion Main	T-554	63469.12	94603.99	318.68	94.03	96.66	2.63	14	-60	387	1.48
Concepcion Main	T-556	63929.60	94691.52	327.70	66.86	69.46	2.61	338	-61	112	2.22
Concepcion Main	T-557	63990.26	94676.20	292.08	108.85	111.73	2.88	340	-62	112	1.49
Concepcion Main	T-558	64041.76	94689.47	303.21	96.25	100.02	3.77	341	-61	12	0.16
Concepcion Main	T-559	63711.27	94632.95	279.30	167.94	170.52	2.58	341	-44	130	0.45
Concepcion Main	T-577	64025.85	94788.12	377.00	8.70	11.67	2.97	0	-90	4	0.03

Assay Composite Listing - Concepción Main Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Concepcion Main	T-578	64010.06	94760.69	360.40	25.30	28.38	3.08	0	-90	133	0.86
Concepcion Main	T-579	63961.79	94743.05	361.85	23.41	27.59	4.18	0	-90	17	0.11
Concepcion Main	T-581	63757.33	94720.79	377.15	16.43	21.27	4.84	342	-47	372	4.74
Concepcion Main	T-582	63732.24	94714.78	377.17	14.22	21.45	7.23	339	-61	24	0.31
Concepcion Main	T-583	63680.68	94708.38	381.45	11.08	20.24	9.16	341	-60	58	1.32
Concepcion Main	T-584	63595.42	94653.12	365.16	34.09	44.08	9.99	341	-59	12	0.21
Concepcion Main	T-585	63547.13	94639.59	370.82	37.83	43.36	5.53	341	-46	90	2.10
Concepcion Main	T-586	63496.16	94631.79	357.00	46.88	51.43	4.55	341	-60	500	4.84
Concepcion Main	T-587	64064.46	94771.54	364.94	24.40	26.76	2.36	0	-60	66	2.18
Concepcion Main	T-588	63836.98	94720.13	371.06	14.78	18.11	3.33	0	-90	30	0.18
Concepcion Main	T-589	63813.06	94713.00	365.77	20.45	24.83	4.38	0	-90	118	0.64
Concepcion Main	T-590	63828.07	94674.40	330.68	55.91	59.67	3.76	0	-90	171	2.57
Concepcion Main	T-591	63818.65	94642.20	295.75	113.95	117.73	3.78	342	-58	100	1.00
Concepcion Main	T-592	63801.10	94617.71	270.02	144.74	147.86	3.13	343	-60	110	1.64
Concepcion Main	T-593	63478.04	94650.54	367.67	31.54	34.22	2.68	32	-62	5	0.03
Concepcion Main	T-594	63449.30	94651.41	355.22	45.52	48.18	2.66	34	-59	7	0.15
Concepcion Main	T-595	63613.48	94620.07	288.08	127.92	131.05	3.14	345	-60	115	1.12
Concepcion Main	T-609	63700.02	94623.52	278.90	172.30	175.33	3.02	24	-42	101	0.83
Concepcion Main	T-610	63664.50	94614.74	272.25	144.26	147.15	2.89	342	-62	156	1.42
Concepcion Main	T-612	63702.91	94658.54	306.60	100.27	103.02	2.75	344	-61	63	1.40
Concepcion Main	T-613	63649.43	94654.24	314.90	92.23	97.49	5.27	339	-61	72	1.13
Concepcion Main	T-614	63634.71	94630.27	294.11	120.03	123.22	3.19	342	-61	54	0.56
Concepcion Main	T-616	63647.22	94592.06	250.39	167.42	170.13	2.71	339	-62	103	2.45
Concepcion Main	T-659	63912.81	94667.16	304.40	95.72	98.90	3.18	339	-61	102	1.21
Concepcion Main	T-660	63866.43	94649.40	300.13	102.15	106.44	4.29	348	-61	455	3.66
Concepcion Main	T-661	63509.21	94650.35	378.81	25.33	29.48	4.15	36	-46	61	0.71
Concepcion Main	T-664	63461.54	94667.28	380.30	18.22	20.81	2.59	36	-48	6	0.29

Assay Composite Listing - Concepción HG Vein

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Vein	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
	T-088	63722.84	94666.61	336.70	52.80	59.69	6.88	297	-89	133	1.86
	T-481	63692.32	94679.02	354.42	44.50	47.09	2.58	337	-61	49	0.26
	T-482	63674.68	94653.78	336.59	67.46	70.02	2.55	336	-60	55	0.57
	T-513	63668.90	94672.50	353.73	45.76	49.32	3.56	338	-61	26	0.35
	T-552	63626.07	94578.48	312.05	100.10	102.80	2.70	342	-60	589	2.37
	T-553	63527.44	94559.72	312.51	98.35	104.05	5.70	341	-61	68	0.51
	T-559	63713.89	94625.34	287.07	156.32	159.76	3.44	341	-44	31	0.25
	T-595	63620.05	94596.85	329.90	79.70	82.71	3.02	343	-60	247	1.40
	T-609	63693.26	94608.23	294.27	149.31	152.90	3.59	24	-43	205	1.14
	T-610	63669.74	94598.61	304.14	108.34	110.85	2.51	342	-62	464	2.49
	T-611	63639.20	94543.82	270.77	145.25	147.95	2.71	338	-60	7	0.03
	T-612	63705.73	94648.84	324.74	78.40	83.36	4.97	344	-61	40	0.23
	T-614	63640.41	94612.31	327.40	81.42	85.33	3.91	342	-61	241	2.00
	T-615	63597.16	94580.05	326.60	81.52	86.88	5.36	339	-61	79	0.61
	T-616	63654.95	94571.38	291.90	120.34	123.19	2.85	339	-62	1059	6.50
	T-617	63607.25	94552.36	279.05	135.69	140.67	4.98	337	-60	185	1.20

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	DDH-042	64656.61	94341.74	380.55	0.00	5.00	5.00	223	-51	0	0.00
Vertical	DDH-042	64654.45	94339.41	376.69	5.00	10.00	5.00	223	-51	0	0.00
Vertical	DDH-042	64652.28	94337.09	372.83	10.00	15.00	5.00	223	-51	13	0.13
Vertical	DDH-042	64650.11	94334.76	368.98	15.00	20.00	5.00	223	-51	40	0.35
Vertical	DDH-042	64647.94	94332.43	365.12	20.00	25.00	5.00	223	-51	23	0.18
Vertical	DDH-042	64645.77	94330.11	361.26	25.00	30.00	5.00	223	-51	30	0.20
Vertical	DDH-042	64643.60	94327.78	357.40	30.00	35.00	5.00	223	-51	24	0.11
Vertical	DDH-042	64641.43	94325.46	353.54	35.00	40.00	5.00	223	-51	25	0.16
Vertical	DDH-042	64639.26	94323.13	349.69	40.00	45.00	5.00	223	-51	88	0.85
Vertical	DDH-042	64637.09	94320.81	345.83	45.00	50.00	5.00	223	-51	14	0.21
Vertical	DDH-042	64634.93	94318.48	341.97	50.00	55.00	5.00	223	-51	6	0.07
Vertical	DDH-042	64632.75	94316.15	338.11	55.00	60.00	5.00	223	-51	49	0.45
Vertical	DDH-042	64630.59	94313.82	334.25	60.00	65.00	5.00	223	-51	32	0.30
Vertical	DDH-042	64628.42	94311.50	330.40	65.00	70.00	5.00	223	-51	18	0.21
Vertical	DDH-042	64626.25	94309.17	326.54	70.00	75.00	5.00	223	-51	14	0.18
Vertical	DDH-042	64624.08	94306.85	322.68	75.00	80.00	5.00	223	-51	16	0.19
Vertical	DDH-042	64621.91	94304.53	318.82	80.00	85.00	5.00	223	-51	24	0.28
Vertical	DDH-042	64619.74	94302.20	314.96	85.00	90.00	5.00	223	-51	82	0.59
Vertical	DDH-042	64617.57	94299.87	311.10	90.00	95.00	5.00	223	-51	20	0.16
Vertical	DDH-042	64615.40	94297.54	307.25	95.00	100.00	5.00	223	-51	14	0.10
Vertical	DDH-042	64613.23	94295.22	303.39	100.00	102.00	2.00	223	-51	18	0.12
A+B+C	DDH-042	64613.23	94295.22	303.39	102.00	105.00	3.00	223	-51	380	14.53
A+B+C	DDH-042	64611.07	94292.89	299.53	105.00	110.00	5.00	223	-51	662	5.70
A+B+C	DDH-042	64608.89	94290.57	295.67	110.00	115.00	5.00	223	-51	158	1.09
A+B+C	DDH-042	64606.73	94288.24	291.81	115.00	120.00	5.00	223	-51	68	0.39
A+B+C	DDH-042	64604.56	94285.92	287.96	120.00	125.00	5.00	223	-51	96	0.49
A+B+C	DDH-042	64602.39	94283.59	284.10	125.00	127.00	2.00	223	-51	608	3.36
Below A	DDH-042	64602.39	94283.59	284.10	127.00	130.00	3.00	223	-51	11	0.12
Below A	DDH-042	64600.22	94281.26	280.24	130.00	135.00	5.00	223	-51	34	0.30
Below A	DDH-042	64598.05	94278.94	276.38	135.00	140.00	5.00	223	-51	213	0.33
Below A	DDH-042	64595.88	94276.61	272.52	140.00	145.00	5.00	223	-51	16	0.07
Below A	DDH-042	64593.71	94274.28	268.67	145.00	150.00	5.00	223	-51	8	0.06
Below A	DDH-042	64591.54	94271.96	264.81	150.00	155.00	5.00	223	-51	0	0.00
Below A	DDH-042	64589.55	94269.82	261.25	155.00	157.00	2.00	223	-51	4	0.03
Below A	DDH-043	64410.68	94289.69	385.85	0.00	5.00	5.00	8	-61	1	0.06
Below A	DDH-043	64411.03	94292.13	381.50	5.00	10.00	5.00	8	-61	2	0.11
Below A	DDH-043	64411.37	94294.57	377.15	10.00	15.00	5.00	8	-61	1	0.20
Below A	DDH-043	64411.73	94297.00	372.80	15.00	20.00	5.00	8	-61	2	0.09
Below A	DDH-043	64412.09	94299.43	368.45	20.00	25.00	5.00	9	-61	5	0.17
Below A	DDH-043	64412.46	94301.86	364.10	25.00	30.00	5.00	9	-61	5	0.03
Below A	DDH-043	64412.84	94304.30	359.74	30.00	35.00	5.00	9	-61	2	0.08
Below A	DDH-043	64413.23	94306.74	355.39	35.00	40.00	5.00	9	-61	8	0.03
Below A	DDH-043	64413.61	94309.17	351.04	40.00	45.00	5.00	9	-61	15	0.10
Below A	DDH-043	64414.01	94311.59	346.69	45.00	50.00	5.00	10	-61	33	0.17
Below A	DDH-043	64414.42	94314.02	342.34	50.00	55.00	5.00	10	-61	2	0.03
Below A	DDH-043	64414.84	94316.44	337.98	55.00	60.00	5.00	10	-61	20	0.50
Below A	DDH-043	64415.28	94318.86	333.63	60.00	65.00	5.00	10	-61	5	0.10
Below A	DDH-043	64415.72	94321.28	329.28	65.00	70.00	5.00	11	-61	4	0.04
Below A	DDH-043	64416.18	94323.70	324.93	70.00	75.00	5.00	11	-61	5	0.04
Below A	DDH-043	64416.65	94326.11	320.58	75.00	80.00	5.00	11	-61	63	0.40
Below A	DDH-043	64417.13	94328.53	316.23	80.00	85.00	5.00	11	-61	2	0.19
Below A	DDH-043	64417.63	94330.94	311.87	85.00	90.00	5.00	12	-61	34	0.31
Below A	DDH-043	64418.14	94333.35	307.52	90.00	95.00	5.00	12	-61	6	0.07
Below A	DDH-043	64418.66	94335.75	303.17	95.00	100.00	5.00	13	-61	7	0.09

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	DDH-043	64419.20	94338.15	298.82	100.00	105.00	5.00	13	-61	5	0.06
Below A	DDH-043	64419.73	94340.55	294.47	105.00	110.00	5.00	13	-61	4	0.05
Below A	DDH-043	64420.28	94342.96	290.11	110.00	115.00	5.00	13	-61	1	0.02
Below A	DDH-043	64420.83	94345.35	285.76	115.00	120.00	5.00	13	-61	1	0.02
Below A	DDH-043	64421.39	94347.75	281.41	120.00	125.00	5.00	13	-61	4	0.05
Below A	DDH-043	64421.95	94350.16	277.06	125.00	130.00	5.00	13	-61	6	0.06
Below A	DDH-043	64422.52	94352.55	272.71	130.00	135.00	5.00	13	-61	25	0.26
Below A	DDH-043	64423.10	94354.94	268.36	135.00	140.00	5.00	14	-61	3	0.04
Below A	DDH-043	64423.68	94357.33	264.00	140.00	145.00	5.00	14	-61	3	0.03
Below A	DDH-043	64424.27	94359.72	259.65	145.00	150.00	5.00	14	-61	4	0.09
Below A	DDH-043	64424.87	94362.11	255.30	150.00	155.00	5.00	14	-61	2	0.03
Below A	DDH-043	64425.49	94364.51	250.96	155.00	160.00	5.00	15	-60	20	0.62
Below A	DDH-043	64426.11	94366.91	246.61	160.00	165.00	5.00	15	-60	127	1.01
Below A	DDH-043	64426.75	94369.31	242.28	165.00	170.00	5.00	15	-60	72	1.59
Below A	DDH-043	64427.41	94371.72	237.95	170.00	175.00	5.00	15	-60	2	0.03
Below A	DDH-043	64428.08	94374.14	233.62	175.00	176.00	1.00	16	-60	2	0.03
A+B+C	DDH-043	64428.08	94374.14	233.62	176.00	180.00	4.00	16	-60	5	0.07
A+B+C	DDH-043	64428.77	94376.57	229.30	180.00	185.00	5.00	16	-60	6	0.08
A+B+C	DDH-043	64429.46	94378.99	224.98	185.00	190.00	5.00	16	-60	11	0.14
A+B+C	DDH-043	64430.18	94381.42	220.68	190.00	195.00	5.00	16	-60	44	0.44
A+B+C	DDH-043	64430.92	94383.87	216.37	195.00	200.00	5.00	17	-59	13	0.15
A+B+C	DDH-043	64431.66	94386.31	212.07	200.00	205.00	5.00	17	-59	5	0.08
A+B+C	DDH-043	64432.42	94388.75	207.78	205.00	210.00	5.00	18	-59	3	0.04
A+B+C	DDH-043	64433.20	94391.19	203.49	210.00	215.00	5.00	18	-59	5	0.06
A+B+C	DDH-043	64433.99	94393.64	199.20	215.00	220.00	5.00	18	-59	3	0.05
A+B+C	DDH-043	64434.80	94396.09	194.91	220.00	223.05	3.05	18	-59	4	0.06
Vertical	DDH-043	64434.80	94396.09	194.91	223.05	225.00	1.95	18	-59	2	0.04
Vertical	DDH-043	64435.62	94398.54	190.63	225.00	230.00	5.00	19	-59	2	0.04
Vertical	DDH-043	64436.45	94401.00	186.35	230.00	235.00	5.00	19	-59	1	0.02
Vertical	DDH-043	64437.30	94403.45	182.08	235.00	240.00	5.00	19	-59	5	0.02
Vertical	DDH-043	64438.16	94405.89	177.81	240.00	245.00	5.00	19	-59	4	0.07
Vertical	DDH-043	64439.04	94408.35	173.54	245.00	250.00	5.00	20	-59	1	0.02
Karina	RDH-035	64809.96	94220.97	340.43	46.00	50.00	4.00	165	-56	94	1.35
Karina	RDH-035	64810.70	94218.23	336.31	50.00	52.00	2.00	165	-56	167	2.55
Below A	T-094	64511.24	94283.79	382.15	0.00	5.00	5.00	10	-50	1	0.01
Below A	T-094	64511.80	94286.96	378.32	5.00	10.00	5.00	10	-50	89	0.70
Below A	T-094	64512.36	94290.12	374.49	10.00	15.00	5.00	10	-50	25	0.31
Below A	T-094	64512.91	94293.28	370.66	15.00	20.00	5.00	10	-50	5	0.03
Below A	T-094	64513.47	94296.45	366.83	20.00	25.00	5.00	10	-50	5	0.03
Below A	T-094	64514.03	94299.61	363.00	25.00	30.00	5.00	10	-50	3	0.02
Below A	T-094	64514.59	94302.78	359.17	30.00	35.00	5.00	10	-50	2	0.03
Below A	T-094	64515.15	94305.95	355.34	35.00	40.00	5.00	10	-50	2	0.02
Below A	T-094	64515.70	94309.11	351.51	40.00	45.00	5.00	10	-50	2	0.02
Below A	T-094	64516.26	94312.28	347.68	45.00	50.00	5.00	10	-50	9	0.08
Below A	T-094	64516.82	94315.44	343.85	50.00	55.00	5.00	10	-50	1	0.01
Below A	T-094	64517.38	94318.60	340.02	55.00	60.00	5.00	10	-50	1	0.02
Below A	T-094	64517.94	94321.77	336.19	60.00	65.00	5.00	10	-50	23	0.32
Below A	T-094	64518.50	94324.93	332.36	65.00	70.00	5.00	10	-50	5	0.07
Below A	T-094	64519.05	94328.10	328.53	70.00	75.00	5.00	10	-50	1	0.03
Below A	T-094	64519.61	94331.27	324.70	75.00	80.00	5.00	10	-50	1	0.02
Below A	T-094	64520.17	94334.43	320.87	80.00	85.00	5.00	10	-50	5	0.08
Below A	T-094	64520.73	94337.60	317.04	85.00	90.00	5.00	10	-50	4	0.03
Below A	T-094	64521.29	94340.76	313.21	90.00	95.00	5.00	10	-50	8	0.25
Below A	T-094	64521.84	94343.92	309.38	95.00	100.00	5.00	10	-50	4	0.06

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-094	64522.40	94347.09	305.55	100.00	105.00	5.00	10	-50	13	0.16
Below A	T-094	64522.96	94350.25	301.72	105.00	110.00	5.00	10	-50	17	0.19
Below A	T-094	64523.52	94353.42	297.89	110.00	113.68	3.68	10	-50	52	0.51
A+B+C	T-094	64523.52	94353.42	297.89	113.68	115.00	1.32	10	-50	49	0.56
A+B+C	T-094	64524.07	94356.59	294.06	115.00	120.00	5.00	10	-50	37	0.44
A+B+C	T-094	64524.63	94359.75	290.23	120.00	125.00	5.00	10	-50	45	0.30
A+B+C	T-094	64525.19	94362.92	286.40	125.00	130.00	5.00	10	-50	31	0.33
A+B+C	T-094	64525.75	94366.08	282.57	130.00	135.00	5.00	10	-50	36	0.21
A+B+C	T-094	64526.31	94369.25	278.74	135.00	136.65	1.65	10	-50	34	0.34
Vertical	T-094	64526.31	94369.25	278.74	136.65	140.00	3.35	10	-50	24	0.19
Vertical	T-094	64526.87	94372.41	274.91	140.00	145.00	5.00	10	-50	9	0.14
Vertical	T-094	64527.43	94375.57	271.08	145.00	150.00	5.00	10	-50	58	0.81
Vertical	T-094	64527.98	94378.75	267.25	150.00	155.00	5.00	10	-50	785	9.18
Vertical	T-094	64528.54	94381.91	263.42	155.00	160.00	5.00	10	-50	232	8.21
Vertical	T-094	64529.10	94385.07	259.59	160.00	165.00	5.00	10	-50	579	12.87
Vertical	T-094	64529.66	94388.24	255.76	165.00	170.00	5.00	10	-50	137	3.11
Vertical	T-094	64530.21	94391.40	251.93	170.00	175.00	5.00	10	-50	107	1.99
Vertical	T-094	64530.77	94394.57	248.10	175.00	180.00	5.00	10	-50	156	2.83
Below A	T-095	64466.19	94317.08	385.40	0.00	5.00	5.00	10	-50	0	0.00
Below A	T-095	64466.75	94320.25	381.57	5.00	10.00	5.00	10	-50	0	0.00
Below A	T-095	64467.30	94323.41	377.74	10.00	15.00	5.00	10	-50	0	0.00
Below A	T-095	64467.86	94326.57	373.91	15.00	20.00	5.00	10	-50	0	0.00
Below A	T-095	64468.42	94329.74	370.08	20.00	25.00	5.00	10	-50	0	0.00
Below A	T-095	64468.98	94332.90	366.25	25.00	30.00	5.00	10	-50	0	0.00
Below A	T-095	64469.54	94336.07	362.42	30.00	35.00	5.00	10	-50	0	0.00
Below A	T-095	64470.10	94339.24	358.59	35.00	40.00	5.00	10	-50	26	0.25
Below A	T-095	64470.65	94342.40	354.76	40.00	45.00	5.00	10	-50	36	0.30
Below A	T-095	64471.21	94345.57	350.93	45.00	46.40	1.40	10	-50	22	0.44
A+B+C	T-095	64471.21	94345.57	350.93	46.40	50.00	3.60	10	-50	10	0.27
A+B+C	T-095	64471.77	94348.73	347.10	50.00	55.00	5.00	10	-50	56	0.53
A+B+C	T-095	64472.33	94351.89	343.27	55.00	60.00	5.00	10	-50	52	0.50
A+B+C	T-095	64472.89	94355.06	339.44	60.00	61.45	1.45	10	-50	30	0.22
Vertical	T-095	64472.89	94355.06	339.44	61.45	65.00	3.55	10	-50	18	0.17
Vertical	T-095	64473.45	94358.22	335.61	65.00	70.00	5.00	10	-50	8	0.08
Vertical	T-095	64474.00	94361.39	331.78	70.00	75.00	5.00	10	-50	26	0.35
Vertical	T-095	64474.56	94364.56	327.95	75.00	80.00	5.00	10	-50	7	0.15
Vertical	T-095	64475.12	94367.72	324.12	80.00	85.00	5.00	10	-50	20	0.19
Vertical	T-095	64475.68	94370.89	320.29	85.00	90.00	5.00	10	-50	5	0.08
Vertical	T-095	64476.23	94374.05	316.46	90.00	95.00	5.00	10	-50	23	0.27
Vertical	T-095	64476.79	94377.21	312.63	95.00	100.00	5.00	10	-50	3	0.08
Vertical	T-095	64477.35	94380.38	308.80	100.00	105.00	5.00	10	-50	4	0.09
Vertical	T-095	64477.91	94383.54	304.97	105.00	110.00	5.00	10	-50	30	0.37
Vertical	T-095	64478.47	94386.71	301.14	110.00	115.00	5.00	10	-50	9	0.12
Vertical	T-095	64479.02	94389.88	297.31	115.00	120.00	5.00	10	-50	7	0.15
Vertical	T-095	64479.58	94393.04	293.48	120.00	125.00	5.00	10	-50	165	3.93
Vertical	T-095	64480.14	94396.21	289.65	125.00	130.00	5.00	10	-50	73	0.92
Vertical	T-095	64480.70	94399.37	285.82	130.00	135.00	5.00	10	-50	62	0.76
Vertical	T-095	64481.26	94402.53	281.99	135.00	140.00	5.00	10	-50	27	0.33
Vertical	T-095	64481.82	94405.70	278.16	140.00	144.77	4.77	10	-50	22	0.40
Vertical	T-096	64609.37	94361.75	382.00	0.00	5.00	5.00	220	-50	0	0.00
Vertical	T-096	64607.30	94359.28	378.17	5.00	10.00	5.00	220	-50	0	0.00
Vertical	T-096	64605.23	94356.82	374.34	10.00	15.00	5.00	220	-50	0	0.00
Vertical	T-096	64603.17	94354.36	370.51	15.00	20.00	5.00	220	-50	24	0.21
Vertical	T-096	64601.10	94351.90	366.68	20.00	25.00	5.00	220	-50	36	0.42

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-096	64599.04	94349.44	362.85	25.00	30.00	5.00	220	-50	18	0.16
Vertical	T-096	64596.97	94346.98	359.02	30.00	35.00	5.00	220	-50	11	0.22
Vertical	T-096	64594.91	94344.51	355.19	35.00	40.00	5.00	220	-50	10	0.16
Vertical	T-096	64592.84	94342.05	351.36	40.00	45.00	5.00	220	-50	23	0.24
Vertical	T-096	64590.77	94339.59	347.53	45.00	50.00	5.00	220	-50	27	0.23
Vertical	T-096	64588.71	94337.13	343.70	50.00	55.00	5.00	220	-50	32	0.49
Vertical	T-096	64586.64	94334.67	339.87	55.00	60.00	5.00	220	-50	20	0.28
Vertical	T-096	64584.57	94332.21	336.04	60.00	65.00	5.00	220	-50	31	0.30
Vertical	T-096	64582.51	94329.75	332.21	65.00	67.82	2.82	220	-50	56	0.74
A+B+C	T-096	64582.51	94329.75	332.21	67.82	70.00	2.18	220	-50	210	2.85
A+B+C	T-096	64580.44	94327.28	328.38	70.00	75.00	5.00	220	-50	363	4.31
A+B+C	T-096	64578.38	94324.82	324.55	75.00	80.00	5.00	220	-50	152	1.47
A+B+C	T-096	64576.31	94322.35	320.72	80.00	85.00	5.00	220	-50	325	2.70
A+B+C	T-096	64574.25	94319.89	316.89	85.00	90.00	5.00	220	-50	255	1.73
A+B+C	T-096	64572.18	94317.43	313.06	90.00	95.00	5.00	220	-50	479	3.57
A+B+C	T-096	64570.11	94314.97	309.23	95.00	95.08	0.08	220	-50	404	4.53
Below A	T-096	64570.11	94314.97	309.23	95.08	100.00	4.92	220	-50	21	0.19
Below A	T-096	64568.05	94312.51	305.40	100.00	102.10	2.10	220	-50	19	0.13
Vertical	T-097	64686.68	94297.88	379.66	0.00	5.00	5.00	214	-50	0	0.00
Vertical	T-097	64684.88	94295.21	375.83	5.00	10.00	5.00	214	-50	15	0.33
Vertical	T-097	64683.09	94292.55	372.00	10.00	15.00	5.00	214	-50	17	0.15
Vertical	T-097	64681.29	94289.89	368.17	15.00	20.00	5.00	214	-50	34	0.33
Vertical	T-097	64679.49	94287.22	364.34	20.00	25.00	5.00	214	-50	22	0.12
Vertical	T-097	64677.70	94284.56	360.51	25.00	30.00	5.00	214	-50	47	0.28
Vertical	T-097	64675.89	94281.89	356.68	30.00	35.00	5.00	214	-50	8	0.03
Vertical	T-097	64674.10	94279.23	352.85	35.00	40.00	5.00	214	-50	8	0.05
Vertical	T-097	64672.30	94276.57	349.02	40.00	45.00	5.00	214	-50	14	0.14
Vertical	T-097	64670.50	94273.90	345.19	45.00	50.00	5.00	214	-50	12	0.12
Vertical	T-097	64668.71	94271.24	341.36	50.00	55.00	5.00	214	-50	39	0.26
Vertical	T-097	64666.91	94268.57	337.53	55.00	60.00	5.00	214	-50	28	0.34
Vertical	T-097	64665.11	94265.91	333.70	60.00	65.00	5.00	214	-50	17	0.10
Vertical	T-097	64663.32	94263.25	329.87	65.00	70.00	5.00	214	-50	24	0.11
Vertical	T-097	64661.52	94260.58	326.04	70.00	73.00	3.00	214	-50	20	0.09
A+B+C	T-097	64661.52	94260.58	326.04	73.00	75.00	2.00	214	-50	161	1.04
A+B+C	T-097	64659.72	94257.92	322.21	75.00	80.00	5.00	214	-50	299	1.79
A+B+C	T-097	64657.93	94255.25	318.38	80.00	85.00	5.00	214	-50	37	0.23
A+B+C	T-097	64656.12	94252.59	314.55	85.00	90.00	5.00	214	-50	6	0.03
A+B+C	T-097	64654.33	94249.92	310.72	90.00	95.00	5.00	214	-50	64	0.25
A+B+C	T-097	64652.53	94247.25	306.89	95.00	96.10	1.10	214	-50	52	0.48
Below A	T-097	64652.53	94247.25	306.89	96.10	100.00	3.90	214	-50	12	0.23
Below A	T-097	64650.73	94244.59	303.06	100.00	105.00	5.00	214	-50	19	0.30
Below A	T-097	64648.94	94241.92	299.23	105.00	110.00	5.00	214	-50	10	0.03
Below A	T-097	64647.14	94239.26	295.40	110.00	111.90	1.90	214	-50	8	0.02
Karina	T-099	64853.64	94231.99	335.59	54.60	55.00	0.40	165	-60	59	0.09
Karina	T-099	64854.29	94229.57	331.26	55.00	60.00	5.00	165	-60	15	0.08
Karina	T-099	64854.94	94227.16	326.93	60.00	65.00	5.00	165	-60	16	0.07
Karina	T-099	64855.59	94224.75	322.60	69.48	70.00	0.52	165	-60	72	0.17
Karina	T-100	64901.33	94246.87	317.04	65.00	70.00	5.00	165	-75	18	0.16
Karina	T-100	64901.66	94245.62	312.21	74.10	75.00	0.90	165	-75	12	0.14
Karina	T-101	64948.92	94264.60	326.29	60.27	65.00	4.73	165	-60	52	0.41
Karina	T-101	64949.56	94262.18	321.96	65.00	70.00	5.00	165	-60	58	0.49
Karina	T-101	64950.21	94259.77	317.63	70.00	75.00	5.00	165	-60	93	0.60
Karina	T-101	64950.86	94257.35	313.30	75.00	80.00	5.00	165	-60	36	0.95
Karina	T-101	64951.50	94254.94	308.97	80.00	80.77	0.77	165	-60	28	2.60

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-102	64723.85	94264.48	377.67	0.00	5.00	5.00	220	-50	1	0.13
Vertical	T-102	64721.78	94262.02	373.84	5.00	10.00	5.00	220	-50	8	0.37
Vertical	T-102	64719.71	94259.56	370.01	10.00	15.00	5.00	220	-50	14	0.39
Vertical	T-102	64717.65	94257.10	366.18	15.00	20.00	5.00	220	-50	13	0.20
Vertical	T-102	64715.58	94254.64	362.35	20.00	25.00	5.00	220	-50	13	0.14
Vertical	T-102	64713.52	94252.17	358.52	25.00	30.00	5.00	220	-50	18	0.15
Vertical	T-102	64711.45	94249.71	354.69	30.00	35.00	5.00	220	-50	16	0.08
Vertical	T-102	64709.39	94247.25	350.86	35.00	40.00	5.00	220	-50	17	0.16
Vertical	T-102	64707.32	94244.78	347.03	40.00	45.00	5.00	220	-50	11	0.11
Vertical	T-102	64705.25	94242.32	343.20	45.00	50.00	5.00	220	-50	19	0.37
Vertical	T-102	64703.19	94239.86	339.37	50.00	55.00	5.00	220	-50	9	0.09
Vertical	T-102	64701.12	94237.40	335.54	55.00	60.00	5.00	220	-50	10	0.11
Vertical	T-102	64699.05	94234.94	331.71	60.00	65.00	5.00	220	-50	11	0.08
Vertical	T-102	64696.99	94232.48	327.88	65.00	65.70	0.70	220	-50	6	0.06
A+B+C	T-102	64696.99	94232.48	327.88	65.70	70.00	4.30	220	-50	376	2.81
A+B+C	T-102	64694.92	94230.01	324.05	70.00	75.00	5.00	220	-50	45	0.44
A+B+C	T-102	64692.86	94227.55	320.22	75.00	78.54	3.54	220	-50	297	3.41
Below A	T-102	64692.86	94227.55	320.22	78.54	79.40	0.86	220	-50	19	0.16
Below A	T-123	64516.92	94323.52	384.60	0.00	5.00	5.00	10	-50	0	0.06
Below A	T-123	64517.48	94326.68	380.77	5.00	10.00	5.00	10	-50	2	0.12
Below A	T-123	64518.04	94329.85	376.94	10.00	15.00	5.00	10	-50	21	0.27
Below A	T-123	64518.59	94333.01	373.11	15.00	20.00	5.00	10	-50	5	0.14
Below A	T-123	64519.15	94336.17	369.28	20.00	25.00	5.00	10	-50	13	0.14
Below A	T-123	64519.71	94339.34	365.45	25.00	27.30	2.30	10	-50	41	0.29
A+B+C	T-123	64519.71	94339.34	365.45	27.30	30.00	2.70	10	-50	22	0.20
A+B+C	T-123	64520.27	94342.50	361.62	30.00	35.00	5.00	10	-50	28	0.19
A+B+C	T-123	64520.83	94345.67	357.79	35.00	40.00	5.00	10	-50	27	0.28
A+B+C	T-123	64521.38	94348.84	353.96	40.00	45.00	5.00	10	-50	22	0.20
A+B+C	T-123	64521.94	94352.00	350.13	45.00	46.60	1.60	10	-50	43	0.29
Vertical	T-123	64521.94	94352.00	350.13	46.60	50.00	3.40	10	-50	24	0.21
Vertical	T-123	64522.50	94355.17	346.30	50.00	55.00	5.00	10	-50	17	0.18
Vertical	T-123	64523.06	94358.33	342.47	55.00	60.00	5.00	10	-50	30	0.19
Vertical	T-123	64523.62	94361.50	338.64	60.00	65.00	5.00	10	-50	6	0.09
Vertical	T-123	64524.18	94364.66	334.81	65.00	70.00	5.00	10	-50	12	0.16
Vertical	T-123	64524.73	94367.82	330.98	70.00	75.00	5.00	10	-50	4	0.05
Vertical	T-123	64525.29	94371.00	327.15	75.00	80.00	5.00	10	-50	5	0.08
Vertical	T-123	64525.85	94374.16	323.32	80.00	85.00	5.00	10	-50	9	0.14
Vertical	T-123	64526.41	94377.32	319.49	85.00	90.00	5.00	10	-50	25	0.31
Vertical	T-123	64526.96	94380.49	315.66	90.00	95.00	5.00	10	-50	29	0.38
Vertical	T-123	64527.52	94383.65	311.83	95.00	100.00	5.00	10	-50	63	0.80
Vertical	T-123	64528.08	94386.82	308.00	100.00	105.00	5.00	10	-50	67	1.16
Vertical	T-123	64528.64	94389.98	304.17	105.00	110.00	5.00	10	-50	391	3.82
Vertical	T-123	64529.20	94393.15	300.34	110.00	115.00	5.00	10	-50	14	0.18
Vertical	T-123	64529.75	94396.32	296.51	115.00	120.00	5.00	10	-50	69	0.61
Vertical	T-123	64530.31	94399.48	292.68	120.00	125.00	5.00	10	-50	16	0.22
Vertical	T-123	64530.87	94402.64	288.85	125.00	130.00	5.00	10	-50	23	0.21
Vertical	T-123	64531.43	94405.81	285.02	130.00	135.00	5.00	10	-50	43	0.36
Vertical	T-123	64531.99	94408.97	281.19	135.00	140.00	5.00	10	-50	3	0.06
Vertical	T-123	64532.53	94412.03	277.49	140.00	142.00	2.00	10	-50	3	0.02
Vertical	T-124	64643.35	94405.50	380.00	0.00	5.00	5.00	217	-45	0	0.00
Vertical	T-124	64641.22	94402.67	376.47	5.00	10.00	5.00	217	-45	0	0.00
Vertical	T-124	64639.09	94399.85	372.93	10.00	15.00	5.00	217	-45	0	0.00
Vertical	T-124	64636.96	94397.03	369.40	15.00	20.00	5.00	217	-45	0	0.00
Vertical	T-124	64634.84	94394.21	365.86	20.00	25.00	5.00	217	-45	0	0.00

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-124	64632.71	94391.38	362.32	25.00	30.00	5.00	217	-45	0	0.00
Vertical	T-124	64630.58	94388.56	358.79	30.00	35.00	5.00	217	-45	364	3.69
Vertical	T-124	64628.45	94385.73	355.25	35.00	40.00	5.00	217	-45	86	0.62
Vertical	T-124	64626.32	94382.91	351.72	40.00	45.00	5.00	217	-45	21	0.14
Vertical	T-124	64624.20	94380.09	348.18	45.00	50.00	5.00	217	-45	16	0.13
Vertical	T-124	64622.07	94377.26	344.65	50.00	55.00	5.00	217	-45	25	0.26
Vertical	T-124	64619.94	94374.44	341.11	55.00	60.00	5.00	217	-45	16	0.15
Vertical	T-124	64617.81	94371.61	337.58	60.00	65.00	5.00	217	-45	31	0.55
Vertical	T-124	64615.69	94368.79	334.04	65.00	70.00	5.00	217	-45	62	0.36
Vertical	T-124	64613.56	94365.96	330.50	70.00	75.00	5.00	217	-45	13	0.12
Vertical	T-124	64611.43	94363.14	326.97	75.00	80.00	5.00	217	-45	86	1.04
Vertical	T-124	64609.30	94360.32	323.43	80.00	85.00	5.00	217	-45	12	0.11
Vertical	T-124	64607.18	94357.50	319.90	85.00	90.00	5.00	217	-45	73	0.73
Vertical	T-124	64605.05	94354.67	316.36	90.00	95.00	5.00	217	-45	18	0.20
Vertical	T-124	64602.92	94351.85	312.83	95.00	100.00	5.00	217	-45	34	0.36
Vertical	T-124	64600.79	94349.03	309.29	100.00	105.00	5.00	217	-45	19	0.16
Vertical	T-124	64598.66	94346.20	305.76	105.00	110.00	5.00	217	-45	109	1.32
Vertical	T-124	64596.54	94343.38	302.22	110.00	115.00	5.00	217	-45	51	0.37
Vertical	T-124	64594.41	94340.56	298.68	115.00	120.00	5.00	217	-45	15	0.14
Vertical	T-124	64592.28	94337.73	295.15	120.00	125.00	5.00	217	-45	25	0.29
Vertical	T-124	64590.15	94334.91	291.61	125.00	130.00	5.00	217	-45	46	0.64
Vertical	T-124	64588.02	94332.08	288.08	130.00	134.10	4.10	217	-45	16	0.07
A+B+C	T-124	64588.02	94332.08	288.08	134.10	135.00	0.90	217	-45	503	6.72
A+B+C	T-124	64585.90	94329.26	284.54	135.00	140.00	5.00	217	-45	306	4.41
A+B+C	T-124	64583.77	94326.44	281.01	140.70	145.00	4.30	217	-45	261	3.60
Below A	T-124	64583.77	94326.44	281.01	144.30	145.00	0.70	217	-45	26	0.16
Below A	T-124	64581.64	94323.61	277.47	145.00	150.00	5.00	217	-45	16	0.15
Below A	T-124	64579.52	94320.79	273.94	150.00	150.50	0.50	217	-45	2	0.03
Vertical	T-125	64474.29	94372.13	386.58	0.00	5.00	5.00	15	-50	1	0.01
Vertical	T-125	64475.12	94375.23	382.75	5.00	10.00	5.00	15	-50	4	0.09
Vertical	T-125	64475.95	94378.33	378.92	10.00	15.00	5.00	15	-50	2	0.05
Vertical	T-125	64476.78	94381.44	375.09	15.00	20.00	5.00	15	-50	8	0.13
Vertical	T-125	64477.61	94384.54	371.26	20.00	25.00	5.00	15	-50	17	0.33
Vertical	T-125	64478.45	94387.65	367.43	25.00	30.00	5.00	15	-50	2	0.11
Vertical	T-125	64479.28	94390.75	363.60	30.00	35.00	5.00	15	-50	8	0.14
Vertical	T-125	64480.11	94393.85	359.77	35.00	40.00	5.00	15	-50	2	0.03
Vertical	T-125	64480.94	94396.96	355.94	40.00	45.00	5.00	15	-50	3	0.12
Vertical	T-125	64481.77	94400.07	352.11	45.00	50.00	5.00	15	-50	25	0.32
Vertical	T-125	64482.61	94403.17	348.28	50.00	55.00	5.00	15	-50	23	0.26
Vertical	T-125	64483.44	94406.28	344.45	55.00	60.00	5.00	15	-50	4	0.09
Vertical	T-125	64484.27	94409.38	340.62	60.00	65.00	5.00	15	-50	30	0.43
Vertical	T-125	64485.10	94412.48	336.79	65.00	70.00	5.00	15	-50	110	1.18
Vertical	T-125	64485.93	94415.59	332.96	70.00	75.00	5.00	15	-50	7	0.14
Vertical	T-125	64486.77	94418.69	329.13	75.00	80.00	5.00	15	-50	7	0.10
Vertical	T-125	64487.60	94421.80	325.30	80.00	85.00	5.00	15	-50	2	0.04
Vertical	T-125	64488.43	94424.90	321.47	85.00	90.00	5.00	15	-50	7	0.13
Vertical	T-125	64489.26	94428.00	317.64	90.00	95.00	5.00	15	-50	3	0.08
Vertical	T-125	64490.09	94431.11	313.81	95.00	95.50	0.50	15	-50	1	0.02
Vertical	T-126	64427.09	94379.05	389.04	0.00	5.00	5.00	10	-50	0	0.00
Vertical	T-126	64427.62	94382.22	385.21	5.00	10.00	5.00	10	-50	14	0.09
Vertical	T-126	64428.14	94385.39	381.38	10.00	15.00	5.00	10	-50	15	0.25
Vertical	T-126	64428.68	94388.56	377.55	15.00	20.00	5.00	10	-50	12	0.29
Vertical	T-126	64429.21	94391.73	373.72	20.00	25.00	5.00	10	-50	5	0.03
Vertical	T-126	64429.74	94394.90	369.89	25.00	30.00	5.00	10	-50	6	0.06

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-126	64430.27	94398.07	366.06	30.00	35.00	5.00	10	-50	67	1.37
Vertical	T-126	64430.80	94401.24	362.23	35.00	40.00	5.00	10	-50	8	0.15
Vertical	T-126	64431.33	94404.41	358.40	40.00	45.00	5.00	10	-50	14	0.21
Vertical	T-126	64431.86	94407.58	354.57	45.00	50.00	5.00	10	-50	17	0.19
Vertical	T-126	64432.39	94410.75	350.74	50.00	55.00	5.00	10	-50	3	0.05
Vertical	T-126	64432.92	94413.92	346.91	55.00	60.00	5.00	10	-50	2	0.04
Vertical	T-126	64433.45	94417.09	343.08	60.00	65.00	5.00	10	-50	4	0.09
Vertical	T-126	64433.98	94420.26	339.25	65.00	70.00	5.00	10	-50	11	0.16
Vertical	T-126	64434.51	94423.42	335.42	70.00	75.00	5.00	10	-50	43	0.46
Vertical	T-126	64435.04	94426.60	331.59	75.00	80.00	5.00	10	-50	54	0.60
Vertical	T-126	64435.57	94429.77	327.76	80.00	85.00	5.00	10	-50	2	0.04
Vertical	T-126	64436.10	94432.93	323.93	85.00	90.00	5.00	10	-50	2	0.03
Vertical	T-126	64436.63	94436.10	320.10	90.00	95.00	5.00	10	-50	79	0.72
Vertical	T-126	64437.16	94439.28	316.27	95.00	100.00	5.00	10	-50	41	0.45
Vertical	T-138	64606.26	94374.03	382.44	0.00	5.00	5.00	10	-45	13	0.17
Vertical	T-138	64606.87	94377.51	378.91	5.00	10.00	5.00	10	-45	45	0.70
Vertical	T-138	64607.48	94380.99	375.37	10.00	15.00	5.00	10	-45	50	0.22
Vertical	T-138	64608.10	94384.47	371.84	15.00	20.00	5.00	10	-45	15	0.07
Vertical	T-138	64608.71	94387.96	368.30	20.00	25.00	5.00	10	-45	7	0.10
Vertical	T-138	64609.32	94391.43	364.76	25.00	30.00	5.00	10	-45	49	0.32
Vertical	T-138	64609.94	94394.92	361.23	30.00	35.00	5.00	10	-45	3	0.05
Vertical	T-138	64610.55	94398.40	357.69	35.00	40.00	5.00	10	-45	54	0.28
Vertical	T-138	64611.10	94401.50	354.54	40.00	43.90	3.90	10	-45	9	0.11
Vertical	T-139	64655.80	94367.00	380.70	0.00	5.00	5.00	10	-45	0	0.00
Vertical	T-139	64656.41	94370.49	377.17	5.00	10.00	5.00	10	-45	22	0.13
Vertical	T-139	64657.02	94373.96	373.63	10.00	15.00	5.00	10	-45	18	0.24
Vertical	T-139	64657.64	94377.45	370.10	15.00	20.00	5.00	10	-45	13	0.15
Vertical	T-139	64658.25	94380.93	366.56	20.00	25.00	5.00	10	-45	5	0.03
Vertical	T-139	64658.86	94384.41	363.02	25.00	30.00	5.00	10	-45	26	0.12
Vertical	T-139	64659.48	94387.89	359.49	30.00	35.00	5.00	10	-45	17	0.11
Vertical	T-139	64660.09	94391.38	355.95	35.00	40.00	5.00	10	-45	13	0.13
Vertical	T-139	64660.45	94393.42	353.87	40.00	40.90	0.90	10	-45	17	0.05
Vertical	T-175	64692.48	94267.65	378.53	0.00	5.00	5.00	221	-45	3	0.05
Vertical	T-175	64690.18	94264.96	375.00	5.00	10.00	5.00	221	-45	10	0.12
Vertical	T-175	64687.89	94262.28	371.46	10.00	15.00	5.00	221	-45	13	0.10
Vertical	T-175	64685.59	94259.59	367.93	15.00	20.00	5.00	221	-45	51	0.49
Vertical	T-175	64683.30	94256.89	364.39	20.00	25.00	5.00	221	-45	14	0.20
Vertical	T-175	64681.00	94254.21	360.85	25.00	30.00	5.00	221	-45	37	0.26
Vertical	T-175	64678.70	94251.52	357.32	30.00	35.00	5.00	221	-45	29	0.14
Vertical	T-175	64676.41	94248.83	353.78	35.00	40.00	5.00	221	-45	14	0.06
Vertical	T-175	64674.11	94246.14	350.25	40.00	45.00	5.00	221	-45	16	0.05
Vertical	T-175	64671.82	94243.46	346.71	45.00	46.69	1.69	221	-45	65	0.09
A+B+C	T-175	64671.82	94243.46	346.71	46.69	50.00	3.31	221	-45	186	1.53
A+B+C	T-175	64669.52	94240.77	343.18	50.00	55.00	5.00	221	-45	252	4.45
A+B+C	T-175	64667.22	94238.08	339.64	55.00	60.00	5.00	221	-45	13	0.08
A+B+C	T-175	64664.93	94235.39	336.11	60.00	65.00	5.00	221	-45	273	1.52
A+B+C	T-175	64662.63	94232.70	332.57	65.00	70.00	5.00	221	-45	187	1.08
Below A	T-175	64660.34	94230.01	329.03	70.00	75.00	5.00	221	-45	101	0.37
Below A	T-175	64658.04	94227.32	325.50	75.00	80.00	5.00	221	-45	37	0.20
Below A	T-175	64655.74	94224.64	321.96	80.00	85.00	5.00	221	-45	5	0.04
Below A	T-175	64653.45	94221.95	318.43	85.00	90.00	5.00	221	-45	0	0.00
Below A	T-175	64651.15	94219.26	314.89	90.00	95.00	5.00	221	-45	26	0.06
Below A	T-175	64648.86	94216.57	311.36	95.00	100.00	5.00	221	-45	5	0.03
Below A	T-175	64646.56	94213.89	307.82	100.00	105.00	5.00	221	-45	4	0.02

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-175	64644.26	94211.19	304.29	105.00	110.00	5.00	221	-45	4	0.02
Below A	T-175	64642.74	94209.41	301.94	110.00	111.63	1.63	221	-45	4	0.05
Vertical	T-176	64651.37	94295.10	380.78	0.00	5.00	5.00	220	-45	0	0.00
Vertical	T-176	64649.10	94292.39	377.25	5.00	10.00	5.00	220	-45	42	0.12
Vertical	T-176	64646.83	94289.68	373.71	10.00	15.00	5.00	220	-45	102	0.27
Vertical	T-176	64644.56	94286.98	370.18	15.00	20.00	5.00	220	-45	141	0.35
Vertical	T-176	64642.29	94284.27	366.64	20.00	25.00	5.00	220	-45	187	0.27
Vertical	T-176	64640.01	94281.56	363.10	25.00	30.00	5.00	220	-45	53	0.18
Vertical	T-176	64637.74	94278.85	359.57	30.00	34.90	4.90	220	-45	71	0.42
A+B+C	T-176	64637.74	94278.85	359.57	34.90	35.00	0.10	220	-45	188	2.05
A+B+C	T-176	64635.47	94276.14	356.03	35.00	40.00	5.00	220	-45	357	2.58
A+B+C	T-176	64633.20	94273.43	352.50	40.00	45.00	5.00	220	-45	50	0.43
A+B+C	T-176	64630.92	94270.73	348.96	45.00	50.00	5.00	220	-45	211	2.81
A+B+C	T-176	64628.65	94268.02	345.43	50.00	55.00	5.00	220	-45	272	1.69
A+B+C	T-176	64626.37	94265.31	341.89	55.00	60.00	5.00	220	-45	372	1.73
A+B+C	T-176	64624.11	94262.60	338.36	60.00	65.00	5.00	220	-45	203	0.90
A+B+C	T-176	64621.83	94259.89	334.82	65.00	70.00	5.00	220	-45	935	6.32
A+B+C	T-176	64619.56	94257.18	331.28	70.00	75.00	5.00	220	-45	258	1.54
A+B+C	T-176	64617.29	94254.48	327.75	75.00	80.00	5.00	220	-45	246	1.54
A+B+C	T-176	64615.02	94251.77	324.21	80.00	85.00	5.00	220	-45	181	1.12
A+B+C	T-176	64612.74	94249.06	320.68	85.00	85.10	0.10	220	-45	73	0.29
Below A	T-176	64612.74	94249.06	320.68	85.10	90.00	4.90	220	-45	51	0.21
Below A	T-176	64610.47	94246.35	317.14	90.00	95.00	5.00	220	-45	67	0.32
Below A	T-176	64608.20	94243.64	313.61	95.00	100.00	5.00	220	-45	41	0.28
Below A	T-176	64605.92	94240.93	310.07	102.00	105.00	3.00	220	-45	17	0.10
Vertical	T-177	64617.72	94330.76	382.71	0.00	5.00	5.00	220	-47	30	0.26
Vertical	T-177	64615.55	94328.13	379.05	5.00	10.00	5.00	220	-47	68	0.42
Vertical	T-177	64613.39	94325.50	375.40	10.00	15.00	5.00	220	-47	41	0.21
Vertical	T-177	64611.22	94322.86	371.74	15.00	20.00	5.00	220	-47	341	3.71
Vertical	T-177	64609.05	94320.23	368.08	20.00	25.00	5.00	220	-47	149	0.74
Vertical	T-177	64606.88	94317.60	364.43	25.00	30.00	5.00	220	-47	238	2.40
Vertical	T-177	64604.71	94314.97	360.77	30.00	35.00	5.00	220	-47	153	0.84
Vertical	T-177	64602.54	94312.34	357.11	35.00	37.50	2.50	220	-47	898	5.21
A+B+C	T-177	64602.54	94312.34	357.11	37.50	40.00	2.50	220	-47	85	0.91
A+B+C	T-177	64600.37	94309.71	353.46	40.00	45.00	5.00	220	-47	14	0.16
A+B+C	T-177	64598.20	94307.07	349.80	45.00	50.00	5.00	220	-47	495	5.69
A+B+C	T-177	64596.04	94304.45	346.14	50.00	55.00	5.00	220	-47	154	1.04
A+B+C	T-177	64593.86	94301.82	342.49	55.00	60.00	5.00	220	-47	120	0.93
A+B+C	T-177	64591.70	94299.18	338.83	60.00	65.00	5.00	220	-47	102	0.54
A+B+C	T-177	64589.53	94296.55	335.17	65.00	70.00	5.00	220	-47	491	3.87
A+B+C	T-177	64587.36	94293.92	331.52	70.00	75.00	5.00	220	-47	51	0.29
Below A	T-177	64585.19	94291.29	327.86	76.00	80.00	4.00	220	-47	30	0.18
A+B+C	T-177	64585.19	94291.29	327.86	79.00	80.00	1.00	220	-47	40	0.17
Below A	T-177	64583.02	94288.66	324.20	80.00	85.00	5.00	220	-47	95	0.53
Below A	T-177	64580.85	94286.03	320.55	85.00	90.00	5.00	220	-47	45	0.44
Below A	T-177	64578.68	94283.39	316.89	90.00	95.00	5.00	220	-47	39	0.85
Below A	T-177	64577.20	94281.60	314.39	95.00	96.38	1.38	220	-47	75	0.72
Vertical	T-178	64593.51	94389.10	381.87	0.00	5.00	5.00	223	-60	2	0.01
Vertical	T-178	64591.80	94387.27	377.54	5.00	10.00	5.00	223	-60	53	0.40
Vertical	T-178	64590.10	94385.44	373.21	10.00	15.00	5.00	223	-60	11	0.06
Vertical	T-178	64588.39	94383.61	368.88	15.00	20.00	5.00	223	-60	42	0.30
Vertical	T-178	64586.69	94381.78	364.55	20.00	25.00	5.00	223	-60	13	0.14
Vertical	T-178	64584.98	94379.96	360.22	25.00	30.00	5.00	223	-60	14	0.18
Vertical	T-178	64583.28	94378.13	355.89	30.00	35.00	5.00	223	-60	7	0.15

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-178	64581.57	94376.30	351.56	35.00	40.00	5.00	223	-60	14	0.15
Vertical	T-178	64579.87	94374.47	347.23	40.00	45.00	5.00	223	-60	112	0.79
Vertical	T-178	64578.16	94372.64	342.90	45.00	50.00	5.00	223	-60	71	0.65
Vertical	T-178	64576.46	94370.82	338.57	50.00	55.00	5.00	223	-60	10	0.12
Vertical	T-178	64574.75	94368.99	334.24	55.00	60.00	5.00	223	-60	8	0.13
Vertical	T-178	64573.05	94367.16	329.91	60.00	65.00	5.00	223	-60	43	0.81
Vertical	T-178	64571.34	94365.33	325.58	65.00	70.00	5.00	223	-60	64	0.28
Vertical	T-178	64569.64	94363.50	321.25	70.00	75.00	5.00	223	-60	61	0.48
Vertical	T-178	64567.93	94361.67	316.92	75.00	80.00	5.00	223	-60	63	0.67
Vertical	T-178	64566.23	94359.84	312.59	80.00	85.00	5.00	223	-60	337	3.82
Vertical	T-178	64564.52	94358.01	308.26	85.00	90.00	5.00	223	-60	32	0.29
Vertical	T-178	64562.82	94356.18	303.93	90.00	92.50	2.50	223	-60	10	0.08
A+B+C	T-178	64562.82	94356.18	303.93	92.50	95.00	2.50	223	-60	281	3.30
A+B+C	T-178	64561.11	94354.35	299.60	95.00	100.00	5.00	223	-60	583	3.53
A+B+C	T-178	64559.41	94352.53	295.27	100.00	105.00	5.00	223	-60	538	8.33
A+B+C	T-178	64557.70	94350.70	290.94	105.00	110.00	5.00	223	-60	113	2.45
Below A	T-178	64556.00	94348.87	286.61	111.10	115.00	3.90	223	-60	89	0.91
A+B+C	T-178	64556.00	94348.87	286.61	113.90	115.00	1.10	223	-60	1268	10.70
Below A	T-178	64554.29	94347.04	282.28	115.00	120.00	5.00	223	-60	19	0.25
Below A	T-178	64552.59	94345.21	277.95	120.00	125.00	5.00	223	-60	11	0.13
Below A	T-178	64550.89	94343.40	273.65	125.00	125.13	0.13	223	-60	0	0.02
Vertical	T-179	64578.02	94373.53	383.20	0.00	5.00	5.00	226	-45	1	0.00
Vertical	T-179	64575.47	94371.07	379.67	5.00	10.00	5.00	226	-45	13	0.03
Vertical	T-179	64572.93	94368.62	376.13	10.00	15.00	5.00	226	-45	8	0.06
Vertical	T-179	64570.39	94366.17	372.60	15.00	20.00	5.00	226	-45	5	0.03
Vertical	T-179	64567.84	94363.71	369.06	20.00	25.00	5.00	226	-45	6	0.06
Vertical	T-179	64565.30	94361.25	365.52	25.00	30.00	5.00	226	-45	29	0.21
Vertical	T-179	64562.76	94358.80	361.99	30.00	35.00	5.00	226	-45	26	0.27
Vertical	T-179	64560.21	94356.34	358.45	35.00	40.00	5.00	226	-45	8	0.11
Vertical	T-179	64557.67	94353.89	354.92	40.00	45.00	5.00	226	-45	26	0.21
Vertical	T-179	64555.13	94351.43	351.38	45.00	50.00	5.00	226	-45	11	0.11
Vertical	T-179	64552.59	94348.97	347.85	50.00	55.00	5.00	226	-45	10	0.14
Vertical	T-179	64550.04	94346.52	344.31	55.00	60.00	5.00	226	-45	26	0.17
Vertical	T-179	64547.50	94344.06	340.78	60.00	61.20	1.20	226	-45	7	0.08
A+B+C	T-179	64547.50	94344.06	340.78	61.20	65.00	3.80	226	-45	21	0.17
A+B+C	T-179	64544.96	94341.60	337.24	65.00	70.00	5.00	226	-45	10	0.16
A+B+C	T-179	64542.41	94339.15	333.70	70.00	71.50	1.50	226	-45	13	0.13
Below A	T-179	64542.41	94339.15	333.70	71.50	75.00	3.50	226	-45	15	0.14
Below A	T-179	64539.87	94336.69	330.17	75.00	80.00	5.00	226	-45	34	0.27
Below A	T-179	64537.32	94334.24	326.63	80.00	85.00	5.00	226	-45	15	0.17
Below A	T-179	64534.78	94331.78	323.10	85.00	90.00	5.00	226	-45	68	0.45
Below A	T-179	64532.66	94329.74	320.15	90.00	93.33	3.33	226	-45	1	0.02
Vertical	T-181	64449.74	94477.32	380.25	0.00	5.00	5.00	229	-45	0	0.00
Vertical	T-181	64447.07	94475.00	376.72	5.00	10.00	5.00	229	-45	0	0.00
Vertical	T-181	64444.41	94472.68	373.18	10.00	15.00	5.00	229	-45	0	0.00
Vertical	T-181	64441.74	94470.36	369.65	15.00	20.00	5.00	229	-45	0	0.00
Vertical	T-181	64439.07	94468.04	366.11	20.00	25.00	5.00	229	-45	0	0.00
Vertical	T-181	64436.40	94465.72	362.57	25.00	30.00	5.00	229	-45	0	0.00
Vertical	T-181	64433.73	94463.40	359.04	30.00	35.00	5.00	229	-45	0	0.00
Vertical	T-181	64431.07	94461.08	355.50	35.00	40.00	5.00	229	-45	0	0.00
Vertical	T-181	64428.40	94458.76	351.97	40.00	45.00	5.00	229	-45	0	0.00
Vertical	T-181	64425.73	94456.44	348.43	45.00	50.00	5.00	229	-45	0	0.00
Vertical	T-181	64423.06	94454.13	344.90	50.00	55.00	5.00	229	-45	0	0.00
Vertical	T-181	64420.39	94451.81	341.36	55.00	60.00	5.00	229	-45	0	0.00

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-181	64417.72	94449.49	337.83	60.00	65.00	5.00	229	-45	0	0.00
Vertical	T-181	64415.34	94447.42	334.67	65.00	68.93	3.93	229	-45	0	0.00
Karina	T-183	64789.43	94196.21	370.25	12.60	15.00	2.40	165	-49	182	1.82
Karina	T-183	64790.28	94193.00	366.50	15.00	20.00	5.00	165	-49	74	0.74
Karina	T-183	64791.14	94189.81	362.76	20.00	25.00	5.00	165	-49	59	0.48
Karina	T-183	64792.00	94186.60	359.01	28.90	30.00	1.10	165	-49	82	0.62
Karina	T-184	64948.04	94248.70	371.24	17.10	20.00	2.90	165	-46	23	0.48
Karina	T-184	64948.95	94245.35	367.64	20.00	25.00	5.00	165	-46	61	0.81
Karina	T-184	64949.84	94241.99	364.05	25.00	30.00	5.00	165	-46	30	0.33
Karina	T-184	64950.74	94238.64	360.45	30.00	34.10	4.10	165	-46	51	0.65
Below A	T-185	64457.61	94312.49	385.62	0.00	5.00	5.00	41	-61	0	0.00
Below A	T-185	64459.20	94314.32	381.25	5.00	10.00	5.00	41	-61	0	0.00
Below A	T-185	64460.79	94316.14	376.88	10.00	15.00	5.00	41	-61	0	0.00
Below A	T-185	64462.37	94317.98	372.50	15.00	20.00	5.00	41	-61	0	0.00
Below A	T-185	64463.96	94319.81	368.13	20.00	25.00	5.00	41	-61	0	0.00
Below A	T-185	64465.55	94321.64	363.76	25.00	30.00	5.00	41	-61	0	0.00
Below A	T-185	64467.14	94323.46	359.38	30.00	35.00	5.00	41	-61	33	0.24
Below A	T-185	64468.73	94325.29	355.01	35.00	40.00	5.00	41	-61	3	0.04
Below A	T-185	64470.33	94327.12	350.64	40.00	45.00	5.00	41	-61	0	0.00
Below A	T-185	64471.92	94328.96	346.27	45.00	50.00	5.00	41	-61	0	0.00
Below A	T-185	64473.51	94330.78	341.89	50.00	55.00	5.00	41	-61	0	0.00
Below A	T-185	64475.10	94332.61	337.52	55.00	60.00	5.00	41	-61	0	0.02
Below A	T-185	64476.69	94334.44	333.15	60.00	65.00	5.00	41	-61	9	0.11
Below A	T-185	64478.28	94336.27	328.77	65.00	70.00	5.00	41	-61	0	0.00
Below A	T-185	64479.87	94338.10	324.40	70.00	75.00	5.00	41	-61	0	0.00
Below A	T-185	64481.46	94339.93	320.03	75.00	80.00	5.00	41	-61	0	0.00
Below A	T-185	64483.05	94341.76	315.65	80.00	85.00	5.00	41	-61	0	0.00
Below A	T-185	64484.64	94343.59	311.28	85.00	90.00	5.00	41	-61	0	0.00
Below A	T-185	64486.23	94345.42	306.91	90.00	95.00	5.00	41	-61	0	0.00
Below A	T-185	64487.82	94347.25	302.53	95.00	100.00	5.00	41	-61	0	0.00
Below A	T-185	64489.41	94349.07	298.16	100.00	101.60	1.60	41	-61	0	0.00
A+B+C	T-185	64489.41	94349.07	298.16	101.60	105.00	3.40	41	-61	669	4.83
A+B+C	T-185	64491.00	94350.91	293.79	105.00	110.00	5.00	41	-61	153	1.10
A+B+C	T-185	64492.59	94352.74	289.42	110.00	115.00	5.00	41	-61	28	0.23
A+B+C	T-185	64494.18	94354.57	285.04	115.00	120.00	5.00	41	-61	0	0.00
A+B+C	T-185	64495.77	94356.39	280.67	120.00	125.00	5.00	41	-61	40	0.66
A+B+C	T-185	64497.36	94358.22	276.30	125.00	130.00	5.00	41	-61	46	0.49
A+B+C	T-185	64498.95	94360.05	271.92	130.00	135.00	5.00	41	-61	30	0.36
A+B+C	T-185	64500.54	94361.89	267.55	135.00	140.00	5.00	41	-61	129	1.64
A+B+C	T-185	64502.13	94363.71	263.18	140.00	145.00	5.00	41	-61	20	0.45
A+B+C	T-185	64503.72	94365.54	258.80	145.00	150.00	5.00	41	-61	32	0.70
A+B+C	T-185	64505.31	94367.37	254.43	150.00	155.00	5.00	41	-61	34	0.41
A+B+C	T-185	64506.90	94369.20	250.06	155.00	160.00	5.00	41	-61	0	0.00
A+B+C	T-185	64508.49	94371.03	245.68	160.00	165.00	5.00	41	-61	22	1.14
A+B+C	T-185	64510.09	94372.86	241.31	165.00	170.00	5.00	41	-61	38	1.25
A+B+C	T-185	64511.68	94374.69	236.94	170.00	175.00	5.00	41	-61	6	0.02
A+B+C	T-185	64513.27	94376.52	232.56	175.00	180.00	5.00	41	-61	12	0.33
A+B+C	T-185	64514.86	94378.35	228.19	180.00	185.00	5.00	41	-61	6	0.04
A+B+C	T-185	64516.45	94380.17	223.82	185.00	190.00	5.00	41	-61	8	0.10
A+B+C	T-185	64518.04	94382.01	219.45	190.00	195.00	5.00	41	-61	5	0.02
A+B+C	T-185	64519.62	94383.84	215.07	195.00	200.00	5.00	41	-61	9	0.08
A+B+C	T-185	64521.21	94385.67	210.70	200.00	205.00	5.00	41	-61	8	0.14
A+B+C	T-185	64522.81	94387.50	206.33	205.00	210.00	5.00	41	-61	6	0.06
A+B+C	T-185	64524.40	94389.32	201.95	210.00	215.00	5.00	41	-61	30	0.22

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
A+B+C	T-185	64525.99	94391.15	197.58	215.00	220.00	5.00	41	-61	14	0.06
A+B+C	T-185	64527.58	94392.99	193.21	220.00	225.00	5.00	41	-61	22	0.14
A+B+C	T-185	64529.17	94394.82	188.83	225.00	230.00	5.00	41	-61	25	0.13
A+B+C	T-185	64530.05	94395.83	186.39	230.00	230.58	0.58	41	-61	8	0.04
Below A	T-186	64518.33	94262.52	381.22	0.00	5.00	5.00	44	-60	0	0.00
Below A	T-186	64520.07	94264.32	376.89	5.00	10.00	5.00	44	-60	2	0.02
Below A	T-186	64521.80	94266.11	372.56	10.00	15.00	5.00	44	-60	17	0.19
Below A	T-186	64523.54	94267.92	368.23	15.00	20.00	5.00	44	-60	293	1.20
Below A	T-186	64525.28	94269.71	363.90	20.00	25.00	5.00	44	-60	9	0.09
Below A	T-186	64527.01	94271.51	359.57	25.00	30.00	5.00	44	-60	2	0.03
Below A	T-186	64528.75	94273.31	355.24	30.00	35.00	5.00	44	-60	6	0.03
Below A	T-186	64530.48	94275.10	350.91	35.00	40.00	5.00	44	-60	25	0.10
Below A	T-186	64532.22	94276.91	346.58	40.00	45.00	5.00	44	-60	95	0.44
Below A	T-186	64533.96	94278.71	342.25	45.00	50.00	5.00	44	-60	19	0.08
Below A	T-186	64535.70	94280.50	337.92	50.00	55.00	5.00	44	-60	21	0.05
Below A	T-186	64537.43	94282.30	333.59	55.00	60.00	5.00	44	-60	29	0.14
Below A	T-186	64539.17	94284.10	329.26	60.00	65.00	5.00	44	-60	30	0.09
Below A	T-186	64540.91	94285.90	324.93	65.00	70.00	5.00	44	-60	20	0.10
Below A	T-186	64542.64	94287.70	320.60	70.00	75.00	5.00	44	-60	5	0.05
Below A	T-186	64544.38	94289.50	316.27	75.00	80.00	5.00	44	-60	2	0.03
Below A	T-186	64546.12	94291.29	311.94	80.00	85.00	5.00	44	-60	0	0.00
Below A	T-186	64547.85	94293.09	307.61	85.00	90.00	5.00	44	-60	0	0.00
Below A	T-186	64549.59	94294.89	303.28	90.00	95.00	5.00	44	-60	2	0.02
Below A	T-186	64551.32	94296.69	298.95	95.00	100.00	5.00	44	-60	62	0.19
Below A	T-186	64553.06	94298.49	294.62	100.00	105.00	5.00	44	-60	100	0.48
Below A	T-186	64554.80	94300.28	290.29	105.00	110.00	5.00	44	-60	88	0.45
Below A	T-186	64556.54	94302.08	285.96	110.00	115.00	5.00	44	-60	68	0.29
Below A	T-186	64558.27	94303.88	281.63	115.00	120.00	5.00	44	-60	64	0.29
Below A	T-186	64560.01	94305.68	277.30	120.00	124.00	4.00	44	-60	34	0.21
Vertical	T-188	64392.55	94428.92	387.22	0.00	5.00	5.00	50	-45	0	0.00
Vertical	T-188	64395.26	94431.19	383.69	5.00	10.00	5.00	50	-45	0	0.00
Vertical	T-188	64397.97	94433.46	380.15	10.00	15.00	5.00	50	-45	0	0.00
Vertical	T-188	64400.68	94435.74	376.62	15.00	20.00	5.00	50	-45	10	0.11
Vertical	T-188	64403.39	94438.01	373.08	20.00	25.00	5.00	50	-45	0	0.00
Vertical	T-188	64406.09	94440.28	369.54	25.00	30.00	5.00	50	-45	0	0.00
Vertical	T-188	64408.80	94442.56	366.01	30.00	35.00	5.00	50	-45	44	0.74
Vertical	T-188	64411.51	94444.83	362.47	35.00	40.00	5.00	50	-45	8	0.07
Vertical	T-188	64414.22	94447.10	358.94	40.00	45.00	5.00	50	-45	6	0.03
Vertical	T-188	64416.93	94449.37	355.40	45.00	50.00	5.00	50	-45	45	0.31
Vertical	T-188	64419.64	94451.64	351.87	50.00	52.20	2.20	50	-45	10	0.15
Vertical	T-189	64644.44	94410.00	379.30	0.00	5.00	5.00	217	-57	0	0.00
Vertical	T-189	64642.80	94407.82	375.11	5.00	10.00	5.00	217	-57	0	0.00
Vertical	T-189	64641.16	94405.64	370.92	10.00	15.00	5.00	217	-57	0	0.00
Vertical	T-189	64639.53	94403.47	366.72	15.00	20.00	5.00	217	-57	0	0.00
Vertical	T-189	64637.89	94401.29	362.53	20.00	25.00	5.00	217	-57	6	0.02
Vertical	T-189	64636.25	94399.12	358.34	25.00	30.00	5.00	217	-57	22	0.11
Vertical	T-189	64634.61	94396.95	354.14	30.00	35.00	5.00	217	-57	10	0.07
Vertical	T-189	64632.97	94394.77	349.95	35.00	40.00	5.00	217	-57	18	0.16
Vertical	T-189	64631.33	94392.60	345.76	40.00	45.00	5.00	217	-57	7	0.15
Vertical	T-189	64629.69	94390.42	341.56	45.00	50.00	5.00	217	-57	42	0.30
Vertical	T-189	64628.05	94388.25	337.37	50.00	55.00	5.00	217	-57	58	0.47
Vertical	T-189	64626.41	94386.07	333.18	55.00	60.00	5.00	217	-57	28	0.22
Vertical	T-189	64624.78	94383.89	328.98	60.00	65.00	5.00	217	-57	3	0.04
Vertical	T-189	64623.14	94381.72	324.79	65.00	70.00	5.00	217	-57	17	0.18

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-189	64621.50	94379.55	320.60	70.00	75.00	5.00	217	-57	37	0.69
Vertical	T-189	64619.86	94377.37	316.40	75.00	80.00	5.00	217	-57	6	0.11
Vertical	T-189	64618.22	94375.20	312.21	80.00	85.00	5.00	217	-57	6	0.09
Vertical	T-189	64616.58	94373.02	308.02	85.00	90.00	5.00	217	-57	12	0.21
Vertical	T-189	64614.94	94370.85	303.82	90.00	95.00	5.00	217	-57	4	0.08
Vertical	T-189	64613.30	94368.67	299.63	95.00	100.00	5.00	217	-57	18	0.18
Vertical	T-189	64611.66	94366.50	295.44	100.00	105.00	5.00	217	-57	3	0.06
Vertical	T-189	64610.03	94364.32	291.24	105.00	110.00	5.00	217	-57	16	0.12
Vertical	T-189	64608.39	94362.14	287.05	110.00	115.00	5.00	217	-57	6	0.10
Vertical	T-189	64606.75	94359.97	282.86	115.00	120.00	5.00	217	-57	7	0.14
Vertical	T-189	64605.11	94357.80	278.66	120.00	125.00	5.00	217	-57	6	0.09
Vertical	T-189	64603.47	94355.62	274.47	125.00	130.00	5.00	217	-57	27	0.25
Vertical	T-189	64601.83	94353.45	270.28	130.00	135.00	5.00	217	-57	15	0.19
Vertical	T-189	64600.19	94351.28	266.08	135.00	140.00	5.00	217	-57	3	0.05
Vertical	T-189	64598.55	94349.10	261.89	140.00	145.00	5.00	217	-57	4	0.11
Vertical	T-189	64596.91	94346.92	257.70	145.00	150.00	5.00	217	-57	7	0.08
Vertical	T-189	64595.28	94344.75	253.50	150.00	155.00	5.00	217	-57	4	0.03
Vertical	T-189	64593.64	94342.57	249.31	155.00	160.00	5.00	217	-57	6	0.08
A+B+C	T-189	64592.00	94340.40	245.12	160.00	163.15	3.15	217	-57	108	1.26
Below A	T-189	64592.00	94340.40	245.12	163.15	165.00	1.85	217	-57	2	0.02
Below A	T-189	64590.36	94338.22	240.92	165.00	170.00	5.00	217	-57	3	0.03
Below A	T-189	64588.72	94336.05	236.73	170.00	172.63	2.63	217	-57	2	0.01
Vertical	T-258	64591.74	94340.23	383.74	0.00	5.00	5.00	220	-46	0	0.00
Vertical	T-258	64589.51	94337.53	380.17	5.00	10.00	5.00	220	-46	6	0.05
Vertical	T-258	64587.28	94334.82	376.60	10.00	15.00	5.00	220	-46	113	0.65
Vertical	T-258	64585.05	94332.12	373.04	15.00	20.00	5.00	220	-46	21	0.14
Vertical	T-258	64582.82	94329.41	369.47	20.00	24.00	4.00	220	-46	43	0.32
A+B+C	T-258	64582.82	94329.41	369.47	24.00	25.00	1.00	220	-46	17	0.36
A+B+C	T-258	64580.59	94326.71	365.91	25.00	30.00	5.00	220	-46	63	0.38
A+B+C	T-258	64578.36	94324.00	362.34	30.00	35.00	5.00	220	-46	20	0.24
A+B+C	T-258	64576.13	94321.30	358.77	35.00	40.00	5.00	220	-46	52	0.58
A+B+C	T-258	64573.90	94318.60	355.21	40.00	45.00	5.00	220	-46	70	0.45
A+B+C	T-258	64571.68	94315.89	351.64	45.00	50.00	5.00	220	-46	64	0.52
Below A	T-258	64569.45	94313.19	348.07	51.45	55.00	3.55	220	-46	35	0.37
A+B+C	T-258	64569.45	94313.19	348.07	53.55	55.00	1.45	220	-46	176	1.27
Below A	T-258	64567.21	94310.48	344.51	55.00	60.00	5.00	220	-46	24	0.26
Below A	T-258	64564.99	94307.78	340.94	60.00	64.85	4.85	220	-46	94	0.89
A+B+C	T-259	64638.06	94277.41	381.09	0.00	5.00	5.00	219	-45	0	0.00
A+B+C	T-259	64635.84	94274.66	377.56	5.00	10.00	5.00	219	-45	0	0.00
A+B+C	T-259	64633.61	94271.92	374.02	10.00	15.00	5.00	219	-45	52	0.27
A+B+C	T-259	64631.38	94269.17	370.49	15.00	20.00	5.00	219	-45	205	1.15
A+B+C	T-259	64629.16	94266.42	366.95	20.00	25.00	5.00	219	-45	478	5.76
A+B+C	T-259	64626.93	94263.67	363.41	25.00	30.00	5.00	219	-45	427	3.71
A+B+C	T-259	64624.71	94260.92	359.88	30.00	35.00	5.00	219	-45	38	0.10
A+B+C	T-259	64622.48	94258.17	356.34	35.00	40.00	5.00	219	-45	100	0.63
A+B+C	T-259	64620.26	94255.43	352.81	40.00	45.00	5.00	219	-45	114	0.81
A+B+C	T-259	64618.04	94252.68	349.27	45.00	50.00	5.00	219	-45	139	0.65
A+B+C	T-259	64615.81	94249.93	345.74	50.00	55.00	5.00	219	-45	49	0.19
A+B+C	T-259	64613.59	94247.18	342.20	55.00	60.00	5.00	219	-45	36	0.15
A+B+C	T-259	64611.36	94244.44	338.67	60.00	65.00	5.00	219	-45	208	0.91
A+B+C	T-259	64609.13	94241.69	335.13	65.00	65.60	0.60	219	-45	235	1.49
Below A	T-259	64609.13	94241.69	335.13	65.60	70.00	4.40	219	-45	191	1.00
Below A	T-259	64606.91	94238.95	331.60	75.00	78.00	3.00	219	-45	79	0.44
Vertical	T-260	64671.84	94278.19	379.61	0.00	5.00	5.00	216	-44	0	0.00

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-260	64669.73	94275.28	376.14	5.00	10.00	5.00	216	-44	0	0.00
Vertical	T-260	64667.61	94272.37	372.67	10.00	15.00	5.00	216	-44	21	0.21
Vertical	T-260	64665.50	94269.46	369.19	15.00	20.00	5.00	216	-44	138	0.86
Vertical	T-260	64663.39	94266.55	365.72	20.00	25.00	5.00	216	-44	121	0.74
Vertical	T-260	64661.27	94263.64	362.25	25.00	30.00	5.00	216	-44	120	1.31
Vertical	T-260	64659.16	94260.73	358.77	30.00	35.00	5.00	216	-44	120	0.46
Vertical	T-260	64657.04	94257.82	355.30	35.00	35.35	0.35	216	-44	19	0.05
A+B+C	T-260	64657.04	94257.82	355.30	35.35	40.00	4.65	216	-44	177	0.88
A+B+C	T-260	64654.93	94254.91	351.83	40.00	45.00	5.00	216	-44	26	0.07
A+B+C	T-260	64652.82	94252.00	348.35	45.00	50.00	5.00	216	-44	366	3.38
A+B+C	T-260	64650.70	94249.09	344.88	50.00	55.00	5.00	216	-44	383	2.19
A+B+C	T-260	64648.59	94246.18	341.41	55.00	60.00	5.00	216	-44	377	2.35
A+B+C	T-260	64646.47	94243.27	337.93	60.00	65.00	5.00	216	-44	73	0.60
A+B+C	T-260	64644.36	94240.36	334.46	65.00	70.00	5.00	216	-44	34	0.44
A+B+C	T-260	64642.25	94237.45	330.99	70.00	75.00	5.00	216	-44	126	0.71
A+B+C	T-260	64640.13	94234.54	327.51	75.00	77.10	2.10	216	-44	395	2.91
Below A	T-260	64640.13	94234.54	327.51	77.10	80.00	2.90	216	-44	22	0.16
Below A	T-260	64638.85	94232.78	325.41	80.00	81.07	1.07	216	-44	14	0.07
Vertical	T-261	64703.82	94240.04	377.55	0.00	5.00	5.00	219	-46	10	0.29
Vertical	T-261	64701.61	94237.32	373.98	5.00	10.00	5.00	219	-46	4	0.16
Vertical	T-261	64699.41	94234.59	370.41	10.00	15.00	5.00	219	-46	12	0.30
Vertical	T-261	64697.20	94231.87	366.85	15.00	20.00	5.00	219	-46	35	0.17
Vertical	T-261	64695.00	94229.14	363.28	20.00	22.00	2.00	219	-46	63	0.23
A+B+C	T-261	64695.00	94229.14	363.28	22.00	25.00	3.00	219	-46	167	1.20
A+B+C	T-261	64692.79	94226.42	359.72	25.00	30.00	5.00	219	-46	168	1.99
A+B+C	T-261	64690.59	94223.70	356.15	30.00	35.00	5.00	219	-46	48	0.23
A+B+C	T-261	64688.38	94220.97	352.58	35.00	40.00	5.00	219	-46	20	0.04
A+B+C	T-261	64686.18	94218.25	349.02	40.00	45.00	5.00	219	-46	27	0.28
A+B+C	T-261	64683.97	94215.53	345.45	45.00	50.00	5.00	219	-46	156	1.30
A+B+C	T-261	64681.77	94212.81	341.88	50.00	51.60	1.60	219	-46	640	6.65
Below A	T-261	64681.77	94212.81	341.88	51.60	55.00	3.40	219	-46	38	0.07
Below A	T-261	64679.56	94210.08	338.32	55.00	59.74	4.74	219	-46	5	0.01
Vertical	T-346-MOC	64625.51	94302.35	382.18	0.00	5.00	5.00	226	-47	7	0.02
Vertical	T-346-MOC	64623.07	94299.98	378.52	5.00	10.00	5.00	226	-47	200	0.95
Vertical	T-346-MOC	64620.63	94297.60	374.87	10.00	15.00	5.00	226	-47	76	0.22
Vertical	T-346-MOC	64618.21	94295.20	371.21	15.00	20.00	5.00	225	-47	97	0.45
Vertical	T-346-MOC	64615.79	94292.79	367.55	20.00	21.90	1.90	225	-47	89	0.60
A+B+C	T-346-MOC	64615.79	94292.79	367.55	21.90	25.00	3.10	225	-47	328	2.65
A+B+C	T-346-MOC	64613.39	94290.37	363.90	25.00	30.00	5.00	225	-47	276	2.01
A+B+C	T-346-MOC	64610.99	94287.94	360.24	30.00	35.00	5.00	225	-47	633	3.92
A+B+C	T-346-MOC	64608.59	94285.52	356.58	35.00	40.00	5.00	225	-47	421	2.13
A+B+C	T-346-MOC	64606.22	94283.07	352.93	40.00	45.00	5.00	224	-47	965	4.32
A+B+C	T-346-MOC	64603.85	94280.62	349.27	45.00	50.00	5.00	224	-47	967	6.05
A+B+C	T-346-MOC	64601.48	94278.17	345.61	50.00	53.94	3.94	224	-47	3065	33.34
Below A	T-346-MOC	64601.48	94278.17	345.61	53.94	55.00	1.06	224	-47	246	0.70
Below A	T-346-MOC	64599.10	94275.73	341.96	55.00	60.00	5.00	224	-47	156	0.50
Below A	T-346-MOC	64596.71	94273.28	338.30	60.00	65.00	5.00	225	-47	35	0.14
Below A	T-346-MOC	64594.32	94270.85	334.64	65.00	70.00	5.00	225	-47	64	0.21
Below A	T-346-MOC	64591.92	94268.43	330.99	70.00	75.00	5.00	225	-47	96	0.31
Below A	T-346-MOC	64589.51	94266.02	327.33	75.00	80.00	5.00	225	-47	479	2.74
Below A	T-346-MOC	64587.10	94263.60	323.67	80.00	85.00	5.00	225	-47	168	0.95
Below A	T-346-MOC	64584.67	94261.21	320.02	85.00	90.00	5.00	225	-47	19	0.11
Below A	T-346-MOC	64582.24	94258.81	316.36	90.00	95.00	5.00	226	-47	9	0.05
Below A	T-346-MOC	64579.80	94256.42	312.70	95.00	100.00	5.00	226	-47	24	0.12

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-346-MOC	64577.37	94254.04	309.05	100.00	105.00	5.00	226	-47	28	0.13
Below A	T-346-MOC	64574.91	94251.67	305.39	105.00	110.00	5.00	226	-47	27	0.19
Below A	T-346-MOC	64572.46	94249.30	301.73	110.00	115.00	5.00	226	-47	7	0.02
Below A	T-346-MOC	64570.01	94246.93	298.08	115.00	120.00	5.00	226	-47	8	0.04
Below A	T-346-MOC	64567.55	94244.57	294.42	120.00	125.00	5.00	226	-47	38	0.43
Below A	T-346-MOC	64565.81	94242.88	291.82	125.00	127.10	2.10	226	-47	6	0.02
Vertical	T-347-MOC	64725.05	94292.14	378.47	0.00	5.00	5.00	227	-55	4	0.04
Vertical	T-347-MOC	64722.96	94290.19	374.37	5.00	10.00	5.00	227	-55	28	0.44
Vertical	T-347-MOC	64720.87	94288.23	370.27	10.00	15.00	5.00	227	-55	8	0.16
Vertical	T-347-MOC	64718.80	94286.27	366.17	15.00	20.00	5.00	227	-55	41	0.25
Vertical	T-347-MOC	64716.73	94284.31	362.06	20.00	25.00	5.00	227	-55	60	0.45
Vertical	T-347-MOC	64714.66	94282.35	357.96	25.00	30.00	5.00	227	-55	27	0.18
Vertical	T-347-MOC	64712.59	94280.39	353.84	30.00	35.00	5.00	227	-55	37	0.22
Vertical	T-347-MOC	64710.54	94278.42	349.73	35.00	40.00	5.00	226	-55	18	0.11
Vertical	T-347-MOC	64708.48	94276.46	345.62	40.00	45.00	5.00	226	-55	25	0.09
Vertical	T-347-MOC	64706.43	94274.50	341.50	45.00	50.00	5.00	226	-55	10	0.09
Vertical	T-347-MOC	64704.39	94272.54	337.38	50.00	55.00	5.00	226	-56	25	0.08
Vertical	T-347-MOC	64702.36	94270.57	333.26	55.00	60.00	5.00	226	-56	26	0.11
Vertical	T-347-MOC	64700.31	94268.62	329.14	60.00	65.00	5.00	226	-56	13	0.08
Vertical	T-347-MOC	64698.27	94266.67	325.01	65.00	70.00	5.00	226	-56	43	0.61
Vertical	T-347-MOC	64696.21	94264.74	320.88	70.00	75.00	5.00	227	-56	6	0.06
Vertical	T-347-MOC	64694.16	94262.80	316.75	75.00	80.00	5.00	227	-56	7	0.05
Vertical	T-347-MOC	64692.11	94260.89	312.62	80.00	85.00	5.00	227	-56	33	0.37
Vertical	T-347-MOC	64690.05	94258.97	308.48	85.00	90.00	5.00	227	-56	21	0.53
Vertical	T-347-MOC	64687.99	94257.06	304.35	90.00	95.00	5.00	228	-56	4	0.05
Vertical	T-347-MOC	64685.92	94255.17	300.20	95.00	100.00	5.00	228	-56	11	0.11
Vertical	T-347-MOC	64683.86	94253.28	296.06	100.00	100.55	0.55	228	-56	15	0.12
A+B+C	T-347-MOC	64683.86	94253.28	296.06	100.55	105.00	4.45	228	-56	123	0.70
Below A	T-347-MOC	64681.78	94251.40	291.92	105.35	110.00	4.65	228	-56	19	0.11
A+B+C	T-347-MOC	64681.78	94251.40	291.92	109.65	110.00	0.35	228	-56	181	1.54
Below A	T-347-MOC	64679.70	94249.53	287.77	110.00	115.00	5.00	228	-56	16	0.03
Below A	T-347-MOC	64677.62	94247.66	283.63	115.00	118.64	3.64	228	-56	9	0.02
Below A	T-348-OC	64602.27	94206.52	377.45	0.00	5.00	5.00	45	-50	0	0.00
Below A	T-348-OC	64604.53	94208.80	373.62	5.00	10.00	5.00	45	-50	0	0.00
Below A	T-348-OC	64606.79	94211.07	369.79	10.00	15.00	5.00	45	-50	3	0.08
Below A	T-348-OC	64609.04	94213.35	365.95	15.00	20.00	5.00	45	-50	13	0.11
Below A	T-348-OC	64611.29	94215.64	362.11	20.00	25.00	5.00	45	-50	12	0.10
Below A	T-348-OC	64613.53	94217.92	358.26	25.00	30.00	5.00	44	-50	1	0.00
Below A	T-348-OC	64615.76	94220.21	354.42	30.00	35.00	5.00	44	-50	0	0.00
Below A	T-348-OC	64617.98	94222.50	350.57	35.00	40.00	5.00	44	-50	0	0.00
Below A	T-348-OC	64620.20	94224.80	346.72	40.00	45.00	5.00	44	-50	0	0.00
Below A	T-348-OC	64622.41	94227.10	342.87	45.00	50.00	5.00	44	-50	65	0.71
Below A	T-348-OC	64624.62	94229.40	339.02	50.00	55.00	5.00	44	-50	55	1.94
Below A	T-348-OC	64626.81	94231.70	335.16	55.00	60.00	5.00	44	-51	72	0.96
Below A	T-348-OC	64629.00	94234.00	331.31	60.00	65.00	5.00	44	-51	41	0.19
Below A	T-348-OC	64631.19	94236.30	327.44	65.00	70.00	5.00	44	-51	12	0.09
Below A	T-348-OC	64633.39	94238.58	323.57	70.00	75.00	5.00	44	-51	2	0.01
Below A	T-348-OC	64635.58	94240.85	319.69	75.00	80.00	5.00	44	-51	0	0.00
Below A	T-348-OC	64637.77	94243.12	315.81	80.00	85.00	5.00	44	-51	0	0.00
Below A	T-348-OC	64639.96	94245.39	311.93	85.00	90.00	5.00	44	-51	9	0.02
Below A	T-348-OC	64642.15	94247.63	308.04	90.00	95.00	5.00	44	-51	14	0.04
Below A	T-348-OC	64644.34	94249.87	304.14	95.00	100.00	5.00	45	-51	81	0.42
Below A	T-348-OC	64646.54	94252.10	300.24	100.00	105.00	5.00	45	-51	27	0.67
Below A	T-348-OC	64648.73	94254.31	296.33	105.00	105.65	0.65	45	-52	52	0.51

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-349-MOC	64504.47	94321.91	384.66	0.00	5.00	5.00	1	-60	3	0.06
Below A	T-349-MOC	64504.50	94324.42	380.34	5.00	10.00	5.00	1	-60	2	0.03
Below A	T-349-MOC	64504.53	94326.93	376.02	10.00	15.00	5.00	1	-60	9	0.12
Below A	T-349-MOC	64504.56	94329.45	371.70	15.00	20.00	5.00	1	-60	6	0.13
Below A	T-349-MOC	64504.61	94331.97	367.38	20.00	25.00	5.00	1	-60	4	0.11
Below A	T-349-MOC	64504.66	94334.50	363.07	25.00	30.00	5.00	1	-60	6	0.11
Below A	T-349-MOC	64504.71	94337.04	358.76	30.00	35.00	5.00	1	-60	38	0.53
Below A	T-349-MOC	64504.77	94339.58	354.45	35.00	38.50	3.50	1	-59	9	0.07
A+B+C	T-349-MOC	64504.77	94339.58	354.45	38.50	40.00	1.50	1	-59	11	0.18
A+B+C	T-349-MOC	64504.83	94342.12	350.15	40.00	45.00	5.00	1	-59	8	0.18
A+B+C	T-349-MOC	64504.90	94344.67	345.85	45.00	50.00	5.00	2	-59	20	0.20
A+B+C	T-349-MOC	64504.97	94347.23	341.56	50.00	55.00	5.00	2	-59	16	0.22
A+B+C	T-349-MOC	64505.05	94349.79	337.26	55.00	60.00	5.00	2	-59	23	0.21
A+B+C	T-349-MOC	64505.14	94352.37	332.98	60.00	63.05	3.05	2	-59	14	0.07
Vertical	T-349-MOC	64505.14	94352.37	332.98	63.05	65.00	1.95	2	-59	14	0.23
Vertical	T-349-MOC	64505.23	94354.94	328.69	65.00	70.00	5.00	2	-59	71	0.74
Vertical	T-349-MOC	64505.32	94357.51	324.41	70.00	75.00	5.00	2	-59	45	0.40
Vertical	T-349-MOC	64505.42	94360.10	320.13	75.00	80.00	5.00	2	-59	29	0.28
Vertical	T-349-MOC	64505.52	94362.67	315.84	80.00	85.00	5.00	2	-59	14	0.19
Vertical	T-349-MOC	64505.62	94365.26	311.56	85.00	90.00	5.00	2	-59	10	0.10
Vertical	T-349-MOC	64505.73	94367.84	307.28	90.00	95.00	5.00	2	-59	15	0.15
Vertical	T-349-MOC	64505.83	94370.42	303.01	95.00	100.00	5.00	2	-59	39	0.46
Vertical	T-349-MOC	64505.95	94373.03	298.73	100.00	105.00	5.00	3	-59	62	0.43
Vertical	T-349-MOC	64506.07	94375.62	294.46	105.00	110.00	5.00	3	-59	5	0.11
Vertical	T-349-MOC	64506.19	94378.21	290.19	110.00	115.00	5.00	3	-59	18	0.38
Vertical	T-349-MOC	64506.31	94380.82	285.92	115.00	120.00	5.00	3	-59	25	0.35
Vertical	T-349-MOC	64506.44	94383.42	281.66	120.00	125.00	5.00	3	-59	18	0.18
Vertical	T-349-MOC	64506.57	94386.03	277.39	125.00	130.00	5.00	3	-59	21	0.43
Vertical	T-349-MOC	64506.70	94388.63	273.12	130.00	135.00	5.00	3	-59	120	3.59
Vertical	T-349-MOC	64506.84	94391.24	268.86	135.00	140.00	5.00	3	-59	95	1.96
Vertical	T-349-MOC	64506.98	94393.85	264.60	140.00	145.00	5.00	3	-59	219	2.98
Vertical	T-349-MOC	64507.11	94396.46	260.33	145.00	146.70	1.70	3	-59	34	0.28
Vertical	T-368	64534.63	94401.60	383.24	0.00	5.00	5.00	11	-52	3	0.08
Vertical	T-368	64535.23	94404.64	379.30	5.00	10.00	5.00	11	-52	35	0.35
Vertical	T-368	64535.83	94407.65	375.36	10.00	15.00	5.00	11	-52	86	0.51
Vertical	T-368	64536.45	94410.67	371.42	15.00	20.00	5.00	12	-52	10	0.09
Vertical	T-368	64537.06	94413.68	367.48	20.00	25.00	5.00	12	-52	56	0.44
Vertical	T-368	64537.68	94416.70	363.54	25.00	30.00	5.00	12	-52	2	0.03
Vertical	T-368	64538.32	94419.71	359.60	30.00	35.00	5.00	12	-52	7	0.11
Vertical	T-368	64538.96	94422.73	355.66	35.00	40.00	5.00	12	-52	7	0.09
Vertical	T-368	64539.62	94425.74	351.72	40.00	45.00	5.00	13	-52	6	0.04
Vertical	T-368	64540.29	94428.74	347.78	45.00	50.00	5.00	13	-52	16	0.11
Vertical	T-368	64540.97	94431.74	343.84	50.00	55.00	5.00	13	-52	10	0.12
Vertical	T-368	64541.67	94434.73	339.90	55.00	60.00	5.00	13	-52	6	0.07
Vertical	T-368	64542.37	94437.73	335.96	60.00	65.00	5.00	13	-52	2	0.02
Vertical	T-368	64543.11	94440.71	332.02	65.00	70.00	5.00	14	-52	2	0.06
Vertical	T-368	64543.85	94443.71	328.08	70.00	75.00	5.00	14	-52	3	0.06
Vertical	T-368	64544.59	94446.64	324.20	75.00	79.85	4.85	14	-52	9	0.09
Below A	T-369	64421.46	94343.23	389.50	0.00	5.00	5.00	11	-56	1	0.03
Below A	T-369	64422.00	94345.97	385.35	5.00	10.00	5.00	11	-56	15	0.47
Below A	T-369	64422.54	94348.72	381.21	10.00	15.00	5.00	11	-56	6	0.17
Below A	T-369	64423.08	94351.48	377.08	15.00	17.40	2.40	11	-56	6	0.28
A+B+C	T-369	64423.08	94351.48	377.08	17.40	20.00	2.60	11	-56	80	0.24
A+B+C	T-369	64423.62	94354.24	372.94	20.00	25.00	5.00	11	-56	15	0.26

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
A+B+C	T-369	64424.17	94357.00	368.81	25.00	30.00	5.00	11	-56	42	0.50
A+B+C	T-369	64424.72	94359.76	364.68	30.00	35.00	5.00	11	-56	14	0.12
A+B+C	T-369	64425.27	94362.52	360.55	35.00	40.00	5.00	12	-56	12	0.07
A+B+C	T-369	64425.84	94365.29	356.43	40.00	41.90	1.90	12	-56	46	0.38
Vertical	T-369	64425.84	94365.29	356.43	41.90	45.00	3.10	12	-56	30	0.12
Vertical	T-369	64426.40	94368.07	352.31	45.00	50.00	5.00	12	-56	20	0.34
Vertical	T-369	64426.98	94370.85	348.19	50.00	55.00	5.00	12	-56	15	0.25
Vertical	T-369	64427.55	94373.62	344.07	55.00	60.00	5.00	12	-56	61	0.58
Vertical	T-369	64428.13	94376.39	339.95	60.00	65.00	5.00	12	-56	26	0.25
Vertical	T-369	64428.71	94379.16	335.82	65.00	70.00	5.00	12	-56	6	0.05
Vertical	T-369	64429.31	94381.92	331.70	70.00	75.00	5.00	12	-56	5	0.11
Vertical	T-369	64429.91	94384.69	327.58	75.00	80.00	5.00	12	-56	12	0.14
Vertical	T-369	64430.51	94387.46	323.46	80.00	85.00	5.00	12	-56	8	0.09
Vertical	T-369	64431.12	94390.22	319.34	85.00	90.00	5.00	13	-56	59	0.61
Vertical	T-369	64431.73	94392.99	315.22	90.00	95.00	5.00	13	-56	31	0.40
Vertical	T-369	64432.34	94395.76	311.10	95.00	100.00	5.00	13	-56	10	0.12
Vertical	T-369	64432.95	94398.53	306.98	100.00	105.00	5.00	13	-56	40	0.43
Vertical	T-369	64433.57	94401.28	302.86	105.00	110.00	5.00	13	-56	99	1.23
Vertical	T-369	64434.20	94404.05	298.74	110.00	115.00	5.00	13	-56	432	5.92
Vertical	T-369	64434.84	94406.81	294.62	115.00	120.00	5.00	13	-56	37	0.44
Vertical	T-369	64435.48	94409.57	290.50	120.00	125.00	5.00	13	-56	7	0.12
Vertical	T-369	64436.14	94412.32	286.38	125.00	130.00	5.00	14	-56	7	0.08
Vertical	T-369	64436.80	94415.07	282.26	130.00	135.00	5.00	14	-56	26	0.28
Vertical	T-369	64437.46	94417.82	278.14	135.00	140.00	5.00	14	-56	11	0.14
Vertical	T-369	64438.13	94420.58	274.02	140.00	145.00	5.00	14	-56	18	0.17
Vertical	T-369	64438.79	94423.33	269.89	145.00	150.00	5.00	14	-56	8	0.09
Vertical	T-369	64439.45	94426.09	265.77	150.00	155.00	5.00	14	-56	2	0.02
Vertical	T-369	64440.11	94428.84	261.65	155.00	160.00	5.00	14	-56	5	0.06
Vertical	T-369	64440.77	94431.60	257.53	160.00	165.00	5.00	14	-56	5	0.08
Vertical	T-369	64441.43	94434.35	253.41	165.00	166.90	1.90	14	-56	4	0.08
Vertical	T-370	64709.46	94379.37	377.89	0.00	5.00	5.00	227	-50	3	0.02
Vertical	T-370	64707.12	94377.17	374.06	5.00	10.00	5.00	227	-50	8	0.03
Vertical	T-370	64704.78	94374.99	370.22	10.00	15.00	5.00	227	-50	6	0.05
Vertical	T-370	64702.45	94372.81	366.37	15.00	20.00	5.00	227	-50	5	0.11
Vertical	T-370	64700.13	94370.62	362.52	20.00	25.00	5.00	227	-50	6	0.08
Vertical	T-370	64697.81	94368.44	358.66	25.00	30.00	5.00	227	-51	53	0.54
Vertical	T-370	64695.50	94366.26	354.80	30.00	35.00	5.00	227	-51	33	0.10
Vertical	T-370	64693.20	94364.09	350.93	35.00	40.00	5.00	227	-51	42	0.16
Vertical	T-370	64690.90	94361.92	347.05	40.00	45.00	5.00	227	-51	17	0.10
Vertical	T-370	64688.61	94359.75	343.17	45.00	50.00	5.00	227	-51	10	0.12
Vertical	T-370	64686.33	94357.58	339.29	50.00	55.00	5.00	227	-51	14	0.08
Vertical	T-370	64684.04	94355.42	335.41	55.00	60.00	5.00	227	-51	14	0.05
Vertical	T-370	64681.75	94353.25	331.53	60.00	65.00	5.00	227	-51	10	0.07
Vertical	T-370	64679.46	94351.07	327.65	65.00	70.00	5.00	227	-51	18	0.10
Vertical	T-370	64677.17	94348.89	323.77	70.00	75.00	5.00	227	-51	16	0.08
Vertical	T-370	64674.87	94346.71	319.90	75.00	80.00	5.00	227	-51	23	0.09
Vertical	T-370	64672.58	94344.53	316.03	80.00	85.00	5.00	227	-51	21	0.14
Vertical	T-370	64670.28	94342.35	312.17	85.00	90.00	5.00	227	-51	19	0.17
Vertical	T-370	64667.97	94340.17	308.30	90.00	95.00	5.00	227	-51	25	0.13
Vertical	T-370	64665.67	94337.98	304.44	95.00	100.00	5.00	227	-51	32	0.16
Vertical	T-370	64663.36	94335.78	300.58	100.00	105.00	5.00	227	-51	5	0.06
Vertical	T-370	64661.05	94333.60	296.73	105.00	110.00	5.00	227	-50	8	0.11
Vertical	T-370	64658.71	94331.43	292.88	110.00	115.00	5.00	227	-50	18	0.24
Vertical	T-370	64656.37	94329.27	289.03	115.00	120.00	5.00	228	-50	8	0.12

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-370	64654.02	94327.10	285.18	120.00	125.00	5.00	228	-50	18	0.22
Vertical	T-370	64651.65	94324.96	281.33	125.00	130.00	5.00	228	-50	3	0.05
Vertical	T-370	64649.27	94322.82	277.49	130.00	135.00	5.00	228	-50	3	0.05
Vertical	T-370	64646.87	94320.68	273.65	135.00	140.00	5.00	229	-50	4	0.05
Vertical	T-370	64644.47	94318.56	269.82	140.00	145.00	5.00	229	-50	5	0.06
Vertical	T-370	64642.06	94316.44	265.99	145.00	150.00	5.00	229	-50	13	0.11
Vertical	T-370	64639.64	94314.33	262.16	150.00	155.00	5.00	229	-50	12	0.09
Vertical	T-370	64637.21	94312.24	258.33	155.00	160.00	5.00	229	-50	18	0.17
Vertical	T-370	64634.77	94310.14	254.50	160.00	160.15	0.15	229	-50	14	0.12
A+B+C	T-370	64634.77	94310.14	254.50	160.15	165.00	4.85	229	-50	221	1.72
A+B+C	T-370	64632.34	94308.03	250.67	165.00	170.00	5.00	229	-50	97	0.65
A+B+C	T-370	64629.90	94305.95	246.83	170.00	171.29	1.29	230	-50	86	1.73
Below A	T-370	64629.90	94305.95	246.83	171.29	175.00	3.71	229	-50	31	0.09
Below A	T-370	64627.45	94303.87	243.00	175.00	180.00	5.00	230	-50	41	0.22
Below A	T-370	64625.00	94301.78	239.17	180.00	185.00	5.00	230	-50	8	0.03
Below A	T-370	64622.55	94299.71	235.34	185.00	190.00	5.00	230	-50	19	0.08
Below A	T-370	64620.10	94297.64	231.51	190.00	195.00	5.00	230	-50	8	0.07
Below A	T-370	64617.64	94295.57	227.68	195.00	200.00	5.00	230	-50	5	0.06
Below A	T-370	64615.18	94293.50	223.85	200.00	205.00	5.00	230	-50	12	0.08
Below A	T-370	64612.72	94291.43	220.02	205.00	210.00	5.00	230	-50	8	0.04
Below A	T-370	64610.25	94289.37	216.19	210.00	215.00	5.00	230	-50	5	0.04
Below A	T-370	64607.79	94287.30	212.36	215.00	220.00	5.00	230	-50	23	0.18
Below A	T-370	64605.80	94285.63	209.26	220.00	223.11	3.11	230	-50	10	0.10
Vertical	T-371	64568.74	94350.99	384.38	0.00	5.00	5.00	227	-45	9	0.13
Vertical	T-371	64566.16	94348.57	380.85	5.00	10.00	5.00	227	-45	30	0.70
Vertical	T-371	64563.58	94346.13	377.32	10.00	15.00	5.00	227	-45	86	0.54
Vertical	T-371	64561.02	94343.69	373.79	15.00	20.00	5.00	226	-45	163	0.97
Vertical	T-371	64558.46	94341.24	370.27	20.00	25.00	5.00	226	-45	236	1.51
Vertical	T-371	64555.90	94338.77	366.75	25.00	30.00	5.00	226	-45	18	0.19
Vertical	T-371	64553.35	94336.29	363.23	30.00	30.32	0.32	225	-45	8	0.06
A+B+C	T-371	64553.35	94336.29	363.23	30.32	35.00	4.68	226	-45	59	0.31
A+B+C	T-371	64550.81	94333.80	359.72	35.00	40.00	5.00	225	-45	34	0.26
A+B+C	T-371	64548.28	94331.30	356.21	40.00	44.65	4.65	225	-45	32	0.22
Below A	T-371	64548.28	94331.30	356.21	44.65	45.00	0.35	225	-45	7	0.04
Below A	T-371	64545.75	94328.78	352.70	45.00	50.00	5.00	225	-45	9	0.05
Below A	T-371	64543.23	94326.26	349.20	50.00	55.00	5.00	225	-45	2	0.06
Below A	T-371	64540.70	94323.75	345.69	55.00	60.00	5.00	226	-45	3	0.08
Below A	T-371	64538.15	94321.27	342.18	60.00	65.00	5.00	226	-45	5	0.05
Below A	T-371	64535.60	94318.78	338.67	65.00	70.00	5.00	226	-45	2	0.03
Below A	T-371	64533.03	94316.32	335.15	70.00	75.00	5.00	226	-45	1	0.02
Below A	T-371	64530.46	94313.90	331.63	75.00	80.00	5.00	227	-45	2	0.02
Below A	T-371	64527.87	94311.47	328.10	80.00	85.00	5.00	227	-45	2	0.03
Below A	T-371	64525.27	94309.06	324.58	85.00	90.00	5.00	227	-45	10	0.10
Below A	T-371	64522.66	94306.66	321.05	90.00	95.00	5.00	227	-45	11	0.11
Below A	T-371	64520.05	94304.28	317.52	95.00	100.00	5.00	228	-45	4	0.03
Below A	T-371	64518.50	94302.89	315.44	100.00	100.88	0.88	228	-45	5	0.01
A+B+C	T-372	64602.04	94304.92	383.85	0.00	5.00	5.00	227	-45	12	0.08
A+B+C	T-372	64599.45	94302.50	380.32	5.00	10.00	5.00	227	-45	16	0.29
A+B+C	T-372	64596.86	94300.09	376.78	10.00	15.00	5.00	227	-45	27	0.34
A+B+C	T-372	64594.28	94297.68	373.25	15.00	20.00	5.00	227	-45	52	0.51
A+B+C	T-372	64591.69	94295.27	369.71	20.00	25.00	5.00	227	-45	128	0.73
A+B+C	T-372	64589.11	94292.85	366.17	25.00	30.00	5.00	227	-45	198	0.98
A+B+C	T-372	64586.52	94290.45	362.64	30.00	33.48	3.48	227	-45	163	0.96
Below A	T-372	64586.52	94290.45	362.64	33.48	35.00	1.52	227	-45	126	0.61

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-372	64583.93	94288.04	359.10	35.00	40.00	5.00	227	-45	59	0.33
Below A	T-372	64581.35	94285.64	355.57	40.00	45.00	5.00	227	-45	19	0.13
Below A	T-372	64578.77	94283.22	352.03	45.00	50.00	5.00	227	-45	29	0.18
Below A	T-372	64576.18	94280.81	348.50	50.00	55.00	5.00	227	-45	55	0.28
Below A	T-372	64573.60	94278.40	344.96	55.00	60.00	5.00	227	-45	102	0.73
Below A	T-372	64571.01	94275.99	341.43	60.00	65.00	5.00	227	-45	23	0.15
Below A	T-372	64568.42	94273.57	337.89	65.00	70.00	5.00	227	-45	174	0.12
Below A	T-372	64565.84	94271.17	334.35	70.00	75.00	5.00	227	-45	19	0.08
Below A	T-372	64563.25	94268.75	330.82	75.00	80.00	5.00	227	-45	87	0.57
Below A	T-372	64560.66	94266.33	327.28	80.00	85.00	5.00	227	-45	86	0.50
Below A	T-372	64558.08	94263.92	323.75	85.00	90.00	5.00	227	-45	16	0.12
Below A	T-372	64555.49	94261.51	320.21	90.00	95.00	5.00	227	-45	14	0.11
Below A	T-372	64552.91	94259.10	316.68	95.00	100.00	5.00	227	-45	28	0.18
Below A	T-372	64551.39	94257.68	314.60	100.00	100.88	0.88	227	-45	10	0.08
Vertical	T-373	64648.18	94356.36	380.74	0.00	5.00	5.00	227	-63	4	0.04
Vertical	T-373	64646.52	94354.82	376.29	5.00	10.00	5.00	227	-63	28	0.29
Vertical	T-373	64644.85	94353.28	371.83	10.00	15.00	5.00	227	-63	20	0.17
Vertical	T-373	64643.18	94351.75	367.38	15.00	20.00	5.00	228	-63	54	0.25
Vertical	T-373	64641.50	94350.21	362.92	20.00	25.00	5.00	228	-63	44	0.26
Vertical	T-373	64639.82	94348.69	358.47	25.00	30.00	5.00	228	-63	463	4.02
Vertical	T-373	64638.14	94347.17	354.01	30.00	35.00	5.00	228	-63	915	9.42
Vertical	T-373	64636.45	94345.65	349.56	35.00	40.00	5.00	228	-63	57	0.43
Vertical	T-373	64634.76	94344.14	345.10	40.00	45.00	5.00	228	-63	22	0.17
Vertical	T-373	64633.06	94342.63	340.65	45.00	50.00	5.00	229	-63	388	2.20
Vertical	T-373	64631.36	94341.12	336.19	50.00	55.00	5.00	229	-63	20	0.27
Vertical	T-373	64629.65	94339.63	331.74	55.00	60.00	5.00	229	-63	31	0.30
Vertical	T-373	64627.94	94338.13	327.29	60.00	65.00	5.00	229	-63	8	0.07
Vertical	T-373	64626.21	94336.62	322.84	65.00	70.00	5.00	229	-63	15	0.21
Vertical	T-373	64624.49	94335.13	318.39	70.00	75.00	5.00	229	-63	129	1.02
Vertical	T-373	64622.75	94333.64	313.95	75.00	80.00	5.00	229	-63	5	0.06
Vertical	T-373	64621.01	94332.14	309.50	80.00	85.00	5.00	229	-63	20	0.20
Vertical	T-373	64619.26	94330.65	305.06	85.00	90.00	5.00	230	-63	32	0.45
Vertical	T-373	64617.51	94329.17	300.62	90.00	95.00	5.00	230	-63	22	0.27
Vertical	T-373	64615.74	94327.67	296.19	95.00	100.00	5.00	230	-63	32	0.28
Vertical	T-373	64613.97	94326.19	291.75	100.00	105.00	5.00	230	-63	17	0.19
Vertical	T-373	64612.21	94324.71	287.32	105.00	110.00	5.00	230	-63	50	0.62
Vertical	T-373	64610.44	94323.24	282.88	110.00	115.00	5.00	230	-63	24	0.27
Vertical	T-373	64608.68	94321.76	278.44	115.00	120.00	5.00	230	-63	21	0.17
Vertical	T-373	64606.92	94320.30	273.99	120.00	121.75	1.75	230	-63	22	0.09
A+B+C	T-373	64606.92	94320.30	273.99	121.75	125.00	3.25	230	-63	1464	11.56
A+B+C	T-373	64605.16	94318.84	269.55	125.00	128.25	3.25	230	-63	378	3.18
Below A	T-373	64605.16	94318.84	269.55	128.25	130.00	1.75	230	-63	9	0.13
Below A	T-373	64603.40	94317.38	265.10	130.00	135.00	5.00	230	-63	24	0.27
Below A	T-373	64601.64	94315.92	260.65	135.00	140.00	5.00	230	-63	32	0.68
Below A	T-373	64599.88	94314.48	256.20	140.00	145.00	5.00	230	-63	161	0.26
Below A	T-373	64598.13	94313.03	251.75	145.00	150.00	5.00	231	-63	106	0.66
Below A	T-373	64596.38	94311.58	247.29	150.00	155.00	5.00	231	-63	43	0.13
Below A	T-373	64594.73	94310.22	243.10	155.00	159.41	4.41	231	-63	20	0.02
A+B+C	T-374	64653.85	94260.24	379.98	0.00	5.00	5.00	227	-45	268	0.39
A+B+C	T-374	64651.26	94257.82	376.45	5.00	10.00	5.00	227	-45	222	3.15
A+B+C	T-374	64648.68	94255.40	372.92	10.00	15.00	5.00	227	-45	607	5.81
A+B+C	T-374	64646.09	94252.98	369.39	15.00	20.00	5.00	227	-45	277	3.68
A+B+C	T-374	64643.50	94250.55	365.87	20.00	25.00	5.00	227	-45	19	0.35
A+B+C	T-374	64640.92	94248.12	362.35	25.00	30.00	5.00	227	-45	80	0.19

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
A+B+C	T-374	64638.33	94245.68	358.83	30.00	35.00	5.00	227	-45	163	0.49
A+B+C	T-374	64635.75	94243.24	355.32	35.00	40.00	5.00	227	-45	28	0.12
A+B+C	T-374	64633.16	94240.79	351.81	40.00	45.00	5.00	227	-45	244	2.34
A+B+C	T-374	64630.57	94238.34	348.30	45.00	50.00	5.00	227	-45	191	0.54
A+B+C	T-374	64627.98	94235.89	344.80	50.00	55.00	5.00	227	-45	95	0.32
A+B+C	T-374	64625.40	94233.42	341.29	55.00	57.90	2.90	227	-45	80	0.43
Below A	T-374	64625.40	94233.42	341.29	57.90	60.00	2.10	227	-45	135	0.76
Below A	T-374	64622.81	94230.97	337.79	60.00	65.00	5.00	227	-45	301	0.78
Below A	T-374	64620.23	94228.52	334.28	65.00	70.00	5.00	227	-45	80	0.14
Below A	T-374	64618.04	94226.45	331.32	70.00	71.00	1.00	227	-45	8	0.04
Vertical	T-375	64672.42	94247.50	378.54	0.00	5.00	5.00	227	-45	0	0.00
Vertical	T-375	64669.84	94245.08	375.01	5.00	5.85	0.85	226	-45	0	0.00
A+B+C	T-375	64669.84	94245.08	375.01	5.85	10.00	4.15	226	-45	182	1.22
A+B+C	T-375	64667.28	94242.64	371.47	10.00	15.00	5.00	226	-45	145	1.13
A+B+C	T-375	64664.73	94240.20	367.94	15.00	20.00	5.00	226	-45	254	2.19
A+B+C	T-375	64662.20	94237.73	364.40	20.00	25.00	5.00	226	-45	31	0.20
A+B+C	T-375	64659.68	94235.25	360.86	25.00	30.00	5.00	225	-45	37	0.16
A+B+C	T-375	64657.18	94232.75	357.33	30.00	35.00	5.00	225	-45	144	0.26
A+B+C	T-375	64654.68	94230.25	353.79	35.00	40.00	5.00	225	-45	161	0.90
A+B+C	T-375	64652.20	94227.73	350.26	40.00	45.00	5.00	225	-45	84	0.42
A+B+C	T-375	64649.72	94225.20	346.72	45.00	49.54	4.54	224	-45	403	2.49
Below A	T-375	64649.72	94225.20	346.72	49.54	50.00	0.46	224	-45	14	0.08
Below A	T-375	64647.27	94222.66	343.19	50.00	55.00	5.00	224	-45	172	0.56
Below A	T-375	64644.81	94220.11	339.65	55.00	60.00	5.00	224	-45	21	0.10
Below A	T-375	64642.36	94217.57	336.12	60.00	65.00	5.00	224	-45	12	0.06
Below A	T-375	64639.90	94215.03	332.58	65.00	70.00	5.00	224	-45	22	0.03
Below A	T-375	64637.44	94212.49	329.04	70.00	75.00	5.00	224	-45	42	0.39
Below A	T-375	64635.85	94210.83	326.75	75.00	76.50	1.50	224	-45	65	0.32
Vertical	T-376	64683.54	94321.50	379.63	0.00	5.00	5.00	227	-54	1	0.00
Vertical	T-376	64681.38	94319.50	375.58	5.00	10.00	5.00	227	-54	14	0.11
Vertical	T-376	64679.23	94317.50	371.53	10.00	15.00	5.00	227	-54	12	0.13
Vertical	T-376	64677.08	94315.51	367.48	15.00	20.00	5.00	227	-54	16	0.08
Vertical	T-376	64674.93	94313.53	363.42	20.00	25.00	5.00	227	-54	336	3.91
Vertical	T-376	64672.77	94311.56	359.37	25.00	30.00	5.00	228	-54	34	0.17
Vertical	T-376	64670.62	94309.59	355.30	30.00	35.00	5.00	228	-54	41	0.37
Vertical	T-376	64668.46	94307.63	351.24	35.00	40.00	5.00	228	-54	28	0.23
Vertical	T-376	64666.31	94305.67	347.18	40.00	45.00	5.00	228	-54	20	0.18
Vertical	T-376	64664.15	94303.73	343.11	45.00	50.00	5.00	228	-55	17	0.11
Vertical	T-376	64661.99	94301.78	339.04	50.00	55.00	5.00	228	-55	11	0.07
Vertical	T-376	64659.83	94299.84	334.96	55.00	60.00	5.00	228	-55	33	0.21
Vertical	T-376	64657.68	94297.91	330.89	60.00	65.00	5.00	228	-55	15	0.14
Vertical	T-376	64655.52	94295.99	326.81	65.00	70.00	5.00	228	-55	31	0.35
Vertical	T-376	64653.36	94294.07	322.73	70.00	75.00	5.00	228	-55	21	0.16
Vertical	T-376	64651.19	94292.15	318.65	75.00	80.00	5.00	229	-55	14	0.09
Vertical	T-376	64649.03	94290.25	314.56	80.00	85.00	5.00	229	-55	36	0.18
Vertical	T-376	64646.87	94288.35	310.47	85.00	90.00	5.00	229	-55	5	0.09
Vertical	T-376	64644.71	94286.46	306.38	90.00	95.00	5.00	229	-55	5	0.04
Vertical	T-376	64642.54	94284.57	302.29	95.00	100.00	5.00	229	-55	32	0.07
Vertical	T-376	64640.38	94282.68	298.19	100.00	103.50	3.50	229	-55	57	0.15
A+B+C	T-376	64640.38	94282.68	298.19	103.50	105.00	1.50	229	-55	986	9.76
A+B+C	T-376	64638.23	94280.81	294.09	105.00	110.00	5.00	229	-55	399	2.64
A+B+C	T-376	64636.07	94278.93	289.99	110.00	115.00	5.00	229	-55	120	0.50
A+B+C	T-376	64633.93	94277.06	285.88	115.00	120.00	5.00	229	-55	134	0.50
A+B+C	T-376	64631.79	94275.18	281.76	120.00	121.65	1.65	229	-55	260	2.25

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-376	64631.79	94275.18	281.76	121.65	125.00	3.35	229	-55	22	0.08
Below A	T-376	64629.66	94273.32	277.64	125.00	130.00	5.00	229	-56	11	0.08
Below A	T-376	64627.54	94271.46	273.51	130.00	135.00	5.00	229	-56	16	0.16
Below A	T-376	64625.43	94269.60	269.38	135.00	140.00	5.00	229	-56	21	0.16
Below A	T-376	64623.32	94267.75	265.25	140.00	145.00	5.00	229	-56	18	0.04
Below A	T-376	64621.22	94265.89	261.11	145.00	150.00	5.00	229	-56	52	0.08
Below A	T-376	64619.12	94264.03	256.96	150.00	155.00	5.00	229	-56	21	0.02
Below A	T-376	64617.79	94262.85	254.32	154.64	156.00	1.36	229	-56	48	0.03
Vertical	T-377	64715.05	94319.65	378.81	0.00	5.00	5.00	227	-51	1	0.03
Vertical	T-377	64712.75	94317.50	374.92	5.00	10.00	5.00	227	-51	45	0.25
Vertical	T-377	64710.45	94315.37	371.03	10.00	15.00	5.00	227	-51	9	0.14
Vertical	T-377	64708.14	94313.25	367.13	15.00	20.00	5.00	227	-51	19	0.13
Vertical	T-377	64705.83	94311.12	363.24	20.00	25.00	5.00	227	-51	71	0.29
Vertical	T-377	64703.52	94309.02	359.34	25.00	30.00	5.00	228	-51	61	0.22
Vertical	T-377	64701.20	94306.91	355.43	30.00	35.00	5.00	228	-51	70	0.40
Vertical	T-377	64698.89	94304.82	351.53	35.00	40.00	5.00	228	-52	6	0.05
Vertical	T-377	64696.58	94302.73	347.62	40.00	45.00	5.00	228	-52	44	0.32
Vertical	T-377	64694.27	94300.64	343.70	45.00	50.00	5.00	228	-52	36	0.24
Vertical	T-377	64691.95	94298.57	339.79	50.00	55.00	5.00	228	-52	24	0.21
Vertical	T-377	64689.63	94296.51	335.87	55.00	60.00	5.00	228	-52	35	0.27
Vertical	T-377	64687.30	94294.46	331.95	60.00	65.00	5.00	229	-52	7	0.07
Vertical	T-377	64684.97	94292.42	328.02	65.00	70.00	5.00	229	-52	7	0.08
Vertical	T-377	64682.64	94290.39	324.10	70.00	75.00	5.00	229	-52	6	0.07
Vertical	T-377	64680.30	94288.35	320.17	75.00	80.00	5.00	229	-52	7	0.06
Vertical	T-377	64677.96	94286.34	316.24	80.00	85.00	5.00	230	-52	8	0.09
Vertical	T-377	64675.61	94284.34	312.30	85.00	90.00	5.00	230	-52	45	2.00
Vertical	T-377	64673.27	94282.34	308.37	90.00	95.00	5.00	230	-52	3	0.08
Vertical	T-377	64670.91	94280.36	304.43	95.00	100.00	5.00	230	-52	7	0.07
Vertical	T-377	64668.55	94278.39	300.49	100.00	105.00	5.00	230	-52	3	0.05
Vertical	T-377	64666.19	94276.41	296.55	105.00	110.00	5.00	230	-52	29	0.15
Vertical	T-377	64663.83	94274.42	292.61	110.00	115.00	5.00	230	-52	42	0.34
Vertical	T-377	64661.48	94272.45	288.67	115.00	116.30	1.30	230	-52	24	0.35
A+B+C	T-377	64661.48	94272.45	288.67	116.30	120.00	3.70	230	-52	295	6.20
A+B+C	T-377	64659.12	94270.47	284.73	120.00	125.00	5.00	230	-52	244	3.24
A+B+C	T-377	64656.76	94268.50	280.79	125.00	127.23	2.23	230	-52	149	1.17
Below A	T-377	64656.76	94268.50	280.79	127.23	130.00	2.77	230	-52	25	0.22
Below A	T-377	64654.40	94266.51	276.85	130.00	135.00	5.00	230	-52	9	0.07
Below A	T-377	64652.04	94264.53	272.91	135.00	140.00	5.00	230	-52	9	0.03
Below A	T-377	64649.68	94262.56	268.97	140.00	145.00	5.00	230	-52	17	0.09
Below A	T-377	64647.55	94260.77	265.41	145.00	147.86	2.86	230	-52	8	0.03
A+B+C	T-378	64623.17	94256.67	380.93	0.00	5.00	5.00	227	-45	0	0.00
A+B+C	T-378	64620.58	94254.26	377.39	5.00	10.00	5.00	228	-45	87	0.82
A+B+C	T-378	64617.98	94251.88	373.85	10.00	15.00	5.00	228	-45	38	0.23
A+B+C	T-378	64615.36	94249.51	370.31	15.00	20.00	5.00	228	-45	22	0.24
A+B+C	T-378	64612.75	94247.15	366.76	20.00	25.00	5.00	228	-45	31	0.21
A+B+C	T-378	64610.12	94244.81	363.21	25.00	30.00	5.00	229	-45	41	0.26
A+B+C	T-378	64607.48	94242.48	359.65	30.00	35.00	5.00	229	-45	102	0.32
A+B+C	T-378	64604.84	94240.17	356.10	35.00	40.00	5.00	229	-45	37	0.44
A+B+C	T-378	64602.19	94237.86	352.54	40.00	43.58	3.58	229	-45	262	1.73
Below A	T-378	64602.19	94237.86	352.54	43.58	45.00	1.42	229	-45	39	0.16
Below A	T-378	64599.53	94235.57	348.97	45.00	50.00	5.00	230	-46	145	0.75
Below A	T-378	64596.87	94233.29	345.41	50.00	55.00	5.00	230	-46	76	0.12
Below A	T-378	64594.20	94231.02	341.84	55.00	60.00	5.00	230	-46	64	0.50
Below A	T-378	64591.72	94228.89	338.52	60.00	63.00	3.00	230	-46	15	0.10

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
A+B+C	T-379	64689.65	94227.75	377.36	0.00	5.00	5.00	227	-45	118	3.25
A+B+C	T-379	64687.07	94225.32	373.82	5.00	10.00	5.00	227	-45	95	1.19
A+B+C	T-379	64684.51	94222.90	370.28	10.00	15.00	5.00	227	-45	63	0.28
A+B+C	T-379	64681.96	94220.47	366.74	15.00	20.00	5.00	226	-45	41	0.69
A+B+C	T-379	64679.42	94218.03	363.19	20.00	25.00	5.00	226	-45	28	0.30
A+B+C	T-379	64676.89	94215.57	359.64	25.00	30.00	5.00	226	-45	30	0.10
A+B+C	T-379	64674.38	94213.11	356.08	30.00	35.00	5.00	226	-45	84	0.29
A+B+C	T-379	64671.86	94210.66	352.53	35.00	37.55	2.55	225	-46	417	2.05
Below A	T-379	64671.86	94210.66	352.53	37.55	40.00	2.45	225	-46	16	0.10
Below A	T-379	64669.38	94208.18	348.96	40.00	45.00	5.00	225	-46	14	0.04
Below A	T-379	64666.90	94205.71	345.40	45.00	50.00	5.00	225	-46	8	0.02
Below A	T-379	64665.14	94203.94	342.86	50.00	52.12	2.12	225	-46	5	0.04
Vertical	T-380	64529.07	94367.51	384.49	0.00	5.00	5.00	47	-57	1	0.00
Vertical	T-380	64531.06	94369.35	380.30	5.00	10.00	5.00	47	-57	33	0.28
Vertical	T-380	64533.05	94371.20	376.10	10.00	15.00	5.00	47	-57	11	0.14
Vertical	T-380	64535.05	94373.04	371.90	15.00	20.00	5.00	47	-57	8	0.16
Vertical	T-380	64537.04	94374.88	367.70	20.00	25.00	5.00	47	-57	4	0.10
Vertical	T-380	64539.04	94376.71	363.49	25.00	30.00	5.00	48	-57	15	0.17
Vertical	T-380	64541.03	94378.53	359.28	30.00	35.00	5.00	48	-57	22	0.19
Vertical	T-380	64543.03	94380.35	355.07	35.00	40.00	5.00	48	-57	22	0.19
Vertical	T-380	64545.02	94382.16	350.86	40.00	45.00	5.00	48	-57	11	0.15
Vertical	T-380	64547.02	94383.96	346.65	45.00	50.00	5.00	48	-58	49	0.39
Vertical	T-380	64549.01	94385.75	342.43	50.00	55.00	5.00	48	-58	34	0.30
Vertical	T-380	64551.01	94387.56	338.21	55.00	60.00	5.00	48	-58	8	0.12
Vertical	T-380	64553.02	94389.34	334.00	60.00	65.00	5.00	48	-58	23	0.28
Vertical	T-380	64555.03	94391.12	329.78	65.00	70.00	5.00	49	-58	17	0.28
Vertical	T-380	64557.05	94392.89	325.56	70.00	75.00	5.00	49	-58	9	0.13
Vertical	T-380	64559.07	94394.67	321.35	75.00	80.00	5.00	49	-58	8	0.12
Vertical	T-380	64561.09	94396.43	317.13	80.00	85.00	5.00	49	-58	12	0.13
Vertical	T-380	64563.12	94398.19	312.91	85.00	90.00	5.00	49	-58	9	0.24
Vertical	T-380	64565.15	94399.95	308.69	90.00	95.00	5.00	49	-58	6	0.14
Vertical	T-380	64567.20	94401.70	304.48	95.00	100.00	5.00	50	-58	2	0.03
Vertical	T-380	64569.24	94403.44	300.26	100.00	105.00	5.00	50	-58	28	0.22
Vertical	T-380	64571.28	94405.19	296.04	105.00	110.00	5.00	50	-58	14	0.10
Vertical	T-380	64573.32	94406.93	291.83	110.00	115.00	5.00	50	-58	2	0.03
Vertical	T-380	64575.37	94408.67	287.61	115.00	120.00	5.00	50	-58	4	0.08
Vertical	T-380	64577.41	94410.42	283.39	120.00	125.00	5.00	50	-58	6	0.08
Vertical	T-380	64579.45	94412.17	279.18	125.00	130.00	5.00	50	-58	6	0.08
Vertical	T-380	64581.50	94413.91	274.96	130.00	135.00	5.00	50	-58	174	0.78
Vertical	T-380	64583.54	94415.65	270.74	135.00	140.00	5.00	50	-58	2	0.03
Vertical	T-380	64585.41	94417.25	266.87	140.00	144.17	4.17	50	-58	3	0.02
Karina	T-381	64857.61	94214.94	362.95	21.94	25.00	3.06	168	-56	65	0.77
Karina	T-381	64858.19	94212.21	358.80	25.00	30.00	5.00	168	-56	65	0.93
Karina	T-381	64858.77	94209.47	354.66	30.00	33.90	3.90	168	-56	18	0.25
Karina	T-382	64809.25	94205.59	358.30	26.40	30.00	3.60	168	-54	36	0.29
Karina	T-382	64809.87	94202.69	354.27	30.00	35.00	5.00	168	-54	53	0.48
Karina	T-382	64810.48	94199.80	350.24	35.00	40.00	5.00	168	-54	87	0.65
Karina	T-382	64811.10	94196.89	346.22	40.00	40.45	0.45	168	-54	25	0.33
Karina	T-384	64784.74	94209.33	353.54	34.75	35.00	0.25	169	-54	233	2.17
Karina	T-384	64785.29	94206.46	349.48	35.00	40.00	5.00	169	-54	84	0.70
Karina	T-384	64785.84	94203.60	345.41	40.00	45.00	5.00	169	-54	106	0.86
Karina	T-384	64786.37	94200.75	341.35	45.00	46.15	1.15	170	-55	77	0.60
Vertical	T-412	64713.12	94280.22	378.60	0.00	5.00	5.00	227	-50	11	0.13
Vertical	T-412	64710.79	94278.01	374.77	5.00	10.00	5.00	226	-50	8	0.23

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-412	64708.48	94275.81	370.92	10.00	15.00	5.00	226	-50	14	0.62
Vertical	T-412	64706.20	94273.59	367.07	15.00	20.00	5.00	226	-51	13	0.36
Vertical	T-412	64703.93	94271.36	363.21	20.00	25.00	5.00	226	-51	43	0.14
Vertical	T-412	64701.68	94269.12	359.34	25.00	30.00	5.00	225	-51	29	0.20
Vertical	T-412	64699.46	94266.88	355.47	30.00	35.00	5.00	225	-51	9	0.12
Vertical	T-412	64697.25	94264.63	351.59	35.00	40.00	5.00	224	-51	4	0.04
Vertical	T-412	64695.07	94262.36	347.70	40.00	45.00	5.00	224	-51	11	0.10
Vertical	T-412	64692.88	94260.10	343.82	45.00	50.00	5.00	224	-51	33	0.22
Vertical	T-412	64690.69	94257.85	339.93	50.00	55.00	5.00	224	-51	22	0.15
Vertical	T-412	64688.50	94255.59	336.04	55.00	60.00	5.00	224	-51	44	0.40
Vertical	T-412	64686.30	94253.34	332.16	60.00	65.00	5.00	224	-51	11	0.14
Vertical	T-412	64684.11	94251.09	328.27	65.00	70.00	5.00	224	-51	4	0.08
Vertical	T-412	64681.91	94248.83	324.39	70.00	75.00	5.00	224	-51	12	0.15
Vertical	T-412	64679.71	94246.58	320.50	75.00	79.35	4.35	224	-51	22	0.06
A+B+C	T-412	64679.71	94246.58	320.50	79.35	80.00	0.65	224	-51	32	0.44
A+B+C	T-412	64677.51	94244.33	316.62	80.00	85.00	5.00	224	-51	530	4.04
A+B+C	T-412	64675.30	94242.09	312.73	85.00	90.00	5.00	225	-51	362	2.35
A+B+C	T-412	64673.10	94239.84	308.84	90.00	90.50	0.50	225	-51	204	3.19
Below A	T-412	64673.10	94239.84	308.84	90.50	93.20	2.70	225	-51	24	0.18
Vertical	T-413	64640.59	94321.38	381.32	0.00	5.00	5.00	227	-50	91	0.81
Vertical	T-413	64638.23	94319.17	377.50	5.00	10.00	5.00	227	-50	104	1.40
Vertical	T-413	64635.89	94316.97	373.67	10.00	15.00	5.00	227	-50	85	0.78
Vertical	T-413	64633.54	94314.76	369.85	15.00	20.00	5.00	227	-50	47	0.26
Vertical	T-413	64631.20	94312.54	366.03	20.00	25.00	5.00	227	-50	119	1.65
Vertical	T-413	64628.86	94310.32	362.22	25.00	30.00	5.00	226	-50	102	1.02
Vertical	T-413	64626.52	94308.08	358.40	30.00	35.00	5.00	226	-50	33	0.41
Vertical	T-413	64624.18	94305.85	354.59	35.00	40.00	5.00	226	-50	29	0.29
Vertical	T-413	64621.84	94303.59	350.79	40.00	45.00	5.00	226	-50	36	0.31
Vertical	T-413	64619.51	94301.33	346.99	45.00	50.00	5.00	226	-50	21	0.18
Vertical	T-413	64617.17	94299.08	343.19	50.00	55.00	5.00	226	-49	56	0.36
Vertical	T-413	64614.82	94296.82	339.39	55.00	60.00	5.00	226	-49	31	0.23
Vertical	T-413	64612.47	94294.56	335.60	60.00	65.00	5.00	226	-49	13	0.10
Vertical	T-413	64610.12	94292.30	331.81	65.00	67.65	2.65	226	-49	50	0.13
A+B+C	T-413	64610.12	94292.30	331.81	67.65	70.00	2.35	226	-49	739	5.74
A+B+C	T-413	64607.76	94290.05	328.02	70.00	75.00	5.00	226	-49	211	2.26
A+B+C	T-413	64605.40	94287.79	324.23	75.00	80.00	5.00	226	-49	315	3.59
A+B+C	T-413	64603.04	94285.53	320.45	80.00	85.00	5.00	226	-49	229	1.39
A+B+C	T-413	64600.66	94283.28	316.67	85.00	90.00	5.00	226	-49	443	1.13
A+B+C	T-413	64598.29	94281.01	312.89	90.00	95.00	5.00	227	-49	80	0.43
A+B+C	T-413	64595.91	94278.75	309.12	95.00	99.70	4.70	227	-49	336	1.58
Below A	T-413	64595.91	94278.75	309.12	99.70	100.00	0.30	227	-49	47	0.95
Below A	T-413	64593.52	94276.51	305.35	100.00	105.00	5.00	227	-49	33	0.29
Below A	T-413	64591.12	94274.28	301.57	105.00	110.00	5.00	227	-49	32	0.17
Below A	T-413	64588.71	94272.06	297.80	110.00	115.00	5.00	228	-49	214	0.71
Below A	T-413	64586.29	94269.85	294.03	115.00	120.00	5.00	228	-49	21	0.05
Below A	T-413	64583.86	94267.63	290.25	120.00	125.00	5.00	229	-49	26	0.10
Below A	T-413	64581.41	94265.45	286.48	125.00	128.00	3.00	229	-49	23	0.13
Vertical	T-414	64667.58	94306.77	380.18	0.00	5.00	5.00	224	-50	13	0.19
Vertical	T-414	64665.35	94304.46	376.35	5.00	10.00	5.00	224	-50	35	0.45
Vertical	T-414	64663.13	94302.16	372.51	10.00	15.00	5.00	224	-50	54	0.48
Vertical	T-414	64660.91	94299.86	368.67	15.00	20.00	5.00	224	-50	84	0.47
Vertical	T-414	64658.69	94297.55	364.83	20.00	25.00	5.00	224	-50	36	0.18
Vertical	T-414	64656.47	94295.26	360.98	25.00	30.00	5.00	224	-50	43	0.16
Vertical	T-414	64654.26	94292.97	357.12	30.00	35.00	5.00	224	-51	10	0.08

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-414	64652.05	94290.68	353.26	35.00	40.00	5.00	224	-51	12	0.09
Vertical	T-414	64649.85	94288.41	349.39	40.00	45.00	5.00	224	-51	14	0.14
Vertical	T-414	64647.66	94286.14	345.52	45.00	50.00	5.00	224	-51	68	0.34
Vertical	T-414	64645.46	94283.86	341.64	50.00	55.00	5.00	224	-51	21	0.15
Vertical	T-414	64643.28	94281.60	337.76	55.00	60.00	5.00	224	-51	20	0.07
Vertical	T-414	64641.09	94279.33	333.87	60.00	65.00	5.00	224	-51	20	0.06
Vertical	T-414	64638.91	94277.07	329.98	65.00	68.65	3.65	224	-51	15	0.09
A+B+C	T-414	64638.91	94277.07	329.98	68.65	70.00	1.35	224	-51	167	1.37
A+B+C	T-414	64636.73	94274.82	326.09	70.00	75.00	5.00	224	-51	284	2.93
A+B+C	T-414	64634.54	94272.56	322.20	75.00	80.00	5.00	224	-51	347	2.56
A+B+C	T-414	64632.36	94270.30	318.31	80.00	85.00	5.00	224	-51	114	0.52
A+B+C	T-414	64630.19	94268.04	314.41	85.00	90.00	5.00	224	-51	80	0.66
A+B+C	T-414	64628.01	94265.78	310.52	90.00	95.00	5.00	224	-51	159	0.98
A+B+C	T-414	64625.84	94263.53	306.62	95.00	100.00	5.00	224	-51	162	0.77
A+B+C	T-414	64623.66	94261.28	302.72	100.00	100.55	0.55	224	-51	188	1.89
Below A	T-414	64623.66	94261.28	302.72	100.55	105.00	4.45	224	-51	29	0.19
Below A	T-414	64621.48	94259.03	298.83	105.00	110.00	5.00	224	-51	104	0.56
Below A	T-414	64619.31	94256.78	294.92	110.00	115.00	5.00	224	-51	70	0.30
Below A	T-414	64617.14	94254.53	291.02	115.00	120.00	5.00	224	-51	148	0.78
Below A	T-414	64614.97	94252.28	287.12	120.00	125.00	5.00	224	-51	72	0.14
Below A	T-414	64613.77	94251.04	284.96	125.00	125.52	0.52	224	-51	45	0.06
Vertical	T-415	64681.55	94360.32	379.44	0.00	5.00	5.00	225	-52	0	0.00
Vertical	T-415	64679.36	94358.12	375.51	5.00	10.00	5.00	225	-52	0	0.00
Vertical	T-415	64677.16	94355.92	371.59	10.00	15.00	5.00	225	-52	0	0.00
Vertical	T-415	64674.97	94353.72	367.68	15.00	20.00	5.00	225	-52	29	0.14
Vertical	T-415	64672.79	94351.50	363.76	20.00	25.00	5.00	225	-52	16	0.13
Vertical	T-415	64670.60	94349.29	359.85	25.00	30.00	5.00	225	-52	21	0.13
Vertical	T-415	64668.41	94347.07	355.93	30.00	35.00	5.00	224	-52	55	0.29
Vertical	T-415	64666.24	94344.85	352.02	35.00	40.00	5.00	224	-52	47	0.21
Vertical	T-415	64664.06	94342.62	348.11	40.00	45.00	5.00	224	-51	76	0.60
Vertical	T-415	64661.88	94340.39	344.20	45.00	50.00	5.00	224	-51	33	0.16
Vertical	T-415	64659.71	94338.14	340.29	50.00	55.00	5.00	224	-51	13	0.13
Vertical	T-415	64657.54	94335.90	336.39	55.00	60.00	5.00	224	-51	20	0.17
Vertical	T-415	64655.37	94333.65	332.49	60.00	65.00	5.00	224	-51	7	0.08
Vertical	T-415	64653.19	94331.40	328.58	65.00	70.00	5.00	224	-51	6	0.04
Vertical	T-415	64651.01	94329.16	324.68	70.00	75.00	5.00	224	-51	15	0.11
Vertical	T-415	64648.83	94326.93	320.78	75.00	80.00	5.00	224	-51	34	0.28
Vertical	T-415	64646.65	94324.71	316.87	80.00	85.00	5.00	224	-51	11	0.15
Vertical	T-415	64644.46	94322.48	312.96	85.00	90.00	5.00	225	-51	7	0.08
Vertical	T-415	64642.27	94320.25	309.05	90.00	95.00	5.00	225	-51	12	0.14
Vertical	T-415	64640.08	94318.04	305.14	95.00	100.00	5.00	225	-52	21	0.14
Vertical	T-415	64637.89	94315.84	301.23	100.00	105.00	5.00	225	-52	6	0.10
Vertical	T-415	64635.69	94313.64	297.32	105.00	110.00	5.00	225	-52	25	0.28
Vertical	T-415	64633.49	94311.43	293.41	110.00	115.00	5.00	225	-52	42	0.41
Vertical	T-415	64631.29	94309.24	289.49	115.00	120.00	5.00	225	-52	6	0.10
Vertical	T-415	64629.08	94307.04	285.58	120.00	125.00	5.00	225	-52	9	0.13
Vertical	T-415	64626.86	94304.85	281.67	125.00	130.00	5.00	226	-52	12	0.10
Vertical	T-415	64624.64	94302.67	277.75	130.00	130.78	0.78	226	-52	38	0.10
A+B+C	T-415	64624.64	94302.67	277.75	130.78	135.00	4.22	226	-52	969	8.45
A+B+C	T-415	64622.41	94300.50	273.84	135.00	140.00	5.00	226	-52	179	1.16
A+B+C	T-415	64620.19	94298.32	269.93	140.00	145.00	5.00	226	-52	43	0.14
A+B+C	T-415	64617.96	94296.15	266.01	145.00	150.00	5.00	226	-52	262	1.50
A+B+C	T-415	64615.72	94293.99	262.10	150.00	151.85	1.85	226	-52	308	1.60
Below A	T-415	64615.72	94293.99	262.10	151.85	155.00	3.15	226	-52	56	0.11

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-415	64613.48	94291.82	258.19	155.00	160.00	5.00	226	-52	37	0.03
Below A	T-415	64611.25	94289.66	254.27	160.00	165.00	5.00	226	-52	16	0.03
Below A	T-415	64609.00	94287.50	250.36	165.00	170.00	5.00	226	-52	5	0.03
Below A	T-415	64607.60	94286.14	247.90	170.00	171.28	1.28	226	-52	25	0.03
Vertical	T-416	64632.37	94343.17	381.49	0.00	5.00	5.00	226	-56	3	0.02
Vertical	T-416	64630.34	94341.21	377.37	5.00	10.00	5.00	226	-56	18	0.21
Vertical	T-416	64628.29	94339.25	373.25	10.00	15.00	5.00	226	-55	25	0.16
Vertical	T-416	64626.24	94337.28	369.14	15.00	20.00	5.00	226	-55	20	0.15
Vertical	T-416	64624.19	94335.31	365.02	20.00	25.00	5.00	226	-55	74	0.49
Vertical	T-416	64622.13	94333.35	360.91	25.00	30.00	5.00	226	-55	165	1.90
Vertical	T-416	64620.06	94331.39	356.80	30.00	35.00	5.00	227	-55	82	0.69
Vertical	T-416	64617.99	94329.42	352.69	35.00	40.00	5.00	227	-55	114	0.78
Vertical	T-416	64615.91	94327.46	348.59	40.00	45.00	5.00	227	-55	66	0.52
Vertical	T-416	64613.83	94325.51	344.49	45.00	50.00	5.00	227	-55	14	0.15
Vertical	T-416	64611.74	94323.55	340.39	50.00	55.00	5.00	227	-55	99	0.80
Vertical	T-416	64609.65	94321.59	336.29	55.00	60.00	5.00	227	-55	58	0.47
Vertical	T-416	64607.55	94319.64	332.20	60.00	65.00	5.00	227	-55	13	0.14
Vertical	T-416	64605.45	94317.69	328.10	65.00	70.00	5.00	227	-55	6	0.12
Vertical	T-416	64603.34	94315.75	324.00	70.00	75.00	5.00	227	-55	79	0.69
Vertical	T-416	64601.22	94313.82	319.91	75.00	80.00	5.00	228	-55	10	0.16
Vertical	T-416	64599.10	94311.89	315.81	80.00	83.60	3.60	228	-55	16	0.23
A+B+C	T-416	64599.10	94311.89	315.81	83.60	85.00	1.40	228	-55	803	7.21
A+B+C	T-416	64596.97	94309.96	311.72	85.00	90.00	5.00	228	-55	375	2.78
A+B+C	T-416	64594.84	94308.05	307.62	90.00	95.00	5.00	228	-55	1109	10.09
A+B+C	T-416	64592.70	94306.14	303.53	95.00	100.00	5.00	229	-55	52	0.09
A+B+C	T-416	64590.55	94304.24	299.43	100.00	101.18	1.18	229	-55	125	0.63
Below A	T-416	64590.55	94304.24	299.43	101.18	105.00	3.82	229	-55	46	0.24
Below A	T-416	64588.40	94302.33	295.33	105.00	110.00	5.00	229	-55	73	0.41
Below A	T-416	64586.23	94300.45	291.24	110.00	115.00	5.00	229	-55	35	0.22
Below A	T-416	64584.07	94298.57	287.14	115.00	120.00	5.00	229	-55	39	0.27
Below A	T-416	64581.91	94296.69	283.05	120.00	125.00	5.00	229	-55	22	0.24
Below A	T-416	64580.70	94295.64	280.77	125.00	125.57	0.57	229	-55	18	0.03
Vertical	T-417	64669.87	94376.66	379.27	0.00	5.00	5.00	228	-60	3	0.01
Vertical	T-417	64668.02	94374.97	374.94	5.00	10.00	5.00	228	-60	16	0.06
Vertical	T-417	64666.19	94373.29	370.61	10.00	15.00	5.00	228	-60	10	0.10
Vertical	T-417	64664.36	94371.61	366.27	15.00	20.00	5.00	228	-60	6	0.08
Vertical	T-417	64662.54	94369.94	361.92	20.00	25.00	5.00	228	-61	24	0.10
Vertical	T-417	64660.72	94368.28	357.57	25.00	30.00	5.00	228	-61	11	0.04
Vertical	T-417	64658.91	94366.62	353.22	30.00	35.00	5.00	228	-61	47	0.29
Vertical	T-417	64657.10	94364.96	348.86	35.00	40.00	5.00	228	-61	12	0.09
Vertical	T-417	64655.30	94363.31	344.50	40.00	45.00	5.00	228	-61	12	0.08
Vertical	T-417	64653.51	94361.67	340.13	45.00	50.00	5.00	228	-61	22	0.12
Vertical	T-417	64651.72	94360.03	335.76	50.00	55.00	5.00	228	-61	13	0.05
Vertical	T-417	64649.93	94358.39	331.38	55.00	60.00	5.00	228	-61	25	0.17
Vertical	T-417	64648.14	94356.76	327.01	60.00	65.00	5.00	228	-61	7	0.09
Vertical	T-417	64646.35	94355.12	322.64	65.00	70.00	5.00	228	-61	13	0.14
Vertical	T-417	64644.55	94353.49	318.26	70.00	75.00	5.00	228	-61	53	0.63
Vertical	T-417	64642.76	94351.85	313.89	75.00	80.00	5.00	228	-61	6	0.13
Vertical	T-417	64640.97	94350.23	309.52	80.00	85.00	5.00	228	-61	43	0.34
Vertical	T-417	64639.17	94348.60	305.14	85.00	90.00	5.00	228	-61	4	0.05
Vertical	T-417	64637.37	94346.98	300.77	90.00	95.00	5.00	228	-61	4	0.05
Vertical	T-417	64635.57	94345.35	296.40	95.00	100.00	5.00	228	-61	4	0.04
Vertical	T-417	64633.77	94343.74	292.02	100.00	105.00	5.00	228	-61	25	0.24
Vertical	T-417	64631.97	94342.12	287.65	105.00	110.00	5.00	228	-61	8	0.10

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-417	64630.18	94340.51	283.27	110.00	115.00	5.00	228	-61	7	0.10
Vertical	T-417	64628.38	94338.92	278.88	115.00	120.00	5.00	228	-61	8	0.11
Vertical	T-417	64626.59	94337.33	274.49	120.00	125.00	5.00	228	-61	10	0.16
Vertical	T-417	64624.81	94335.75	270.09	125.00	130.00	5.00	229	-62	7	0.06
Vertical	T-417	64623.02	94334.17	265.70	130.00	135.00	5.00	229	-62	12	0.10
Vertical	T-417	64621.24	94332.61	261.29	135.00	140.00	5.00	229	-62	12	0.13
Vertical	T-417	64619.46	94331.06	256.89	140.00	145.00	5.00	229	-62	11	0.11
Vertical	T-417	64617.69	94329.50	252.48	145.00	150.00	5.00	229	-62	7	0.04
Vertical	T-417	64615.92	94327.96	248.06	150.00	150.83	0.83	229	-62	33	0.08
A+B+C	T-417	64615.92	94327.96	248.06	151.93	155.00	3.07	229	-62	151	1.34
Below A	T-417	64615.92	94327.96	248.06	153.90	155.00	1.10	229	-62	7	0.09
Below A	T-417	64614.15	94326.42	243.65	155.00	160.00	5.00	229	-62	23	0.19
Below A	T-417	64612.38	94324.89	239.23	160.00	165.00	5.00	229	-62	11	0.04
Below A	T-417	64610.61	94323.34	234.82	165.00	170.00	5.00	229	-62	102	0.41
Below A	T-417	64608.83	94321.80	230.41	170.00	175.00	5.00	229	-62	7	0.04
Below A	T-417	64607.06	94320.26	225.99	175.00	180.00	5.00	229	-62	3	0.01
Below A	T-417	64606.05	94319.38	223.46	180.00	180.73	0.73	229	-62	2	0.02
Vertical	T-418	64697.81	94335.51	378.97	0.00	5.00	5.00	226	-60	1	0.01
Vertical	T-418	64696.03	94333.79	374.63	5.00	10.00	5.00	226	-60	9	0.11
Vertical	T-418	64694.25	94332.07	370.28	10.00	15.00	5.00	226	-60	4	0.08
Vertical	T-418	64692.48	94330.35	365.93	15.00	20.00	5.00	226	-60	15	0.21
Vertical	T-418	64690.71	94328.63	361.58	20.00	25.00	5.00	226	-61	17	0.10
Vertical	T-418	64688.94	94326.92	357.23	25.00	30.00	5.00	226	-61	20	0.12
Vertical	T-418	64687.18	94325.21	352.88	30.00	35.00	5.00	226	-61	34	0.14
Vertical	T-418	64685.42	94323.49	348.52	35.00	40.00	5.00	226	-61	9	0.09
Vertical	T-418	64683.66	94321.78	344.17	40.00	45.00	5.00	226	-61	19	0.11
Vertical	T-418	64681.92	94320.06	339.81	45.00	50.00	5.00	226	-61	27	0.16
Vertical	T-418	64680.17	94318.35	335.45	50.00	55.00	5.00	226	-61	8	0.05
Vertical	T-418	64678.43	94316.64	331.08	55.00	60.00	5.00	226	-61	2	0.07
Vertical	T-418	64676.68	94314.93	326.72	60.00	65.00	5.00	226	-61	8	0.09
Vertical	T-418	64674.93	94313.24	322.36	65.00	70.00	5.00	226	-61	9	0.10
Vertical	T-418	64673.18	94311.53	317.99	70.00	75.00	5.00	226	-61	13	0.11
Vertical	T-418	64671.43	94309.85	313.62	75.00	80.00	5.00	226	-61	49	0.96
Vertical	T-418	64669.68	94308.16	309.25	80.00	85.00	5.00	226	-61	11	0.13
Vertical	T-418	64667.92	94306.48	304.89	85.00	90.00	5.00	226	-61	11	0.16
Vertical	T-418	64666.16	94304.80	300.52	90.00	95.00	5.00	226	-61	6	0.21
Vertical	T-418	64664.40	94303.13	296.15	95.00	100.00	5.00	227	-61	7	0.10
Vertical	T-418	64662.64	94301.46	291.77	100.00	105.00	5.00	227	-61	20	0.10
Vertical	T-418	64660.88	94299.78	287.40	105.00	110.00	5.00	227	-61	12	0.09
Vertical	T-418	64659.12	94298.11	283.03	110.00	115.00	5.00	227	-61	15	0.13
Vertical	T-418	64657.37	94296.45	278.65	115.00	120.00	5.00	227	-61	10	0.10
Vertical	T-418	64655.61	94294.78	274.28	120.00	125.00	5.00	227	-61	15	0.27
Vertical	T-418	64653.85	94293.11	269.91	125.00	130.00	5.00	227	-61	79	0.10
Vertical	T-418	64652.09	94291.44	265.53	130.00	131.00	1.00	227	-61	10	0.04
A+B+C	T-418	64652.09	94291.44	265.53	131.00	135.00	4.00	227	-61	135	2.88
A+B+C	T-418	64650.33	94289.78	261.16	135.00	138.10	3.10	227	-61	357	2.41
Below A	T-418	64650.33	94289.78	261.16	138.10	140.00	1.90	227	-61	19	0.06
Below A	T-418	64648.57	94288.10	256.79	140.00	145.00	5.00	227	-61	9	0.03
Below A	T-418	64646.82	94286.43	252.41	145.00	150.00	5.00	227	-61	9	0.02
Below A	T-418	64645.06	94284.77	248.04	150.00	155.00	5.00	227	-61	23	0.03
Below A	T-418	64643.48	94283.28	244.13	155.00	156.00	1.00	227	-61	7	0.03
Vertical	T-419	64744.96	94282.40	378.08	0.00	5.00	5.00	224	-51	9	0.09
Vertical	T-419	64742.76	94280.11	374.22	5.00	10.00	5.00	224	-51	18	0.31
Vertical	T-419	64740.55	94277.83	370.36	10.00	15.00	5.00	224	-51	99	0.40

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-419	64738.35	94275.56	366.49	15.00	20.00	5.00	224	-51	38	0.50
Vertical	T-419	64736.15	94273.29	362.61	20.00	25.00	5.00	224	-51	29	0.16
Vertical	T-419	64733.95	94271.03	358.73	25.00	30.00	5.00	224	-51	13	0.11
Vertical	T-419	64731.76	94268.78	354.84	30.00	35.00	5.00	224	-51	13	0.14
Vertical	T-419	64729.57	94266.53	350.95	35.00	40.00	5.00	224	-51	7	0.07
Vertical	T-419	64727.39	94264.29	347.05	40.00	45.00	5.00	224	-51	34	0.19
Vertical	T-419	64725.20	94262.07	343.14	45.00	50.00	5.00	225	-52	5	0.07
Vertical	T-419	64723.02	94259.85	339.23	50.00	55.00	5.00	225	-52	5	0.10
Vertical	T-419	64720.84	94257.64	335.31	55.00	60.00	5.00	225	-52	6	0.06
Vertical	T-419	64718.66	94255.42	331.39	60.00	65.00	5.00	225	-52	12	0.08
Vertical	T-419	64716.48	94253.22	327.47	65.00	70.00	5.00	225	-52	19	0.11
Vertical	T-419	64714.30	94251.02	323.55	70.00	75.00	5.00	225	-52	4	0.07
Vertical	T-419	64712.12	94248.82	319.62	75.00	80.00	5.00	225	-52	5	0.09
Vertical	T-419	64709.94	94246.63	315.69	80.00	85.00	5.00	225	-52	22	0.40
Vertical	T-419	64707.76	94244.44	311.76	85.00	90.00	5.00	225	-52	2	0.07
Vertical	T-419	64705.58	94242.25	307.82	90.00	94.48	4.48	225	-52	16	0.07
A+B+C	T-419	64705.58	94242.25	307.82	94.48	95.00	0.52	225	-52	247	1.29
A+B+C	T-419	64703.40	94240.07	303.89	95.00	97.10	2.10	225	-52	178	0.85
Below A	T-419	64703.40	94240.07	303.89	97.10	100.00	2.90	225	-52	12	0.11
Below A	T-419	64701.23	94237.89	299.95	100.00	102.00	2.00	225	-52	2	0.04
Vertical	T-420	64609.32	94408.44	380.57	0.00	5.00	5.00	226	-61	3	0.02
Vertical	T-420	64607.57	94406.76	376.20	5.00	10.00	5.00	226	-61	12	0.02
Vertical	T-420	64605.84	94405.08	371.82	10.00	15.00	5.00	226	-61	7	0.03
Vertical	T-420	64604.10	94403.40	367.45	15.00	20.00	5.00	226	-61	6	0.05
Vertical	T-420	64602.36	94401.73	363.07	20.00	25.00	5.00	226	-61	3	0.03
Vertical	T-420	64600.62	94400.06	358.69	25.00	30.00	5.00	226	-61	39	0.21
Vertical	T-420	64598.89	94398.39	354.31	30.00	35.00	5.00	226	-61	7	0.06
Vertical	T-420	64597.16	94396.71	349.92	35.00	40.00	5.00	226	-61	159	1.09
Vertical	T-420	64595.44	94395.04	345.54	40.00	45.00	5.00	226	-61	5	0.10
Vertical	T-420	64593.71	94393.38	341.15	45.00	50.00	5.00	226	-61	2	0.06
Vertical	T-420	64591.98	94391.71	336.77	50.00	55.00	5.00	227	-61	18	0.34
Vertical	T-420	64590.23	94390.07	332.38	55.00	60.00	5.00	227	-61	2	0.07
Vertical	T-420	64588.48	94388.42	327.99	60.00	65.00	5.00	227	-61	2	0.05
Vertical	T-420	64586.73	94386.80	323.60	65.00	70.00	5.00	227	-61	62	0.96
Vertical	T-420	64584.96	94385.17	319.21	70.00	75.00	5.00	228	-61	3	0.07
Vertical	T-420	64583.20	94383.57	314.82	75.00	80.00	5.00	228	-61	41	0.43
Vertical	T-420	64581.42	94381.96	310.43	80.00	85.00	5.00	229	-62	6	0.11
Vertical	T-420	64579.64	94380.38	306.04	85.00	90.00	5.00	229	-62	5	0.16
Vertical	T-420	64577.85	94378.79	301.64	90.00	95.00	5.00	229	-62	5	0.15
Vertical	T-420	64576.06	94377.21	297.25	95.00	100.00	5.00	229	-62	276	2.62
Vertical	T-420	64574.27	94375.64	292.85	100.00	105.00	5.00	229	-62	71	0.79
Vertical	T-420	64572.48	94374.07	288.46	105.00	110.00	5.00	229	-62	16	0.16
Vertical	T-420	64570.70	94372.50	284.06	110.00	115.00	5.00	229	-62	13	0.21
Vertical	T-420	64568.91	94370.92	279.66	115.00	120.00	5.00	229	-62	22	0.34
Vertical	T-420	64567.12	94369.36	275.26	120.00	125.00	5.00	229	-62	10	0.23
Vertical	T-420	64565.33	94367.79	270.86	125.00	130.00	5.00	229	-62	9	0.15
Vertical	T-420	64563.54	94366.23	266.46	130.00	135.00	5.00	229	-62	19	0.35
Vertical	T-420	64561.75	94364.68	262.06	135.00	136.80	1.80	229	-62	5	0.09
A+B+C	T-420	64561.75	94364.68	262.06	136.80	140.00	3.20	229	-62	102	2.83
A+B+C	T-420	64559.97	94363.13	257.66	140.00	142.35	2.35	229	-62	133	2.67
Below A	T-420	64559.97	94363.13	257.66	142.35	145.00	2.65	229	-62	9	0.17
Below A	T-420	64558.18	94361.57	253.25	145.00	150.00	5.00	229	-62	2	0.04
Below A	T-420	64556.39	94360.02	248.85	150.00	155.00	5.00	229	-62	5	0.05
Below A	T-421	64418.04	94344.24	389.68	0.00	5.00	5.00	48	-60	2	0.02

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-421	64419.91	94345.92	385.36	5.00	10.00	5.00	48	-60	10	0.49
Below A	T-421	64421.79	94347.59	381.04	10.00	15.00	5.00	48	-60	6	0.09
Below A	T-421	64423.66	94349.26	376.72	15.00	20.00	5.00	48	-60	10	0.13
Below A	T-421	64425.54	94350.92	372.39	20.00	21.00	1.00	49	-60	6	0.12
A+B+C	T-421	64425.54	94350.92	372.39	21.00	25.00	4.00	49	-60	40	0.33
A+B+C	T-421	64427.43	94352.58	368.07	25.00	30.00	5.00	49	-60	48	0.65
A+B+C	T-421	64429.33	94354.24	363.75	30.00	35.00	5.00	49	-60	27	0.26
A+B+C	T-421	64431.24	94355.89	359.43	35.00	40.00	5.00	49	-60	27	0.28
A+B+C	T-421	64433.14	94357.53	355.12	40.00	45.00	5.00	50	-60	22	0.22
A+B+C	T-421	64435.06	94359.17	350.80	45.00	50.00	5.00	50	-60	12	0.10
A+B+C	T-421	64436.98	94360.82	346.48	50.00	55.00	5.00	50	-60	17	0.09
A+B+C	T-421	64438.91	94362.44	342.17	55.00	60.00	5.00	50	-60	16	0.12
A+B+C	T-421	64440.84	94364.06	337.85	60.00	65.00	5.00	50	-60	38	0.31
A+B+C	T-421	64442.78	94365.67	333.53	65.00	66.16	1.16	50	-60	154	0.78
Vertical	T-421	64442.78	94365.67	333.53	66.16	70.00	3.84	50	-60	7	0.09
Vertical	T-421	64444.71	94367.29	329.22	70.00	75.00	5.00	50	-60	16	0.18
Vertical	T-421	64446.65	94368.92	324.90	75.00	80.00	5.00	50	-60	7	0.09
Vertical	T-421	64448.59	94370.53	320.58	80.00	85.00	5.00	50	-60	1	0.02
Vertical	T-421	64450.52	94372.14	316.26	85.00	90.00	5.00	50	-60	3	0.06
Vertical	T-421	64452.46	94373.75	311.94	90.00	95.00	5.00	50	-60	12	0.25
Vertical	T-421	64454.39	94375.35	307.62	95.00	100.00	5.00	50	-60	7	0.08
Vertical	T-421	64456.33	94376.96	303.30	100.00	105.00	5.00	50	-60	4	0.10
Vertical	T-421	64458.27	94378.56	298.98	105.00	110.00	5.00	51	-60	4	0.17
Vertical	T-421	64460.21	94380.15	294.66	110.00	115.00	5.00	51	-60	20	0.27
Vertical	T-421	64462.16	94381.75	290.33	115.00	120.00	5.00	51	-60	18	0.31
Vertical	T-421	64464.11	94383.33	286.01	120.00	125.00	5.00	51	-60	9	0.54
Vertical	T-421	64466.08	94384.90	281.69	125.00	130.00	5.00	52	-60	8	0.24
Vertical	T-421	64468.05	94386.47	277.37	130.00	135.00	5.00	52	-60	4	0.10
Vertical	T-421	64470.03	94388.03	273.05	135.00	140.00	5.00	52	-60	26	0.55
Vertical	T-421	64472.01	94389.59	268.73	140.00	145.00	5.00	52	-60	22	0.54
Vertical	T-421	64474.01	94391.14	264.42	145.00	150.00	5.00	53	-60	89	1.87
Vertical	T-421	64476.01	94392.67	260.10	150.00	155.00	5.00	53	-60	361	10.65
Vertical	T-421	64478.02	94394.19	255.78	155.00	160.00	5.00	53	-60	134	2.29
Vertical	T-421	64480.03	94395.71	251.47	160.00	165.00	5.00	53	-60	108	2.67
Vertical	T-421	64482.05	94397.23	247.15	165.00	170.00	5.00	53	-60	9	0.08
Vertical	T-421	64484.06	94398.75	242.83	170.00	175.00	5.00	53	-60	222	1.35
Vertical	T-421	64486.07	94400.27	238.51	175.00	180.00	5.00	53	-60	66	0.75
Vertical	T-421	64488.09	94401.78	234.20	180.00	185.00	5.00	53	-60	127	2.43
Vertical	T-421	64490.11	94403.30	229.88	185.00	190.00	5.00	53	-60	258	2.72
Vertical	T-421	64492.12	94404.82	225.56	190.00	195.00	5.00	53	-60	6	0.08
Vertical	T-421	64493.94	94406.19	221.67	195.00	199.02	4.02	53	-60	78	0.53
Vertical	T-422	64579.98	94420.22	380.78	0.00	5.00	5.00	220	-60	1	0.00
Vertical	T-422	64578.38	94418.31	376.45	5.00	10.00	5.00	220	-60	4	0.00
Vertical	T-422	64576.77	94416.39	372.12	10.00	15.00	5.00	220	-60	2	0.04
Vertical	T-422	64575.16	94414.48	367.79	15.00	20.00	5.00	220	-60	17	0.11
Vertical	T-422	64573.55	94412.57	363.46	20.00	25.00	5.00	220	-60	2	0.01
Vertical	T-422	64571.93	94410.67	359.13	25.00	30.00	5.00	220	-60	11	0.10
Vertical	T-422	64570.31	94408.76	354.80	30.00	35.00	5.00	220	-60	12	0.13
Vertical	T-422	64568.70	94406.85	350.47	35.00	40.00	5.00	221	-60	3	0.05
Vertical	T-422	64567.07	94404.96	346.14	40.00	45.00	5.00	221	-60	2	0.06
Vertical	T-422	64565.45	94403.05	341.81	45.00	50.00	5.00	221	-60	4	0.06
Vertical	T-422	64563.82	94401.15	337.48	50.00	55.00	5.00	221	-60	25	0.22
Vertical	T-422	64562.19	94399.26	333.15	55.00	60.00	5.00	221	-60	14	0.13
Vertical	T-422	64560.55	94397.38	328.82	60.00	65.00	5.00	221	-60	18	0.21

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-422	64558.90	94395.50	324.49	65.00	70.00	5.00	221	-60	5	0.10
Vertical	T-422	64557.25	94393.62	320.16	70.00	75.00	5.00	222	-60	20	0.37
Vertical	T-422	64555.59	94391.75	315.83	75.00	80.00	5.00	222	-60	209	1.38
Vertical	T-422	64553.94	94389.88	311.50	80.00	85.00	5.00	220	-60	243	1.28
Vertical	T-422	64552.27	94388.02	307.17	85.00	90.00	5.00	222	-60	46	0.28
Vertical	T-422	64550.59	94386.17	302.84	90.00	95.00	5.00	222	-60	94	0.69
Vertical	T-422	64548.91	94384.31	298.51	95.00	100.00	5.00	222	-60	113	1.14
Vertical	T-422	64547.23	94382.46	294.18	100.00	105.00	5.00	222	-60	41	0.30
Vertical	T-422	64545.55	94380.64	289.84	105.00	110.00	5.00	223	-60	130	0.87
Vertical	T-422	64543.86	94378.82	285.50	110.00	115.00	5.00	223	-60	95	1.04
Vertical	T-422	64542.17	94377.00	281.16	115.00	120.00	5.00	223	-60	88	1.13
Vertical	T-422	64540.48	94375.19	276.82	120.00	125.00	5.00	223	-60	654	11.41
Vertical	T-422	64538.78	94373.39	272.47	125.00	130.00	5.00	224	-60	747	7.89
A+B+C	T-422	64537.07	94371.60	268.12	130.00	135.00	5.00	224	-60	221	6.47
A+B+C	T-422	64535.37	94369.83	263.77	135.00	140.00	5.00	224	-61	53	0.57
A+B+C	T-422	64533.66	94368.06	259.42	140.00	145.00	5.00	224	-61	45	0.38
A+B+C	T-422	64531.95	94366.28	255.07	145.00	149.50	4.50	224	-61	131	1.27
Below A	T-422	64531.95	94366.28	255.07	149.50	150.00	0.50	224	-61	15	0.14
Below A	T-422	64530.53	94364.82	251.46	150.00	152.70	2.70	224	-61	14	0.15
Vertical	T-423	64362.16	94401.71	390.68	0.00	5.00	5.00	47	-47	8	0.20
Vertical	T-423	64364.65	94404.03	387.02	5.00	10.00	5.00	47	-47	9	0.04
Vertical	T-423	64367.16	94406.34	383.37	10.00	15.00	5.00	48	-47	8	0.06
Vertical	T-423	64369.68	94408.64	379.71	15.00	20.00	5.00	48	-47	10	0.32
Vertical	T-423	64372.19	94410.94	376.05	20.00	25.00	5.00	48	-47	16	0.17
Vertical	T-423	64374.72	94413.22	372.40	25.00	30.00	5.00	48	-47	3	0.05
Vertical	T-423	64377.25	94415.51	368.74	30.00	35.00	5.00	48	-47	6	0.08
Vertical	T-423	64379.80	94417.77	365.08	35.00	40.00	5.00	48	-47	13	0.15
Vertical	T-423	64382.35	94420.03	361.43	40.00	45.00	5.00	48	-47	8	0.07
Vertical	T-423	64384.92	94422.28	357.77	45.00	50.00	5.00	49	-47	4	0.05
Vertical	T-423	64387.49	94424.53	354.11	50.00	55.00	5.00	49	-47	6	0.07
Vertical	T-423	64390.06	94426.76	350.46	55.00	60.00	5.00	49	-47	176	2.69
Vertical	T-423	64392.62	94429.01	346.80	60.00	65.00	5.00	49	-47	31	0.52
Vertical	T-423	64395.19	94431.27	343.14	65.00	70.00	5.00	49	-47	6	0.07
Vertical	T-423	64397.75	94433.52	339.49	70.00	75.00	5.00	49	-47	177	1.58
Vertical	T-423	64400.30	94435.78	335.83	75.00	80.00	5.00	48	-47	3	0.04
Vertical	T-423	64402.85	94438.04	332.17	80.00	85.00	5.00	48	-47	1	0.04
Vertical	T-423	64405.40	94440.31	328.52	85.00	90.00	5.00	48	-47	1	0.06
Vertical	T-423	64407.94	94442.58	324.86	90.00	95.00	5.00	48	-47	1	0.05
Vertical	T-423	64410.48	94444.86	321.20	95.00	100.00	5.00	48	-47	5	0.10
Vertical	T-423	64413.02	94447.14	317.55	100.00	105.00	5.00	48	-47	66	0.84
Vertical	T-423	64415.55	94449.41	313.88	105.00	110.00	5.00	48	-47	1	0.06
Vertical	T-423	64418.08	94451.67	310.21	110.00	115.00	5.00	48	-47	0	0.05
Vertical	T-423	64420.62	94453.90	306.53	115.00	120.00	5.00	49	-48	0	0.00
Vertical	T-423	64423.16	94456.13	302.84	120.00	125.00	5.00	49	-48	0	0.00
Vertical	T-423	64425.70	94458.34	299.14	125.00	130.00	5.00	49	-48	0	0.00
Vertical	T-423	64428.24	94460.53	295.44	130.00	135.00	5.00	49	-48	27	0.33
Vertical	T-423	64430.78	94462.72	291.73	135.00	140.00	5.00	50	-48	0	0.00
Vertical	T-423	64433.32	94464.89	288.01	140.00	145.00	5.00	50	-48	0	0.00
Vertical	T-423	64435.78	94467.00	284.43	146.70	150.00	3.30	50	-48	0	0.01
Vertical	T-426	64553.11	94434.73	381.34	0.00	5.00	5.00	219	-59	3	0.01
Vertical	T-426	64551.46	94432.70	377.08	5.00	10.00	5.00	219	-59	2	0.03
Vertical	T-426	64549.82	94430.67	372.81	10.00	15.00	5.00	219	-59	3	0.03
Vertical	T-426	64548.17	94428.64	368.55	15.00	20.00	5.00	219	-59	4	0.06
Vertical	T-426	64546.52	94426.61	364.29	20.00	25.00	5.00	219	-59	14	0.10

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-426	64544.87	94424.59	360.02	25.00	30.00	5.00	219	-59	3	0.03
Vertical	T-426	64543.22	94422.57	355.76	30.00	35.00	5.00	219	-59	2	0.08
Vertical	T-426	64541.56	94420.54	351.50	35.00	40.00	5.00	219	-59	1	0.02
Vertical	T-426	64539.91	94418.52	347.23	40.00	45.00	5.00	219	-59	2	0.04
Vertical	T-426	64538.25	94416.51	342.97	45.00	50.00	5.00	220	-59	4	0.08
Vertical	T-426	64536.59	94414.50	338.71	50.00	55.00	5.00	220	-59	5	0.07
Vertical	T-426	64534.92	94412.48	334.44	55.00	60.00	5.00	220	-59	6	0.05
Vertical	T-426	64533.26	94410.46	330.18	60.00	65.00	5.00	220	-59	5	0.07
Vertical	T-426	64531.59	94408.46	325.92	65.00	70.00	5.00	220	-59	6	0.10
Vertical	T-426	64529.93	94406.45	321.65	70.00	75.00	5.00	220	-59	12	0.11
Vertical	T-426	64528.25	94404.44	317.39	75.00	80.00	5.00	220	-59	36	0.39
Vertical	T-426	64526.58	94402.43	313.13	80.00	85.00	5.00	220	-59	7	0.08
Vertical	T-426	64524.91	94400.42	308.86	85.00	90.00	5.00	220	-59	6	0.11
Vertical	T-426	64523.23	94398.42	304.60	90.00	95.00	5.00	220	-59	8	0.09
Vertical	T-426	64521.55	94396.42	300.34	95.00	100.00	5.00	220	-59	7	0.13
Vertical	T-426	64519.87	94394.42	296.07	100.00	105.00	5.00	220	-59	14	0.28
Vertical	T-426	64518.20	94392.42	291.81	105.00	110.00	5.00	220	-59	117	3.61
Vertical	T-426	64516.51	94390.42	287.55	110.00	115.00	5.00	220	-59	245	4.65
Vertical	T-426	64514.83	94388.42	283.28	115.00	120.00	5.00	220	-59	67	1.16
Vertical	T-426	64513.14	94386.42	279.02	120.00	125.00	5.00	220	-59	9	0.21
Vertical	T-426	64511.45	94384.43	274.76	125.00	130.00	5.00	220	-59	21	0.25
Vertical	T-426	64509.76	94382.44	270.50	130.00	135.00	5.00	220	-59	55	0.94
Vertical	T-426	64508.07	94380.45	266.23	135.00	140.00	5.00	220	-59	39	1.14
Vertical	T-426	64506.37	94378.46	261.97	140.00	144.85	4.85	220	-59	6	0.10
A+B+C	T-426	64506.37	94378.46	261.97	144.85	145.00	0.15	220	-59	13	0.19
A+B+C	T-426	64504.68	94376.47	257.71	145.00	150.00	5.00	221	-59	22	0.58
A+B+C	T-426	64502.98	94374.48	253.44	150.00	155.00	5.00	221	-59	32	0.71
A+B+C	T-426	64501.29	94372.50	249.18	155.00	160.00	5.00	221	-59	14	0.15
A+B+C	T-426	64499.59	94370.51	244.92	160.00	164.40	4.40	221	-59	21	0.87
Below A	T-426	64499.59	94370.51	244.92	164.40	165.00	0.60	221	-59	1	0.03
Below A	T-426	64498.23	94368.92	241.51	165.00	168.00	3.00	221	-59	4	0.07
Vertical	T-427	64570.00	94407.60	381.76	0.00	5.00	5.00	220	-61	2	0.01
Vertical	T-427	64568.45	94405.75	377.39	5.00	10.00	5.00	220	-61	27	0.22
Vertical	T-427	64566.88	94403.90	373.02	10.00	15.00	5.00	220	-61	83	0.59
Vertical	T-427	64565.32	94402.05	368.64	15.00	20.00	5.00	220	-61	121	0.86
Vertical	T-427	64563.75	94400.19	364.27	20.00	25.00	5.00	221	-61	17	0.13
Vertical	T-427	64562.18	94398.35	359.90	25.00	30.00	5.00	221	-61	13	0.14
Vertical	T-427	64560.60	94396.51	355.52	30.00	35.00	5.00	221	-61	334	2.14
Vertical	T-427	64559.02	94394.67	351.15	35.00	40.00	5.00	221	-61	5	0.08
Vertical	T-427	64557.44	94392.84	346.78	40.00	45.00	5.00	221	-61	3	0.07
Vertical	T-427	64555.85	94391.00	342.41	45.00	50.00	5.00	221	-61	6	0.07
Vertical	T-427	64554.26	94389.17	338.03	50.00	55.00	5.00	221	-61	5	0.09
Vertical	T-427	64552.67	94387.35	333.66	55.00	60.00	5.00	221	-61	31	0.33
Vertical	T-427	64551.08	94385.52	329.29	60.00	65.00	5.00	221	-61	8	0.15
Vertical	T-427	64549.49	94383.69	324.91	65.00	70.00	5.00	221	-61	87	0.38
Vertical	T-427	64547.90	94381.86	320.54	70.00	75.00	5.00	221	-61	61	0.96
Vertical	T-427	64546.31	94380.03	316.17	75.00	80.00	5.00	221	-61	12	0.17
Vertical	T-427	64544.71	94378.20	311.79	80.00	85.00	5.00	221	-61	45	0.47
Vertical	T-427	64543.12	94376.37	307.42	85.00	90.00	5.00	221	-61	6	0.11
Vertical	T-427	64541.54	94374.54	303.05	90.00	95.00	5.00	221	-61	32	0.73
Vertical	T-427	64539.95	94372.72	298.67	95.00	100.00	5.00	221	-61	48	0.38
Vertical	T-427	64538.36	94370.89	294.30	100.00	105.00	5.00	221	-61	24	0.28
Vertical	T-427	64536.77	94369.06	289.93	105.00	110.00	5.00	221	-61	22	0.23
Vertical	T-427	64535.18	94367.23	285.56	110.00	113.80	3.80	221	-61	21	0.21

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
A+B+C	T-427	64535.18	94367.23	285.56	113.80	115.00	1.20	221	-61	171	1.21
A+B+C	T-427	64533.59	94365.40	281.18	115.00	120.00	5.00	221	-61	35	0.21
A+B+C	T-427	64532.00	94363.57	276.81	120.00	125.00	5.00	221	-61	41	0.61
A+B+C	T-427	64530.40	94361.75	272.44	125.00	129.10	4.10	221	-61	21	1.28
Below A	T-427	64530.40	94361.75	272.44	129.10	130.00	0.90	221	-61	37	0.28
Below A	T-427	64528.81	94359.92	268.06	130.00	135.00	5.00	221	-61	86	0.76
Below A	T-427	64527.22	94358.08	263.69	135.00	140.00	5.00	221	-61	110	0.92
Below A	T-427	64525.63	94356.25	259.32	140.00	145.00	5.00	221	-61	11	0.10
Below A	T-427	64524.05	94354.43	254.94	145.00	150.00	5.00	221	-61	95	0.33
Below A	T-427	64522.46	94352.60	250.57	150.00	155.00	5.00	221	-61	25	0.20
Below A	T-427	64520.87	94350.78	246.20	155.00	159.00	4.00	221	-61	2	0.07
Vertical	T-428	64590.15	94432.62	379.51	0.00	5.00	5.00	220	-61	1	0.05
Vertical	T-428	64588.58	94430.72	375.16	5.00	10.00	5.00	220	-61	5	0.01
Vertical	T-428	64587.01	94428.83	370.81	10.00	15.00	5.00	220	-61	2	0.01
Vertical	T-428	64585.44	94426.93	366.46	15.00	20.00	5.00	220	-61	3	0.02
Vertical	T-428	64583.87	94425.03	362.11	20.00	25.00	5.00	220	-61	2	0.04
Vertical	T-428	64582.30	94423.14	357.76	25.00	30.00	5.00	220	-61	8	0.06
Vertical	T-428	64580.72	94421.25	353.40	30.00	35.00	5.00	220	-61	3	0.04
Vertical	T-428	64579.15	94419.35	349.05	35.00	40.00	5.00	220	-61	21	0.12
Vertical	T-428	64577.57	94417.46	344.70	40.00	45.00	5.00	220	-61	2	0.03
Vertical	T-428	64575.99	94415.57	340.35	45.00	50.00	5.00	220	-61	2	0.03
Vertical	T-428	64574.41	94413.68	336.00	50.00	55.00	5.00	220	-61	2	0.05
Vertical	T-428	64572.83	94411.80	331.64	55.00	60.00	5.00	220	-61	10	0.09
Vertical	T-428	64571.25	94409.91	327.29	60.00	65.00	5.00	220	-61	2	0.02
Vertical	T-428	64569.66	94408.03	322.94	65.00	70.00	5.00	220	-61	2	0.03
Vertical	T-428	64568.07	94406.15	318.59	70.00	75.00	5.00	220	-61	10	0.22
Vertical	T-428	64566.48	94404.27	314.24	75.00	80.00	5.00	220	-61	7	0.13
Vertical	T-428	64564.89	94402.39	309.89	80.00	85.00	5.00	220	-61	6	0.06
Vertical	T-428	64563.29	94400.52	305.53	85.00	90.00	5.00	221	-61	4	0.09
Vertical	T-428	64561.70	94398.65	301.18	90.00	95.00	5.00	221	-61	4	0.14
Vertical	T-428	64560.09	94396.78	296.83	95.00	100.00	5.00	221	-61	3	0.10
Vertical	T-428	64558.48	94394.92	292.48	100.00	105.00	5.00	221	-61	12	0.30
Vertical	T-428	64556.88	94393.05	288.13	105.00	110.00	5.00	221	-61	21	0.35
Vertical	T-428	64555.27	94391.18	283.78	110.00	115.00	5.00	221	-61	3	0.07
Vertical	T-428	64553.66	94389.32	279.42	115.00	120.00	5.00	221	-61	6	0.09
Vertical	T-428	64552.04	94387.46	275.07	120.00	125.00	5.00	221	-61	1	0.05
Vertical	T-428	64550.42	94385.60	270.72	125.00	130.00	5.00	221	-61	7	0.13
Vertical	T-428	64548.80	94383.75	266.37	130.00	135.00	5.00	221	-61	92	0.70
Vertical	T-428	64547.18	94381.91	262.02	135.00	140.00	5.00	221	-61	35	0.43
Vertical	T-428	64545.55	94380.06	257.66	140.00	145.00	5.00	221	-61	100	2.27
Vertical	T-428	64543.93	94378.21	253.31	145.00	147.00	2.00	222	-61	40	0.48
A+B+C	T-428	64543.93	94378.21	253.31	147.00	150.00	3.00	222	-61	97	1.93
A+B+C	T-428	64542.30	94376.36	248.96	150.00	155.00	5.00	222	-61	213	7.39
A+B+C	T-428	64540.66	94374.52	244.61	155.00	160.00	5.00	222	-61	78	2.46
A+B+C	T-428	64539.02	94372.68	240.26	160.00	165.00	5.00	222	-61	77	0.93
A+B+C	T-428	64537.38	94370.85	235.91	165.00	165.75	0.75	222	-61	90	0.86
Below A	T-428	64537.38	94370.85	235.91	165.75	170.00	4.25	222	-61	16	0.18
Below A	T-428	64535.74	94369.01	231.55	170.00	175.00	5.00	222	-61	8	0.07
Below A	T-428	64534.10	94367.17	227.20	175.00	180.00	5.00	222	-61	4	0.05
Below A	T-428	64532.45	94365.35	222.85	180.00	185.00	5.00	222	-61	1	0.02
Below A	T-428	64530.82	94363.53	218.55	185.00	189.88	4.88	222	-61	6	0.08
Vertical	T-439	64519.80	94449.46	379.93	0.00	5.00	5.00	224	-60	2	0.01
Vertical	T-439	64518.08	94447.65	375.60	5.00	10.00	5.00	224	-60	4	0.04
Vertical	T-439	64516.36	94445.84	371.27	10.00	15.00	5.00	224	-60	2	0.00

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-439	64514.64	94444.03	366.94	15.00	20.00	5.00	224	-60	1	0.00
Vertical	T-439	64512.92	94442.20	362.61	20.00	25.00	5.00	224	-60	4	0.05
Vertical	T-439	64511.20	94440.39	358.28	25.00	30.00	5.00	224	-60	14	0.16
Vertical	T-439	64509.47	94438.58	353.95	30.00	35.00	5.00	224	-60	58	0.49
Vertical	T-439	64507.75	94436.77	349.62	35.00	40.00	5.00	224	-60	9	0.08
Vertical	T-439	64506.03	94434.96	345.29	40.00	45.00	5.00	224	-60	6	0.09
Vertical	T-439	64504.32	94433.14	340.96	45.00	50.00	5.00	224	-60	5	0.10
Vertical	T-439	64502.59	94431.32	336.63	50.00	55.00	5.00	224	-60	3	0.06
Vertical	T-439	64500.87	94429.51	332.31	55.00	60.00	5.00	224	-60	3	0.07
Vertical	T-439	64499.14	94427.70	327.98	60.00	65.00	5.00	224	-60	10	0.23
Vertical	T-439	64497.41	94425.88	323.66	65.00	70.00	5.00	224	-60	8	0.14
Vertical	T-439	64495.67	94424.06	319.34	70.00	75.00	5.00	224	-60	5	0.07
Vertical	T-439	64493.93	94422.25	315.02	75.00	80.00	5.00	224	-60	4	0.06
Vertical	T-439	64492.18	94420.42	310.70	80.00	85.00	5.00	224	-60	3	0.08
Vertical	T-439	64490.43	94418.60	306.38	85.00	90.00	5.00	224	-60	6	0.09
Vertical	T-439	64488.68	94416.78	302.07	90.00	95.00	5.00	224	-60	2	0.05
Vertical	T-439	64486.92	94414.96	297.76	95.00	100.00	5.00	224	-60	4	0.08
Vertical	T-439	64485.16	94413.13	293.45	100.00	105.00	5.00	224	-60	8	0.18
Vertical	T-439	64483.38	94411.32	289.15	105.00	110.00	5.00	225	-59	4	0.11
Vertical	T-439	64481.59	94409.51	284.84	110.00	115.00	5.00	225	-59	11	0.19
Vertical	T-439	64479.78	94407.71	280.54	115.00	120.00	5.00	226	-59	27	0.34
Vertical	T-439	64477.95	94405.92	276.24	120.00	125.00	5.00	226	-59	17	0.25
Vertical	T-439	64476.11	94404.15	271.95	125.00	130.00	5.00	226	-59	12	0.18
Vertical	T-439	64474.26	94402.39	267.65	130.00	135.00	5.00	226	-59	29	0.31
Vertical	T-439	64472.39	94400.63	263.36	135.00	140.00	5.00	227	-59	38	0.44
Vertical	T-439	64470.50	94398.89	259.07	140.00	145.00	5.00	227	-59	13	0.22
Vertical	T-439	64468.61	94397.14	254.78	145.00	150.00	5.00	228	-59	71	1.96
Vertical	T-439	64466.70	94395.42	250.49	150.00	155.00	5.00	228	-59	111	3.61
Vertical	T-439	64464.77	94393.71	246.21	155.00	160.00	5.00	228	-59	63	1.16
Vertical	T-439	64462.84	94392.00	241.93	160.00	165.00	5.00	228	-59	26	0.74
Vertical	T-439	64460.90	94390.28	237.65	165.00	170.00	5.00	229	-59	13	0.14
Vertical	T-439	64458.95	94388.58	233.37	170.00	172.15	2.15	229	-59	43	0.95
A+B+C	T-439	64458.95	94388.58	233.37	172.15	175.00	2.85	229	-59	1428	23.28
A+B+C	T-439	64456.99	94386.87	229.10	175.00	180.00	5.00	229	-59	135	4.19
A+B+C	T-439	64455.02	94385.17	224.83	180.00	185.00	5.00	229	-59	62	1.83
A+B+C	T-439	64453.05	94383.48	220.56	185.00	190.00	5.00	230	-59	20	0.39
A+B+C	T-439	64451.06	94381.79	216.29	190.00	193.80	3.80	230	-59	10	0.14
Below A	T-439	64451.06	94381.79	216.29	193.80	195.00	1.20	230	-59	4	0.05
Below A	T-439	64449.07	94380.11	212.02	195.00	200.00	5.00	230	-59	5	0.12
Below A	T-439	64447.27	94378.60	208.20	200.00	203.97	3.97	230	-59	13	0.24
Vertical	T-440	64473.55	94473.50	379.44	0.00	5.00	5.00	221	-61	2	0.00
Vertical	T-440	64471.94	94471.64	375.09	5.00	10.00	5.00	221	-61	5	0.02
Vertical	T-440	64470.32	94469.79	370.74	10.00	15.00	5.00	221	-61	2	0.01
Vertical	T-440	64468.70	94467.95	366.38	15.00	20.00	5.00	221	-61	1	0.00
Vertical	T-440	64467.08	94466.10	362.02	20.00	25.00	5.00	222	-61	1	0.00
Vertical	T-440	64465.46	94464.27	357.66	25.00	30.00	5.00	222	-61	1	0.01
Vertical	T-440	64463.84	94462.44	353.30	30.00	35.00	5.00	222	-61	2	0.02
Vertical	T-440	64462.22	94460.62	348.94	35.00	40.00	5.00	222	-61	10	0.08
Vertical	T-440	64460.60	94458.79	344.57	40.00	45.00	5.00	222	-61	4	0.03
Vertical	T-440	64458.98	94456.99	340.20	45.00	50.00	5.00	222	-61	1	0.02
Vertical	T-440	64457.36	94455.19	335.83	50.00	55.00	5.00	222	-61	2	0.02
Vertical	T-440	64455.73	94453.38	331.46	55.00	60.00	5.00	222	-61	10	0.09
Vertical	T-440	64454.12	94451.57	327.09	60.00	65.00	5.00	222	-61	5	0.03
Vertical	T-440	64452.51	94449.73	322.72	65.00	70.00	5.00	221	-61	1	0.03

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-440	64450.90	94447.90	318.36	70.00	75.00	5.00	221	-61	0	0.01
Vertical	T-440	64449.30	94446.05	314.00	75.00	80.00	5.00	221	-61	1	0.01
Vertical	T-440	64447.70	94444.20	309.64	80.00	85.00	5.00	221	-61	1	0.03
Vertical	T-440	64446.10	94442.34	305.28	85.00	90.00	5.00	220	-61	1	0.02
Vertical	T-440	64444.51	94440.47	300.92	90.00	95.00	5.00	220	-61	1	0.04
Vertical	T-440	64442.93	94438.59	296.57	95.00	100.00	5.00	220	-61	8	0.14
Vertical	T-440	64441.34	94436.71	292.22	100.00	105.00	5.00	220	-61	4	0.06
Vertical	T-440	64439.75	94434.82	287.87	105.00	110.00	5.00	221	-60	8	0.07
Vertical	T-440	64438.14	94432.94	283.52	110.00	115.00	5.00	221	-60	3	0.03
Vertical	T-440	64436.52	94431.07	279.17	115.00	120.00	5.00	221	-60	1	0.02
Vertical	T-440	64434.89	94429.21	274.83	120.00	125.00	5.00	221	-60	2	0.03
Vertical	T-440	64433.25	94427.36	270.49	125.00	130.00	5.00	222	-60	2	0.03
Vertical	T-440	64431.59	94425.51	266.15	130.00	135.00	5.00	222	-60	2	0.03
Vertical	T-440	64429.92	94423.66	261.81	135.00	140.00	5.00	222	-60	1	0.02
Vertical	T-440	64428.24	94421.82	257.48	140.00	145.00	5.00	222	-60	5	0.03
Vertical	T-440	64426.55	94419.99	253.15	145.00	150.00	5.00	223	-60	8	0.07
Vertical	T-440	64424.84	94418.16	248.82	150.00	155.00	5.00	223	-60	11	0.12
Vertical	T-440	64423.14	94416.33	244.49	155.00	160.00	5.00	223	-60	4	0.05
Vertical	T-440	64421.42	94414.51	240.16	160.00	165.00	5.00	223	-60	1	0.02
Vertical	T-440	64419.71	94412.69	235.83	165.00	170.00	5.00	223	-60	3	0.04
Vertical	T-440	64417.99	94410.88	231.50	170.00	175.00	5.00	223	-60	2	0.04
Vertical	T-440	64416.27	94409.06	227.17	175.00	180.00	5.00	224	-60	15	0.35
Vertical	T-440	64414.55	94407.25	222.84	180.00	185.00	5.00	224	-60	60	1.08
Vertical	T-440	64412.82	94405.45	218.51	185.00	190.00	5.00	224	-60	26	0.57
Vertical	T-440	64411.09	94403.64	214.18	190.00	195.00	5.00	224	-60	21	0.56
Vertical	T-440	64409.36	94401.84	209.85	195.00	200.00	5.00	224	-60	4	0.04
Vertical	T-440	64407.62	94400.03	205.52	200.00	205.00	5.00	224	-60	3	0.03
Vertical	T-440	64405.88	94398.25	201.19	205.00	210.00	5.00	224	-60	4	0.09
Vertical	T-440	64404.13	94396.46	196.86	210.00	211.50	1.50	224	-60	5	0.11
A+B+C	T-440	64404.13	94396.46	196.86	211.50	215.00	3.50	224	-60	7	0.06
A+B+C	T-440	64402.37	94394.69	192.53	215.00	220.00	5.00	225	-60	12	0.06
A+B+C	T-440	64400.61	94392.92	188.19	220.00	225.00	5.00	225	-60	3	0.01
A+B+C	T-440	64398.84	94391.15	183.86	225.00	230.00	5.00	225	-60	2	0.02
A+B+C	T-440	64397.07	94389.39	179.53	230.00	231.70	1.70	225	-60	3	0.04
Below A	T-440	64397.07	94389.39	179.53	231.70	235.00	3.30	225	-60	2	0.02
Below A	T-440	64395.29	94387.63	175.20	235.00	240.00	5.00	226	-60	2	0.05
Below A	T-440	64393.50	94385.88	170.87	242.00	245.00	3.00	226	-60	1	0.06
A+B+C	T-441	64344.05	94394.86	218.37	193.75	195.00	1.25	221	-61	7	0.06
A+B+C	T-441	64342.47	94393.03	213.99	195.00	200.00	5.00	221	-61	19	0.41
A+B+C	T-441	64340.88	94391.20	209.62	200.00	200.75	0.75	221	-61	8	0.09
Vertical	T-444	64508.18	94435.15	381.50	0.00	5.00	5.00	222	-60	1	0.00
Vertical	T-444	64506.50	94433.25	377.19	5.00	10.00	5.00	222	-60	5	0.11
Vertical	T-444	64504.82	94431.36	372.88	10.00	15.00	5.00	222	-60	58	0.38
Vertical	T-444	64503.14	94429.46	368.56	15.00	20.00	5.00	222	-60	5	0.05
Vertical	T-444	64501.46	94427.57	364.25	20.00	25.00	5.00	222	-60	2	0.03
Vertical	T-444	64499.78	94425.69	359.93	25.00	30.00	5.00	222	-60	4	0.05
Vertical	T-444	64498.10	94423.81	355.62	30.00	35.00	5.00	222	-60	36	0.50
Vertical	T-444	64496.43	94421.93	351.30	35.00	40.00	5.00	222	-60	33	0.33
Vertical	T-444	64494.75	94420.06	346.97	40.00	45.00	5.00	222	-60	5	0.24
Vertical	T-444	64493.07	94418.19	342.65	45.00	50.00	5.00	222	-60	2	0.06
Vertical	T-444	64491.40	94416.33	338.32	50.00	55.00	5.00	222	-60	3	0.07
Vertical	T-444	64489.73	94414.47	333.99	55.00	60.00	5.00	222	-60	2	0.05
Vertical	T-444	64488.04	94412.61	329.66	60.00	65.00	5.00	222	-60	4	0.08
Vertical	T-444	64486.35	94410.76	325.34	65.00	70.00	5.00	222	-60	1	0.04

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-444	64484.66	94408.92	321.01	70.00	75.00	5.00	223	-60	2	0.04
Vertical	T-444	64482.96	94407.07	316.68	75.00	80.00	5.00	223	-60	6	0.11
Vertical	T-444	64481.25	94405.23	312.36	80.00	85.00	5.00	223	-60	163	1.91
Vertical	T-444	64479.53	94403.39	308.04	85.00	90.00	5.00	223	-60	107	1.08
Vertical	T-444	64477.80	94401.57	303.72	90.00	95.00	5.00	224	-60	4	0.05
Vertical	T-444	64476.07	94399.74	299.40	95.00	100.00	5.00	224	-60	47	0.96
Vertical	T-444	64474.34	94397.91	295.08	100.00	105.00	5.00	224	-60	293	3.81
Vertical	T-444	64472.59	94396.10	290.76	105.00	110.00	5.00	224	-60	4	0.12
Vertical	T-444	64470.83	94394.28	286.44	110.00	115.00	5.00	224	-60	2	0.04
Vertical	T-444	64469.08	94392.47	282.12	115.00	120.00	5.00	224	-60	4	0.11
Vertical	T-444	64467.32	94390.67	277.80	120.00	125.00	5.00	224	-60	1	0.05
Vertical	T-444	64465.57	94388.88	273.48	125.00	130.00	5.00	224	-60	2	0.05
Vertical	T-444	64463.81	94387.08	269.16	130.00	135.00	5.00	224	-60	4	0.12
Vertical	T-444	64462.05	94385.28	264.83	135.00	140.00	5.00	225	-60	15	0.49
Vertical	T-444	64460.29	94383.50	260.51	140.00	145.00	5.00	225	-60	4	0.10
Vertical	T-444	64458.53	94381.71	256.18	145.00	149.75	4.75	225	-60	4	0.09
A+B+C	T-444	64458.53	94381.71	256.18	149.75	150.00	0.25	225	-60	9	0.15
A+B+C	T-444	64456.77	94379.93	251.86	150.00	155.00	5.00	225	-60	22	0.33
A+B+C	T-444	64455.01	94378.14	247.53	155.00	160.00	5.00	225	-60	79	0.87
A+B+C	T-444	64453.24	94376.38	243.20	160.00	165.00	5.00	225	-60	31	0.40
A+B+C	T-444	64451.47	94374.61	238.87	165.00	168.75	3.75	225	-60	8	0.31
Below A	T-444	64451.47	94374.61	238.87	168.75	170.00	1.25	225	-60	1	0.03
Below A	T-444	64449.70	94372.85	234.54	170.00	175.00	5.00	225	-60	2	0.05
Below A	T-444	64448.66	94371.80	231.99	175.00	175.90	0.90	225	-60	2	0.03
A+B+C	T-463	64654.60	94223.61	377.72	0.00	5.00	5.00	221	-45	10	0.04
A+B+C	T-463	64652.29	94220.96	374.17	5.00	10.00	5.00	221	-45	14	0.11
A+B+C	T-463	64650.00	94218.30	370.61	10.00	15.00	5.00	221	-45	27	0.43
A+B+C	T-463	64647.70	94215.64	367.05	15.00	20.00	5.00	221	-45	20	0.15
A+B+C	T-463	64645.41	94212.98	363.49	20.00	24.55	4.55	221	-45	156	1.32
Below A	T-463	64645.41	94212.98	363.49	24.55	25.00	0.45	221	-45	14	0.19
Below A	T-463	64643.12	94210.32	359.93	25.00	30.00	5.00	221	-46	11	0.09
Below A	T-463	64640.86	94207.67	356.39	30.00	34.93	4.93	221	-46	18	0.04
Vertical	T-464	64515.85	94462.50	379.20	0.00	5.00	5.00	191	-46	2	0.00
Vertical	T-464	64515.21	94459.05	375.63	5.00	10.00	5.00	191	-46	4	0.01
Vertical	T-464	64514.57	94455.60	372.07	10.00	15.00	5.00	191	-45	3	0.00
Vertical	T-464	64513.92	94452.15	368.51	15.00	20.00	5.00	191	-45	2	0.03
Vertical	T-464	64513.28	94448.69	364.95	20.00	25.00	5.00	191	-45	1	0.02
Vertical	T-464	64512.62	94445.24	361.40	25.00	30.00	5.00	191	-45	2	0.04
Vertical	T-464	64511.97	94441.78	357.84	30.00	35.00	5.00	191	-45	3	0.03
Vertical	T-464	64511.31	94438.32	354.30	35.00	40.00	5.00	191	-45	6	0.07
Vertical	T-464	64510.65	94434.86	350.75	40.00	45.00	5.00	191	-45	13	0.14
Vertical	T-464	64509.98	94431.39	347.21	45.00	50.00	5.00	191	-45	3	0.06
Vertical	T-464	64509.30	94427.92	343.68	50.00	55.00	5.00	191	-45	2	0.04
Vertical	T-464	64508.62	94424.46	340.14	55.00	60.00	5.00	191	-45	2	0.04
Vertical	T-464	64507.93	94420.99	336.60	60.00	65.00	5.00	191	-45	1	0.03
Vertical	T-464	64507.24	94417.52	333.07	65.00	70.00	5.00	192	-45	5	0.08
Vertical	T-464	64506.54	94414.06	329.53	70.00	75.00	5.00	192	-45	1	0.03
Vertical	T-464	64505.82	94410.59	326.00	75.00	80.00	5.00	192	-45	4	0.05
Vertical	T-464	64505.11	94407.13	322.46	80.00	85.00	5.00	192	-45	3	0.02
Vertical	T-464	64504.38	94403.67	318.93	85.00	90.00	5.00	192	-45	6	0.07
Vertical	T-464	64503.64	94400.21	315.39	90.00	95.00	5.00	192	-45	57	0.92
Vertical	T-464	64502.90	94396.76	311.86	95.00	100.00	5.00	192	-45	58	0.42
Vertical	T-464	64502.16	94393.30	308.32	100.00	105.00	5.00	192	-45	39	0.40
Vertical	T-464	64501.39	94389.85	304.79	105.00	110.00	5.00	193	-45	18	0.22

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Vertical	T-464	64500.61	94386.39	301.26	110.00	115.00	5.00	193	-45	20	0.36
Vertical	T-464	64499.82	94382.94	297.73	115.00	120.00	5.00	193	-45	9	0.19
Vertical	T-464	64499.02	94379.48	294.21	120.00	125.00	5.00	193	-45	9	0.23
Vertical	T-464	64498.20	94376.03	290.69	125.00	130.00	5.00	194	-45	3	0.08
Vertical	T-464	64497.36	94372.57	287.17	130.00	135.00	5.00	194	-45	13	0.26
Vertical	T-464	64496.51	94369.13	283.66	135.00	140.00	5.00	194	-45	19	0.33
Vertical	T-464	64495.65	94365.67	280.15	140.00	141.55	1.55	194	-45	14	0.37
A+B+C	T-464	64495.65	94365.67	280.15	141.55	145.00	3.45	194	-45	50	0.86
A+B+C	T-464	64494.77	94362.22	276.64	145.00	150.00	5.00	195	-45	18	0.50
A+B+C	T-464	64493.88	94358.77	273.14	150.00	155.00	5.00	195	-45	81	0.58
A+B+C	T-464	64492.99	94355.32	269.63	155.00	156.15	1.15	195	-45	382	7.64
Below A	T-464	64492.99	94355.32	269.63	156.15	160.00	3.85	195	-45	9	0.12
Below A	T-464	64492.09	94351.86	266.13	160.00	164.00	4.00	195	-45	56	0.50
Vertical	T-465	64608.46	94455.79	376.94	3.04	5.00	1.96	218	-60	6	0.02
Vertical	T-465	64606.89	94453.79	372.63	5.00	10.00	5.00	218	-60	13	0.02
Vertical	T-465	64605.32	94451.80	368.32	10.00	15.00	5.00	218	-60	3	0.01
Vertical	T-465	64603.75	94449.81	364.01	15.00	20.00	5.00	218	-60	8	0.01
Vertical	T-465	64602.18	94447.82	359.70	20.00	25.00	5.00	219	-59	2	0.00
Vertical	T-465	64600.59	94445.83	355.40	25.00	30.00	5.00	219	-59	1	0.02
Vertical	T-465	64598.99	94443.84	351.10	30.00	35.00	5.00	219	-59	1	0.03
Vertical	T-465	64597.39	94441.86	346.79	35.00	40.00	5.00	219	-59	1	0.03
Vertical	T-465	64595.79	94439.89	342.49	40.00	45.00	5.00	219	-59	2	0.02
Vertical	T-465	64594.17	94437.92	338.19	45.00	50.00	5.00	220	-59	1	0.02
Vertical	T-465	64592.55	94435.95	333.89	50.00	55.00	5.00	220	-59	1	0.03
Vertical	T-465	64590.91	94433.97	329.59	55.00	60.00	5.00	220	-59	0	0.02
Vertical	T-465	64589.27	94432.00	325.30	60.00	65.00	5.00	220	-59	1	0.02
Vertical	T-465	64587.61	94430.03	321.02	65.00	70.00	5.00	220	-59	1	0.02
Vertical	T-465	64585.95	94428.07	316.73	70.00	75.00	5.00	220	-59	1	0.06
Vertical	T-465	64584.27	94426.10	312.45	75.00	80.00	5.00	221	-59	1	0.04
Vertical	T-465	64582.58	94424.14	308.17	80.00	85.00	5.00	221	-59	1	0.05
Vertical	T-465	64580.88	94422.17	303.90	85.00	90.00	5.00	221	-59	1	0.03
Vertical	T-465	64579.17	94420.22	299.63	90.00	95.00	5.00	221	-59	1	0.03
Vertical	T-465	64577.45	94418.27	295.36	95.00	100.00	5.00	222	-59	3	0.08
Vertical	T-465	64575.72	94416.32	291.09	100.00	105.00	5.00	222	-59	5	0.18
Vertical	T-465	64573.98	94414.36	286.83	105.00	110.00	5.00	222	-59	3	0.10
Vertical	T-465	64572.23	94412.42	282.57	110.00	115.00	5.00	222	-59	7	0.28
Vertical	T-465	64570.48	94410.49	278.30	115.00	120.00	5.00	223	-59	7	0.16
Vertical	T-465	64568.71	94408.57	274.04	120.00	125.00	5.00	223	-59	3	0.05
Vertical	T-465	64566.94	94406.65	269.78	125.00	130.00	5.00	223	-59	2	0.02
Vertical	T-465	64565.16	94404.74	265.51	130.00	135.00	5.00	223	-59	19	0.47
Vertical	T-465	64563.37	94402.83	261.25	135.00	140.00	5.00	224	-59	5	0.10
Vertical	T-465	64561.57	94400.94	256.99	140.00	145.00	5.00	224	-59	10	0.21
Vertical	T-465	64559.76	94399.06	252.72	145.00	150.00	5.00	224	-59	4	0.07
Vertical	T-465	64557.95	94397.17	248.46	150.00	155.00	5.00	224	-59	4	0.06
Vertical	T-465	64556.12	94395.30	244.20	155.00	160.00	5.00	224	-58	5	0.05
Vertical	T-465	64554.29	94393.42	239.94	160.00	165.00	5.00	224	-58	2	0.05
Vertical	T-465	64552.46	94391.55	235.69	165.00	170.00	5.00	225	-58	122	0.67
Vertical	T-465	64550.61	94389.68	231.43	170.00	175.00	5.00	225	-58	9	0.25
Vertical	T-465	64548.76	94387.81	227.18	175.00	176.58	1.58	225	-58	6	0.05
A+B+C	T-465	64548.76	94387.81	227.18	176.58	180.00	3.42	225	-58	111	2.09
A+B+C	T-465	64546.90	94385.95	222.93	180.00	185.00	5.00	225	-58	38	1.01
A+B+C	T-465	64545.03	94384.08	218.68	185.00	189.00	4.00	225	-58	76	1.82
Below A	T-465	64545.03	94384.08	218.68	189.00	190.00	1.00	225	-58	4	0.10
Below A	T-465	64543.16	94382.22	214.44	190.00	195.00	5.00	225	-58	3	0.14

Assay Composite Listing - Karina-Unión, All Domains

		Mid-Point Coordinates (Truncated)			Drill Depth Interval			Interval Orientation		Composite Grades	
Domain	Hole_ID	East	North	Elevation (m)	From (m)	To (m)	Length (m)	Azimuth	Inclination	Ag (g/t)	Au (g/t)
Below A	T-465	64541.27	94380.36	210.20	195.00	200.00	5.00	226	-58	6	0.17
Below A	T-465	64539.38	94378.51	205.96	200.00	205.00	5.00	226	-58	7	0.06
Below A	T-465	64537.49	94376.65	201.72	205.00	210.00	5.00	226	-58	4	0.14
Below A	T-465	64535.60	94374.79	197.48	210.00	215.00	5.00	226	-58	0	0.01
Below A	T-465	64534.22	94373.43	194.38	215.00	217.31	2.31	226	-58	1	0.01
Vertical	T-518	64531.02	94463.07	346.68	39.43	40.00	0.57	217	-60	0	0.00
Vertical	T-518	64529.52	94461.07	342.35	40.00	45.00	5.00	217	-60	0	0.00
Vertical	T-518	64528.02	94459.07	338.02	45.00	50.00	5.00	217	-60	0	0.00
Vertical	T-518	64526.51	94457.08	333.69	50.00	55.00	5.00	217	-60	0	0.00
Vertical	T-518	64525.01	94455.08	329.36	55.00	60.00	5.00	217	-60	0	0.00
Vertical	T-518	64523.50	94453.08	325.03	60.00	65.00	5.00	217	-60	0	0.00
Vertical	T-518	64522.00	94451.09	320.70	65.00	70.00	5.00	217	-60	0	0.00
Vertical	T-518	64520.49	94449.09	316.37	70.00	75.00	5.00	217	-60	0	0.00
Vertical	T-518	64518.99	94447.10	312.04	75.00	80.00	5.00	217	-60	1	0.00
Vertical	T-518	64517.48	94445.10	307.71	80.00	85.00	5.00	217	-60	2	0.02
Vertical	T-518	64515.98	94443.10	303.38	85.00	90.00	5.00	217	-60	0	0.00
Vertical	T-518	64514.48	94441.10	299.05	90.00	95.00	5.00	217	-60	0	0.00
Vertical	T-518	64512.97	94439.11	294.72	95.00	100.00	5.00	217	-60	2	0.02
Vertical	T-518	64511.46	94437.11	290.39	100.00	105.00	5.00	217	-60	4	0.03
Vertical	T-518	64509.96	94435.11	286.06	105.00	110.00	5.00	217	-60	5	0.08
Vertical	T-518	64508.46	94433.12	281.73	110.00	115.00	5.00	217	-60	5	0.06
Vertical	T-518	64506.95	94431.12	277.40	115.00	120.00	5.00	217	-60	57	0.58
Vertical	T-518	64505.45	94429.13	273.07	120.00	125.00	5.00	217	-60	10	0.07
Vertical	T-518	64503.94	94427.13	268.74	125.00	130.00	5.00	217	-60	7	0.09
Vertical	T-518	64502.44	94425.14	264.41	130.00	135.00	5.00	217	-60	0	0.00
Vertical	T-518	64500.93	94423.14	260.08	135.00	140.00	5.00	217	-60	0	0.00
Vertical	T-518	64499.43	94421.14	255.75	140.00	145.00	5.00	217	-60	2	0.01
Vertical	T-518	64497.93	94419.14	251.42	145.00	150.00	5.00	217	-60	5	0.08
Vertical	T-518	64496.42	94417.14	247.09	150.00	155.00	5.00	217	-60	1	0.01
Vertical	T-518	64494.91	94415.15	242.76	155.00	160.00	5.00	217	-60	0	0.00
Vertical	T-518	64493.41	94413.15	238.43	160.00	165.00	5.00	217	-60	0	0.00
Vertical	T-518	64491.91	94411.16	234.10	165.00	170.00	5.00	217	-60	0	0.00
Vertical	T-518	64490.40	94409.16	229.77	170.00	175.00	5.00	217	-60	0	0.00
Vertical	T-518	64488.90	94407.17	225.44	175.00	180.00	5.00	217	-60	0	0.00
Vertical	T-518	64487.39	94405.17	221.11	180.00	185.00	5.00	217	-60	19	0.42
Vertical	T-518	64485.89	94403.17	216.78	185.00	190.00	5.00	217	-60	15	0.28
Vertical	T-518	64484.38	94401.17	212.45	190.00	195.00	5.00	217	-60	6	0.08
Vertical	T-518	64482.88	94399.17	208.12	195.00	200.00	5.00	217	-60	3	0.04
Vertical	T-518	64481.37	94397.18	203.79	200.00	205.00	5.00	217	-60	10	0.44
Vertical	T-518	64479.87	94395.18	199.46	205.00	205.85	0.85	217	-60	4	0.05
A+B+C	T-518	64479.87	94395.18	199.46	205.85	210.00	4.15	217	-60	7	0.23
A+B+C	T-518	64478.37	94393.19	195.13	210.00	215.00	5.00	217	-60	2	0.04
A+B+C	T-518	64476.86	94391.19	190.80	215.00	220.00	5.00	217	-60	3	0.03
A+B+C	T-518	64475.36	94389.19	186.47	220.00	225.00	5.00	217	-60	2	0.03
A+B+C	T-518	64473.85	94387.20	182.14	225.00	228.40	3.40	217	-60	2	0.04
Below A	T-518	64473.85	94387.20	182.14	228.40	230.00	1.60	217	-60	3	0.05
Below A	T-518	64472.35	94385.20	177.81	230.00	235.00	5.00	217	-60	2	0.03
Below A	T-518	64471.05	94383.48	174.07	235.00	238.64	3.64	217	-60	1	0.03